

## 382 MT Maiden JORC Resource at Port Moresby Limestone project – key milestone in PNG's Nation Building Industrialisation agenda with an opportunity for new Lime and Cement Industry

### HIGHLIGHTS:

- Significant maiden Resource (JORC 2012) of 382 million tonnes (MT) of high grade limestone across two deposits (Kido / Lea Lea), situated along the coastline 25km from the capital Port Moresby on tenement EL2303.
- 205MT @ 53.5% CaO classified as a 'Measured Mineral Resource', 128 MT @ 51.8% CaO classified as 'Indicated Mineral Resource' and 49 MT @48.3% CaO considered to be an *Inferred Mineral Resource*.
- 22 diamond holes totaling 1,592.5 metres drilled across the two deposits.
- 806 multi-element assays from core used to determine the Resource estimate. These assays were generally consistent with the rock chip data previously collected.
- At surface coastal location with minimal strip ratio, expected to yield very low raw limestone mining costs to be competitively priced and proposed to be utilized on site in vertically integrated lime kilns and cement making facilities.
- The large scale and quality of the limestone Resource has potential to enable the development of a multi-generational lime and cement (clinker/powder) business, located next to PNG's first LNG Plant (PNG LNG)^.
- Further advances MRL's three pillar 'Nation Building Industrialisation Strategy' to diversify PNG's mineral resources inventory and develop associated downstream value add industry.
- Opportunity to supply lime to PNG domestic and international export markets e.g. Australia's alumina and copper/gold mining sectors; also, clinker and powder cement exported into Australian based coastal import terminals.
- BFS and Commercialization study underway with completion planned in 2018\*

^refer to separate announcement re Mayur signing gas supply MOU with Kumul Petroleum; \*subject to outcome of joint venture strategy

**Mayur Resources Ltd (ASX:MRL)** has delineated a limestone Mineral Resource estimate of 382 Mt (2012 JORC) at its Port Moresby limestone project. This is a key milestone in MRL's strategy of developing PNG's huge mineral wealth and assisting in the country's 'Nation Building' Industrialisation agenda.

As previously announced on 24 October 2017, a 22-hole drilling programme was completed across the two deposits of Kido and Lea Lea and following the completion of subsequent assaying, petrological test works MRL engaged Groundwork Plus to undertake a resource estimation study. The Resource estimate is summarised in the table below.

**MEASURED MINERAL RESOURCE ESTIMATE\***

Area	Category	CaO cut off %**	Tonnes	CaO %	Al <sub>2</sub> O <sub>3</sub> %	SiO <sub>2</sub> %
Lea Lea	Measured	52%	61,000,000	53.4	0.6	1.65
Kido	Measured	52%	144,000,000	53.6	0.62	1.77
<b>Total</b>	<b>Measured</b>	<b>52%</b>	<b>205,000,000*</b>	<b>53.5</b>	<b>0.61</b>	<b>1.73</b>

**INDICATED MINERAL RESOURCE ESTIMATE\***

Area	Category	CaO cut off %**	Tonnes	CaO %	Al <sub>2</sub> O <sub>3</sub> %	SiO <sub>2</sub> %
Lea Lea	Indicated	50%	117,000,000	51.8	0.9	2.7
Kido	Indicated	50%	11,000,000	51.5	0.6	1.1
<b>Total</b>	<b>Indicated</b>	<b>50%</b>	<b>128,000,000</b>	<b>51.8</b>	<b>0.9</b>	<b>2.6</b>

**INFERRED MINERAL RESOURCE ESTIMATE\***

Area	Category	CaO cut off %**	Tonnes	CaO %	Al <sub>2</sub> O <sub>3</sub> %	SiO <sub>2</sub> %
Lea Lea	Inferred	48%	7,000,000	48.1	1.1	2.5
Kido	Inferred	48%	42,000,000	48.4	1	1.8
<b>Total</b>	<b>Inferred</b>	<b>48%</b>	<b>49,000,000</b>	<b>48.3</b>	<b>1</b>	<b>1.9</b>

\*Minor rounding errors apply pursuant to JORC 2012. \*\*The cut-off grade for the Measured Mineral Resource is based on a commonly accepted CaO grade for the production of lime and quick lime.

**Table 1 - Port Moresby Limestone Project – JORC Resource Statement**

Mineral Resources have been reported in terms of CaO as this is the value used in most specifications for production of raw kiln feed and clinker. CaO or quicklime is produced upon heating or calcination of the CaCO<sub>3</sub> limestone raw feed. A commonly used conversion factor is CaCO<sub>3</sub> X 0.56 = CaO, although this generic equation should be used with care and has been provided to allow for a quick approximation of CaCO<sub>3</sub> levels.

It should be noted that the work by Groundwork Plus is at a Mineral Resource Estimate level where further works will be undertaken with the objective to have sufficient information to support the estimation of ore reserves. Further work and appropriate studies are required before Mayur will be able to estimate any ore reserves or, to provide any assurance of an economic development case being viable. Additionally, this further work may or may not result in the upgrade of the Mineral Resources to Ore Reserves.



**Figure 1 – Drill pad at Kido deposit with the PNG LNG plant site in the far distance. White limestone outcrop and subcrop is evident in the foreground.**



**Figure 2 – Aerial photo of the Kido coastal deposit**



**Figure 3 – Limestone sample pit at Kido deposit showing the limited thickness of overburden occurring on site.**

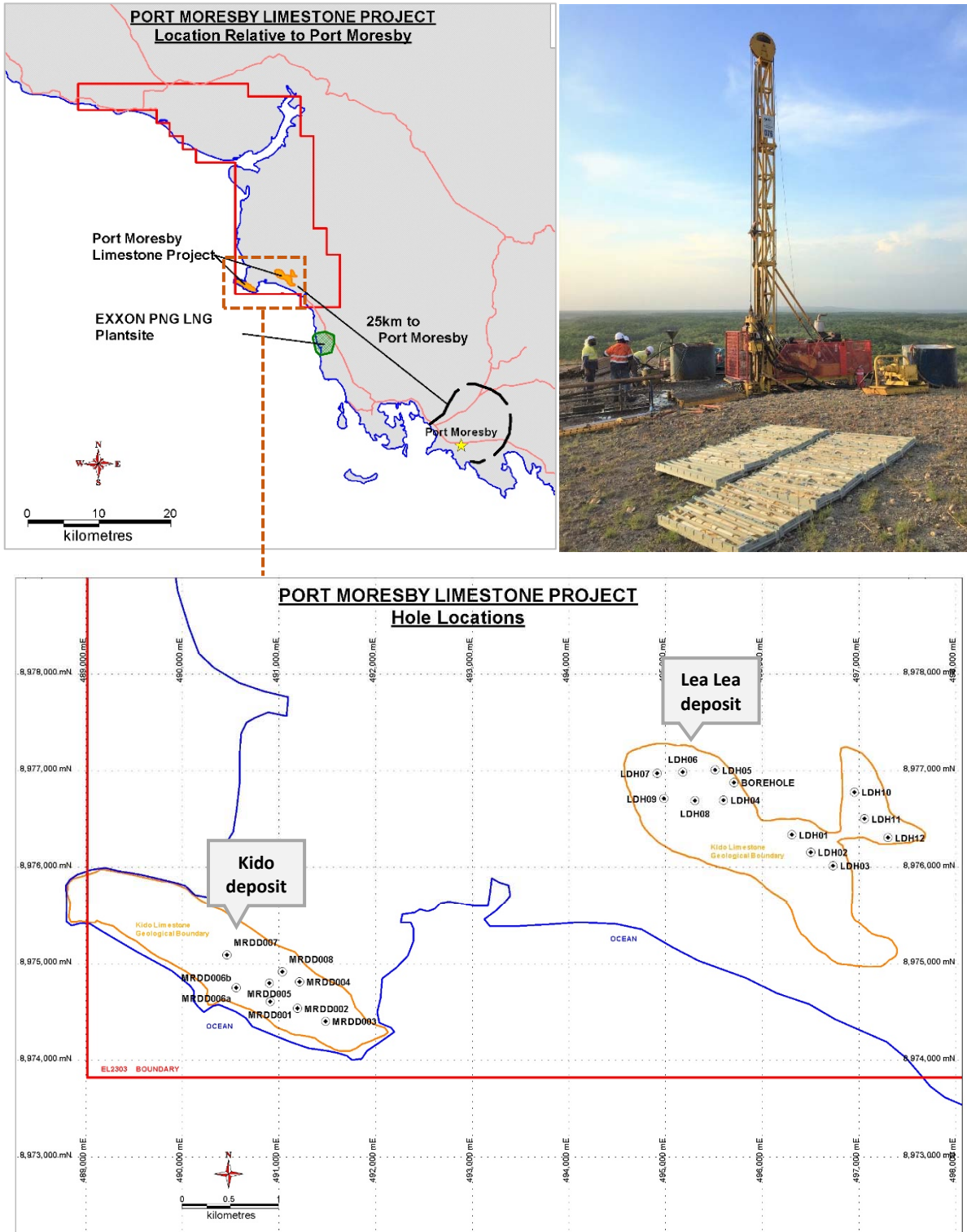
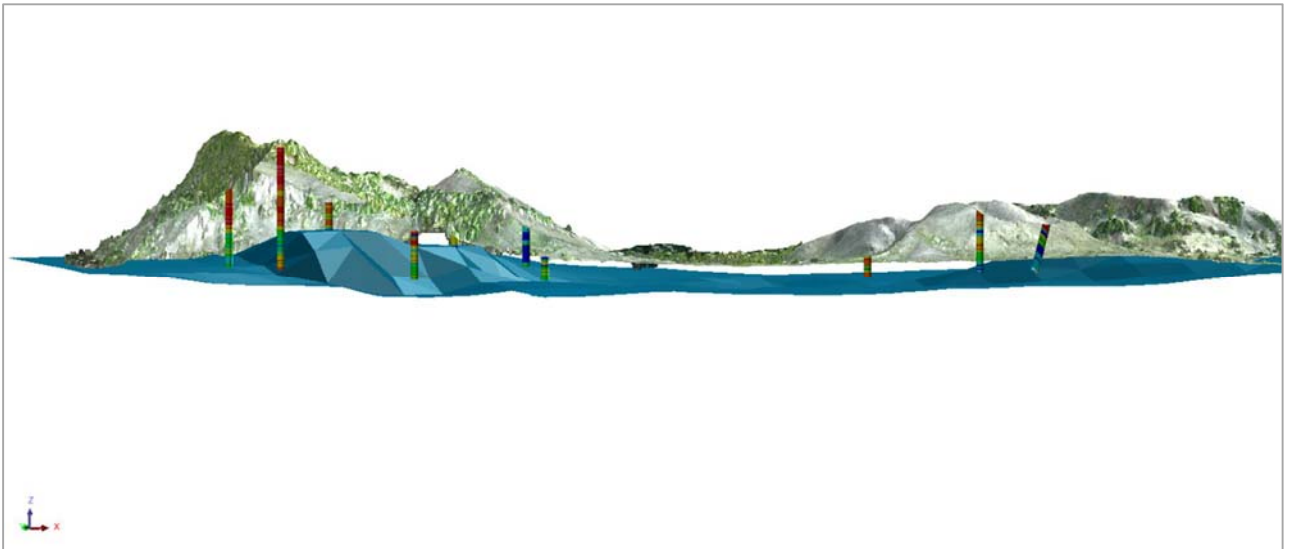


Figure 4 - (Clockwise from top left) Location of Port Moresby Limestone project, drill rig and core trays on Lea Lea, and location of drill holes at Kido and Lea Lea within Mayur's EL2303 (refer to 24 October 2017 Announcement for drill hole coordinates)

The full assay results of the 22 holes drilled at Kido and Lea Lea are provided in **Annexure A and B** respectively



**Figure 5 - Indicative 3D cross section of the Lea Lea deposit – with the interpreted base of the limestone shown by the blue surface. The drill holes are visible as coloured columns beneath the green topographic surface.**

Refer to **Annexure C** for more detailed plan and sectional diagrams for the drill holes at Kido and Lea Lea.

### **Advancing PNG’s ‘Nation Building’ Industrialisation Agenda**

MRL is pursuing a strategy of advancing PNGs nation building agenda via the development of the country’s rich natural resources inventory. This is based on establishing several development pillars as follows:

PILLAR 1	PILLAR 2	PILLAR 3
COORDINATED DEVELOPMENT OF MINERAL AND ENERGY RESOURCES	DIVERSIFICATION OF PNG’S MINERAL WEALTH	DEVELOPMENT OF DOMESTIC DOWNSTREAM VERTICALLY INTEGRATED INDUSTRY

**Table 1 – MRLs strategic pillars to advance PNG Nation Building agenda**

As part of Pillar 1, and as previously announced (7 December 2017), the Company has entered a Memorandum of Agreement (MOA) with the Gulf Provincial Government. Gulf Province is situated adjacent to Central Province and is home to extensive mineral and energy resources. MRL has extensive mineral exploration interests in Gulf Province and intends to leverage the proximity of plentiful, cheap and accessible domestic energy to industrial mineral resources to deliver various development opportunities for the region.

Delineating a significant JORC Resource at the Port Moresby limestone JORC in Central Province is a key milestone in diversifying PNG’s mineral wealth (‘Pillar 2’) beyond copper and gold that have traditionally dominated the mining industry in PNG. The Port Moresby project has also been endorsed by the Central Province Governor (Hon. Robert Agarobe) who recently visited site with MRL’s executive management team. The Governor has committed to be involved and help drive economic activity and prosperity for the people of Central Province.

The JORC Resource of 382 million tonnes now provides the foundation to develop a domestic and export lime and cement based business in Caution Bay (Central Province). It is anticipated that there will be a downstream value add opportunity to service PNG’s domestic quicklime and cement needs

along with other lime products as well as develop an export industry to supply to such countries as Australia and other Asia Pacific jurisdictions.

With the limestone being at surface, on the coast, next to gas (PNG LNG) and with domestic and international markets nearby, this provides a compelling opportunity and an ideal pillar for nation building in PNG. Exxon Mobil has already expended some USD\$20 billion in establishing the first LNG facility in PNG at Caution Bay with TOTAL SA in JV with Exxon and others proposing the next LNG facility that is also proposed to be of a similar multibillion dollar investment size.

The establishment of such a precinct on the coast at Caution Bay aims to open up various value adding industries supported by the PNG governments ‘domestic market obligation rights’ for provision of gas. This has already commenced with cheaper more reliable gas being provided for power generation by the PNG LNG facility at Caution Bay (being undertaken by Kumul Petroleum and Oil Search) that displaces higher cost imported fuel oils.

There are also regional opportunities of note, that include Australia’s initial shift towards importation of clinker due to increasing energy costs and other factors such as higher cost labour. Moreover, Australian producers are now also importing cement in final powdered form, to avoid high energy costs of grinding imported clinker and established powder based cement import terminals.



**Figure 6 - limestone was crushed for petrography analysis, and shows good aggregate potential and shape**

MRL has commenced discussions with domestic and international consumers of quicklime as well as a number of Australian businesses in relation to the importation of cement (clinker and powder) – as there is interest in supply diversification, supporting PNG locally produced products as well as reducing current supply costs in comparison to their other domestic and international suppliers.

MRL’s lime strategy is aligned with the ongoing development of bi-lateral trade between Australia and PNG and seeks to provide a pathway to create a highly competitive cement and lime business that ultimately rivals the current suppliers servicing Australia and wider south-east Asia and Pacific region.



**Figure 7 - Mayur's Head of Business Affairs (Darren Lockyer), MD (Paul Mulder) and Central Province Governor (Hon Robert Agarobe) addressing the community at the Port Moresby Limestone Project**

## Conclusion

On the release of this maiden JORC, MRL MD Mr Paul Mulder commented “This limestone JORC Resource is a particularly exciting development for the company and represents a key vertical integration opportunity for MRL to add significant value both within PNG and for MRL shareholders gaining exposure to a downstream industry that will aim to supply domestic and international markets that are vulnerable to a disruptive entrant”.

Major strategic advantages of the Port Moresby limestone JORC Resource include the following:

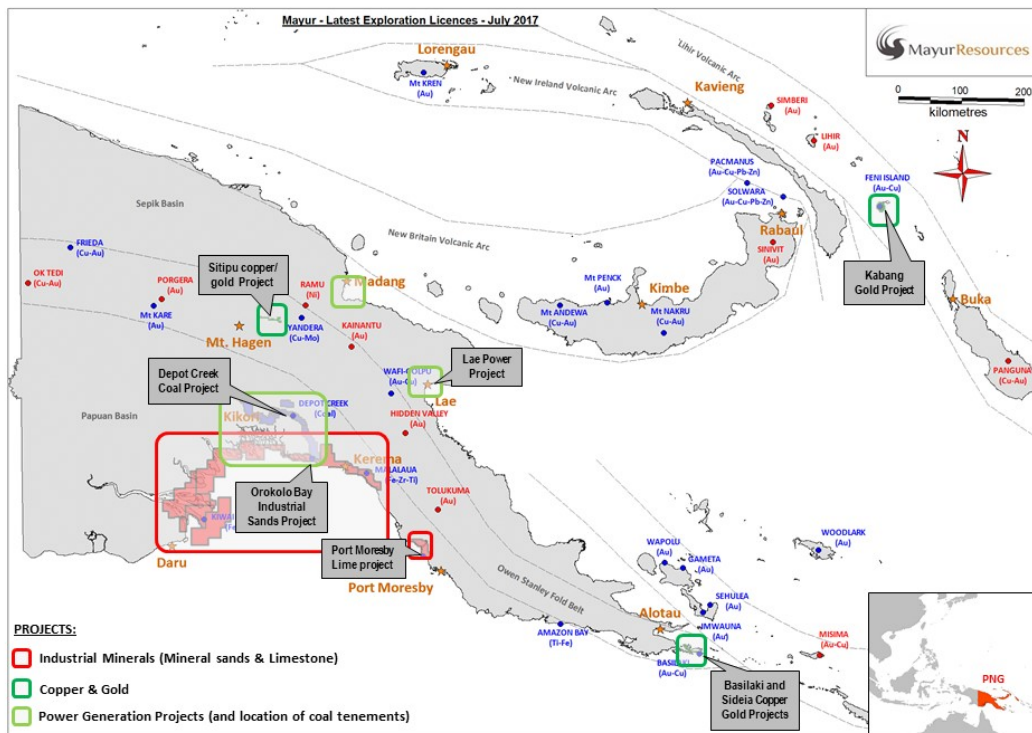
- (1) located on the coast only 25km from Port Moresby.
- (2) located close to anticipated low-cost energy sources in the form of coal (via deposits owned by MRL) and gas.
- (3) located just 7km from the US\$20bn PNG LNG production facility as well as the proposed LNG facility being developed by TOTAL SA
- (4) access to PNG's low labour costs
- (5) a coastal location to enable easy access to both existing domestic Quick lime and cement end users and other regional markets in Australia and Asia Pacific.

## COMPETENT PERSONS STATEMENT

Statements contained in this announcement relating to Mineral Resource estimates are based on, and fairly represents, information and supporting documentation prepared by Mr. Rod Huntley, who is a member of the Australian Institute of Geoscientists). Mr. Huntley has decades of sufficient and relevant experience (including PNG) that specifically relate to the delineation of limestone deposits. The type and method of assay testing used to obtain the results reported in this announcement (provided by ALS Global) were set by Mr Huntley in advance of this exploration campaign taking place. Mr Huntley qualifies as a Competent Person as defined in the Australian Code for Reporting of Identified Mineral Resources and Ore Reserves (JORC) Code 2012. Mr Huntley is an employee of Groundworks Pty Ltd and is contracted as a consultant to Mayur Resources and consents to the use of the matters based on his information in the form and context in which it appears. As a competent person Mr Huntley takes responsibility for the form and context in which this initial Mineral Resource Estimate prepared for the Port Moresby Lime and Aggregate Project appears.

## About Mayur Resources

Mayur has been operating since 2011 with the purpose of acquiring, exploring and developing mineral and energy development opportunities in Papua New Guinea and neighbouring countries.



Over the last 5 years Mayur has established an impressive portfolio of projects that includes:

- (a) **Industrial Minerals.** (construction sands, magnetite sands, heavy mineral sands and limestone) The Company is focusing its efforts on developing the Orokolo Bay Industrial Sands Project along the southern coast of PNG. Following the delineation of a JORC Resource, a Pre-Feasibility Study was completed based on a low-cost mining operation using a combination of excavators and simple gravity and magnetic mineral processing. The PFS also identified the opportunity to establish a multi-product mine that could produce fine grain construction sands, titanomagnetite (iron ore), industrial magnetite and a zircon-rich Valuable Heavy Mineral Concentrate by-product. The Company has secured a permit to export up to 200,000 tonnes of material that may enable the company to begin bulk sample shipments for customer testing by December 2018. The other key project in this portfolio is the Port Moresby Limestone Project which seeks to develop a multi-product lime based business for both domestic and export markets.
- (b) **Copper and Gold.** The Company holds the Feni Island Project in New Ireland Province, as well as the prospective Basilaki/ Sideia project in Milne Bay Province and the Sitipu project located in the Eastern Highlands region of the prolific Owen Stanley Fold Belt. The company is undertaking or planning exploration activities at each of the projects.
- (c) **Coal and Power.** The Company has delineated PNG's first JORC coal Resource at Depot Creek in the Gulf Province and has been developing a vertically integrated domestic power project at PNG's second largest city of Lae. A definitive feasibility study has been completed for a project that utilizes domestic coal from Depot Creek together with other renewable fuel sources to power a 52.5MW (net) power facility at Lae (with future scalability to 200MW). The Company has, via PNG Ports, secured an Environmental Approval from the Conservation and Environmental Protection Authority in PNG, to construct the power facility and on the request of PNG Power, the state-owned power entity, has submitted a detailed Power Purchase Agreement (PPA).

### Enquiries

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## Annexure A – Kido Drilling Results (9 Holes)

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
MRDD001	0	2	53.1	94.8	0.9	0.58	0.41	0.005	2.59
MRDD001	2	4	48.4	86.4	2.49	1.27	0.69	0.01	8.12
MRDD001	4	6	51.8	92.4	1.26	0.79	0.49	0.005	4.08
MRDD001	6	8	51.7	92.3	1.29	0.72	0.5	0.005	4.12
MRDD001	8	10	49.8	88.9	1.64	0.91	0.58	0.005	5.51
MRDD001	10	12	52	92.8	1.16	0.76	0.53	0.01	3.49
MRDD001	12	14	54.4	97.1	0.22	0.19	0.31	0.01	0.62
MRDD001	14	16	54	96.4	0.53	0.47	0.39	0.01	1.57
MRDD001	16	18	53.6	95.7	0.61	0.42	0.43	0.01	1.87
MRDD001	18	20	53.8	96	0.56	0.42	0.41	0.01	1.79
MRDD001	20	22	53.7	95.8	0.65	0.48	0.45	0.01	2.04
MRDD001	22	24	53.5	95.5	0.68	0.5	0.44	0.01	2.02
MRDD001	24	26	52.9	94.4	0.53	0.36	0.38	0.005	1.65
MRDD001	26	28	53	94.6	0.77	0.48	0.42	0.01	2.63
MRDD001	28	30	53.6	95.7	0.39	0.29	0.32	0.005	1.32
MRDD001	30	32	54.7	97.6	0.32	0.24	0.33	0.005	0.98
MRDD001	32	34	53.5	95.5	0.38	0.27	0.32	0.01	1.1
MRDD001	34	36	54.6	97.4	0.27	0.22	0.34	0.01	0.8
MRDD001	36	38	53.3	95.1	0.5	0.35	0.35	0.01	1.54
MRDD001	38	40	54.3	96.9	0.38	0.26	0.33	0.01	1.19
MRDD001	40	42	54.2	96.7	0.39	0.29	0.32	0.005	1.18
MRDD001	42	44	54.6	97.4	0.24	0.2	0.33	0.005	0.67
MRDD001	44	46	54.9	98	0.17	0.16	0.29	0.005	0.46
MRDD001	46	48	54.5	97.3	0.26	0.23	0.32	0.005	0.71
MRDD001	48	50	53.7	95.8	0.35	0.3	0.34	0.01	1.01
MRDD001	50	52	54.8	97.8	0.23	0.18	0.33	0.01	0.62
MRDD001	52	54	54.7	97.6	0.26	0.22	0.32	0.005	0.7
MRDD001	54	56	54.7	97.6	0.24	0.17	0.36	0.005	0.63
MRDD001	56	58	54.9	98	0.17	0.11	0.33	0.005	0.42
MRDD001	58	60	54.5	97.3	0.21	0.18	0.4	0.01	0.54
MRDD001	60	62	54.5	97.3	0.29	0.21	0.42	0.01	0.74
MRDD001	62	64	54.3	96.9	0.37	0.22	0.44	0.01	0.91
MRDD001	64	66	53.4	95.3	0.37	0.24	0.39	0.01	0.92
MRDD001	66	68	53.3	95.1	0.41	0.27	0.4	0.01	1.06
MRDD001	68	70	53.7	95.8	0.45	0.32	0.74	0.02	1.16
MRDD001	70	72	53.8	96	0.47	0.41	0.47	0.03	1.19
MRDD001	72	74	52.9	94.4	0.59	0.38	0.53	0.03	1.5
MRDD001	74	76	53.4	95.3	0.53	0.52	0.54	0.03	1.44
MRDD001	76	78	53.8	96	0.22	0.15	0.33	0.01	0.54
MRDD001	78	80	54.7	97.6	0.18	0.13	0.27	0.005	0.45

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
MRDD001	80	82	55	98.2	0.22	0.15	0.28	0.005	0.53
MRDD001	82	84	54.9	98	0.23	0.15	0.27	0.005	0.56
MRDD001	84	86	54.8	97.8	0.25	0.16	0.27	0.005	0.61
MRDD001	86	88	53.9	96.2	0.26	0.17	0.31	0.005	0.63
MRDD001	88	90	53.9	96.2	0.26	0.16	0.31	0.005	0.63
MRDD001	90	92	55	98.2	0.13	0.09	0.26	0.005	0.31
MRDD001	92	94	54.3	96.9	0.13	0.1	0.27	0.005	0.34
MRDD001	94	96	54.6	97.4	0.22	0.14	0.31	0.005	0.5
MRDD001	96	98	54.7	97.6	0.21	0.13	0.31	0.005	0.51
MRDD002	0	2	54.6	97.4	0.23	0.15	0.27	0.005	0.52
MRDD002	2	4	51.2	91.4	1.4	0.71	0.45	0.005	4.12
MRDD002	4	6	52	92.8	1.14	0.69	0.43	0.005	3.22
MRDD002	6	8	52.7	94	0.93	0.6	0.4	0.005	2.59
MRDD002	8	10	50.8	90.7	1.62	0.9	0.5	0.01	4.57
MRDD002	10	12	51.9	92.6	1.23	0.73	0.46	0.005	3.48
MRDD002	12	14	52.1	93	1.19	0.72	0.46	0.005	3.35
MRDD002	14	16	52.2	93.2	1.14	0.68	0.44	0.005	3.17
MRDD002	16	18	51.3	91.5	1.46	0.86	0.53	0.005	4.11
MRDD002	18	20	51.7	92.3	1.29	0.79	0.47	0.01	3.56
MRDD002	20	22	53.7	95.8	0.54	0.41	0.34	0.005	1.45
MRDD002	22	24	52.7	94	0.85	0.6	0.44	0.01	2.34
MRDD002	24	26	51.7	92.3	1.18	0.82	0.49	0.01	3.48
MRDD002	26	28	53.3	95.1	0.65	0.47	0.4	0.005	2.09
MRDD002	28	30	54.1	96.5	0.46	0.33	0.36	0.005	1.32
MRDD002	30	32	53.3	95.1	0.6	0.43	0.39	0.005	1.62
MRDD002	32	34	53.6	95.7	0.55	0.37	0.37	0.005	1.47
MRDD002	34	36	52.2	93.2	0.98	0.65	0.5	0.01	2.66
MRDD002	36	38	52.1	93	1.04	0.67	0.53	0.01	2.82
MRDD002	38	40	53.6	95.7	0.5	0.34	0.39	0.005	1.38
MRDD002	40	42	54.7	97.6	0.24	0.18	0.33	0.005	0.65
MRDD002	42	44	54.5	97.3	0.29	0.19	0.32	0.005	0.69
MRDD002	44	46	54.1	96.5	0.44	0.3	0.34	0.005	1.1
MRDD002	46	48	54.6	97.4	0.22	0.16	0.29	0.005	0.52
MRDD002	48	50	55.3	98.7	0.13	0.13	0.26	0.005	0.31
MRDD002	50	52	54	96.4	0.17	0.13	0.3	0.005	0.4
MRDD002	52	54	54.4	97.1	0.32	0.21	0.36	0.005	0.76
MRDD002	54	56	54.4	97.1	0.33	0.23	0.32	0.005	0.77
MRDD002	56	58	54.5	97.3	0.22	0.19	0.34	0.01	0.51
MRDD002	58	60	54.6	97.4	0.28	0.22	0.34	0.01	0.69
MRDD002	60	62	54.1	96.5	0.37	0.29	0.43	0.02	0.91
MRDD002	62	64	54	96.4	0.39	0.3	0.4	0.02	0.92
MRDD002	64	66	54.1	96.5	0.37	0.27	0.42	0.02	0.93

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
MRDD002	66	68	54.1	96.5	0.37	0.25	0.39	0.02	0.95
MRDD002	68	70	54.1	96.5	0.33	0.23	0.38	0.02	0.91
MRDD002	70	72	55.1	98.3	0.13	0.1	0.28	0.01	0.29
MRDD003	0	2	53.7	95.8	0.52	0.33	0.35	0.01	1.29
MRDD003	2	4	53.7	95.8	0.54	0.33	0.37	0.005	1.46
MRDD003	4	6	49.3	88	1.96	1.15	0.67	0.01	5.52
MRDD003	6	8	47.1	84.1	2.8	1.71	0.83	0.01	7.97
MRDD003	8	10	54	96.4	0.38	0.25	0.33	0.005	1.06
MRDD003	10	12	51.4	91.7	1.18	0.72	0.53	0.01	3.79
MRDD003	12	14	51.7	92.3	1.15	0.68	0.55	0.005	3.66
MRDD003	14	16	51.4	91.7	1.09	0.64	0.54	0.005	3.45
MRDD003	16	18	51.2	91.4	1.19	0.68	0.55	0.005	3.62
MRDD003	18	20	53	94.6	0.63	0.46	0.44	0.005	1.94
MRDD003	20	22	51.6	92.1	1.14	0.76	0.6	0.01	3.52
MRDD003	22	24	49.6	88.5	1.76	1.11	0.71	0.01	5.25
MRDD003	24	26	50.3	89.8	1.46	0.96	0.67	0.01	4.64
MRDD003	26	28	53.1	94.8	0.56	0.39	0.43	0.01	1.89
MRDD003	28	30	53.3	95.1	0.52	0.37	0.43	0.005	1.68
MRDD003	30	32	53.8	96	0.37	0.3	0.37	0.005	1.15
MRDD003	32	34	53.2	94.9	0.63	0.4	0.42	0.005	1.92
MRDD003	34	36	52.6	93.9	0.75	0.49	0.47	0.01	2.39
MRDD003	36	38	52.9	94.4	0.79	0.52	0.5	0.005	2.45
MRDD003	38	40	55	98.2	0.31	0.27	0.38	0.01	0.99
MRDD003	40	42	54	96.4	0.44	0.37	0.41	0.005	1.32
MRDD003	42	44	54.6	97.4	0.36	0.33	0.43	0.01	1.04
MRDD003	44	46	55	98.2	0.31	0.21	0.39	0.005	0.83
MRDD003	46	48	55.4	98.9	0.21	0.14	0.36	0.005	0.52
MRDD003	48	50	55.4	98.9	0.16	0.16	0.34	0.005	0.39
MRDD003	50	52	54.6	97.4	0.27	0.2	0.38	0.01	0.64
MRDD003	52	54	54.2	96.7	0.35	0.27	0.37	0.02	0.85
MRDD003	54	56	54	96.4	0.34	0.29	0.41	0.02	0.85
MRDD003	56	57.6	54	96.4	0.32	0.36	0.38	0.01	0.76
MRDD004	0	2	54.8	97.8	0.32	0.27	0.31	0.01	0.67
MRDD004	2	4	54.5	97.3	0.24	0.24	0.37	0.02	0.55
MRDD004	4	6	53.8	96	0.38	0.35	0.38	0.02	0.89
MRDD004	6	8	54.3	96.9	0.56	0.43	0.32	0.02	1.3
MRDD004	8	10	54.3	96.9	0.28	0.21	0.28	0.005	0.66
MRDD004	10	12	54.5	97.3	0.49	0.33	0.34	0.01	1.19
MRDD004	12	14	54.9	98	0.36	0.28	0.33	0.01	0.9
MRDD004	14	16	53.5	95.5	0.86	0.53	0.4	0.01	2.17
MRDD004	16	18	52.5	93.7	1.28	0.77	0.49	0.01	3.25
MRDD004	18	20	51.2	91.4	1.26	0.78	0.47	0.01	3.56

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
MRDD004	20	22	52.6	93.9	0.97	0.61	0.42	0.01	3
MRDD004	22	24	52.8	94.2	0.81	0.59	0.38	0.01	2.85
MRDD004	24	26	53.4	95.3	0.73	0.61	0.35	0.02	2.53
MRDD004	26	28	53.1	94.8	0.63	0.65	0.33	0.03	1.95
MRDD004	28	30	53.4	95.3	0.62	0.45	0.38	0.01	1.94
MRDD004	30	32	50.8	90.7	1.64	1.09	0.54	0.02	5.17
MRDD004	32	34	52.2	93.2	0.86	0.62	0.42	0.01	2.74
MRDD004	34	36	53.2	94.9	0.73	0.54	0.42	0.01	2.47
MRDD004	36	38	47.4	84.6	2.67	1.69	0.98	0.02	8.76
MRDD004	38	40	47.1	84.1	2.36	1.56	0.97	0.01	7.6
MRDD005	0	1.8	55.2	98.5	0.31	0.17	0.2	0.005	0.74
MRDD005	1.8	4	55.6	99.2	0.39	0.27	0.22	0.005	0.95
MRDD005	4	6	53.9	96.2	0.63	0.43	0.31	0.005	1.65
MRDD005	6	8	54.6	97.4	0.35	0.29	0.28	0.005	0.93
MRDD005	8	10	55.3	98.7	0.33	0.25	0.32	0.005	0.81
MRDD005	10	12	54.4	97.1	0.32	0.24	0.29	0.005	0.75
MRDD005	12	14	55.4	98.9	0.28	0.21	0.28	0.005	0.69
MRDD005	14	16	54.3	96.9	0.4	0.31	0.28	0.005	0.96
MRDD005	16	18	54.2	96.7	0.39	0.23	0.3	0.005	0.9
MRDD005	18	20	54.3	96.9	0.32	0.23	0.31	0.005	0.74
MRDD005	20	22	54.7	97.6	0.2	0.15	0.32	0.005	0.58
MRDD005	22	24	55.4	98.9	0.15	0.12	0.29	0.01	0.31
MRDD005	24	26	54.5	97.3	0.18	0.13	0.29	0.01	0.38
MRDD005	26	28.2	55.3	98.7	0.26	0.19	0.3	0.01	0.58
MRDD006A	0	2	53.6	95.7	0.33	0.22	0.36	0.005	0.89
MRDD006A	2	4	54.7	97.6	0.3	0.24	0.44	0.01	0.81
MRDD006A	4	6	53.6	95.7	0.38	0.29	0.45	0.005	1.03
MRDD006A	6	8	54.2	96.7	0.33	0.27	0.4	0.01	0.9
MRDD006A	8	10	54	96.4	0.46	0.33	0.46	0.01	1.33
MRDD006A	10	12	54.1	96.5	0.22	0.19	0.35	0.005	0.59
MRDD006A	12	14	54.6	97.4	0.31	0.26	0.38	0.01	0.91
MRDD006A	14	16	54.6	97.4	0.3	0.28	0.38	0.02	0.85
MRDD006A	16	18	53.6	95.7	0.6	0.48	0.49	0.02	1.72
MRDD006A	18	20	54.3	96.9	0.38	0.28	0.41	0.02	1.08
MRDD006A	20	22	54.1	96.5	0.26	0.15	0.35	0.01	0.69
MRDD006A	22	24	54.4	97.1	0.16	0.1	0.33	0.01	0.48
MRDD006A	24	26	54.6	97.4	0.21	0.18	0.4	0.02	0.54
MRDD006A	26	28	54.8	97.8	0.2	0.15	0.35	0.01	0.52
MRDD006A	28	30	54.8	97.8	0.19	0.19	0.41	0.02	0.52
MRDD006A	30	32	54.4	97.1	0.18	0.15	0.41	0.01	0.48
MRDD006B	0	2.4	54.1	96.5	0.58	0.37	0.46	0.005	1.42
MRDD006B	2.4	4.4	54.6	97.4	0.47	0.35	0.47	0.005	1.16

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
MRDD006B	4.4	6	54.5	97.3	0.41	0.32	0.44	0.005	1.02
MRDD006B	6	8.1	54.6	97.4	0.41	0.32	0.42	0.01	1.04
MRDD006B	8.1	10.1	54.8	97.8	0.41	0.31	0.38	0.005	1.13
MRDD006B	10.1	11.8	54.7	97.6	0.38	0.31	0.36	0.005	1.04
MRDD006B	11.8	13.9	55.4	98.9	0.26	0.26	0.35	0.01	0.72
MRDD006B	13.9	16	53.2	94.9	0.79	0.55	0.48	0.02	2.2
MRDD006B	16	18	53.4	95.3	0.78	0.58	0.48	0.02	2.14
MRDD006B	18	20	54.8	97.8	0.47	0.3	0.44	0.01	1.25
MRDD006B	20	22	54.7	97.6	0.31	0.18	0.35	0.01	0.85
MRDD006B	22	24	55.6	99.2	0.17	0.12	0.31	0.01	0.46
MRDD006B	24	26	55	98.2	0.27	0.2	0.36	0.01	0.68
MRDD006B	26	28	54.8	97.8	0.29	0.25	0.41	0.02	0.73
MRDD006B	28	30	54.9	98	0.22	0.22	0.39	0.01	0.53
MRDD006B	30	32	54.6	97.4	0.29	0.24	0.43	0.01	0.74
MRDD006B	32	34	54.9	98	0.21	0.16	0.46	0.01	0.56
MRDD006B	34	36	55.4	98.9	0.19	0.15	0.43	0.01	0.47
MRDD006B	36	38	55.2	98.5	0.2	0.16	0.45	0.01	0.49
MRDD006B	38	40	55	98.2	0.18	0.2	0.37	0.02	0.46
MRDD006B	40	42	54.7	97.6	0.28	0.26	0.48	0.03	0.66
MRDD006B	42	44	55.3	98.7	0.23	0.22	0.47	0.02	0.57
MRDD006B	44	46	54.9	98	0.22	0.22	0.4	0.02	0.56
MRDD006B	46	47.6	55.4	98.9	0.14	0.15	0.35	0.01	0.34
MRDD006B	47.6	49.6	55	98.2	0.23	0.18	0.35	0.01	0.59
MRDD006B	49.6	51.6	55	98.2	0.3	0.22	0.34	0.005	0.77
MRDD006B	51.6	53	55.1	98.3	0.21	0.15	0.28	0.005	0.49
MRDD006B	53	55	56	99.9	0.19	0.17	0.3	0.005	0.46
MRDD006B	55	57	54.1	96.5	0.39	0.31	0.35	0.005	1
MRDD006B	57	59	54	96.4	0.29	0.2	0.31	0.005	0.74
MRDD006B	59	61	55.1	98.3	0.24	0.2	0.3	0.005	0.63
MRDD006B	61	63	55.8	99.6	0.21	0.18	0.28	0.005	0.54
MRDD006B	63	65	55	98.2	0.2	0.16	0.28	0.005	0.5
MRDD006B	65	67	54.8	97.8	0.38	0.28	0.36	0.005	1.01
MRDD006B	67	69	54.7	97.6	0.3	0.22	0.32	0.005	0.81
MRDD006B	69	71	54.6	97.4	0.3	0.23	0.34	0.005	0.8
MRDD006B	71	73	54.8	97.8	0.29	0.22	0.34	0.005	0.77
MRDD007	0	2	54.8	97.8	0.35	0.22	0.24	0.005	0.82
MRDD007	2	4	55.2	98.5	0.35	0.24	0.29	0.005	0.84
MRDD007	4	6.2	55.1	98.3	0.33	0.24	0.29	0.005	0.81
MRDD007	6.2	8.3	54.7	97.6	0.36	0.26	0.31	0.005	0.94
MRDD007	8.3	10.6	54.1	96.5	0.62	0.38	0.35	0.005	1.55
MRDD007	10.6	12.3	54.6	97.4	0.46	0.3	0.32	0.005	1.2
MRDD007	12.3	14.5	54.5	97.3	0.46	0.32	0.32	0.005	1.24
MRDD007	14.5	16.8	53.7	95.8	0.82	0.48	0.4	0.005	2.14

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
MRDD007	16.8	19	53.9	96.2	0.89	0.54	0.41	0.01	2.21
MRDD007	19	21	53	94.6	1.07	0.69	0.48	0.01	2.93
MRDD007	21	23	53.7	95.8	0.76	0.52	0.42	0.01	2.1
MRDD007	23	25	53.8	96	0.77	0.5	0.42	0.01	2.21
MRDD007	25	27	53.8	96	0.7	0.48	0.5	0.03	1.95
MRDD007	27	29.1	53.9	96.2	0.69	0.51	0.47	0.02	1.97
MRDD007	29.1	31	54.4	97.1	0.44	0.32	0.32	0.005	1.27
MRDD007	31	33	55.1	98.3	0.35	0.26	0.32	0.005	0.96
MRDD007	33	34.6	54.7	97.6	0.35	0.25	0.32	0.005	0.94
MRDD007	34.6	36.6	54.7	97.6	0.35	0.25	0.31	0.005	0.93
MRDD007	36.6	38.6	54.4	97.1	0.46	0.33	0.34	0.005	1.18
MRDD007	38.6	40	54.4	97.1	0.47	0.32	0.35	0.005	1.23
MRDD007	40	42	55	98.2	0.38	0.28	0.31	0.005	0.99
MRDD007	42	44	54.6	97.4	0.47	0.32	0.34	0.005	1.21
MRDD007	44	46	54.3	96.9	0.57	0.39	0.35	0.01	1.47
MRDD007	46	48	54.5	97.3	0.46	0.31	0.34	0.005	1.18
MRDD007	48	50	54.3	96.9	0.63	0.4	0.42	0.02	1.65
MRDD007	50	52	53	94.6	1.14	0.73	0.54	0.03	3.03
MRDD007	52	54	54	96.4	0.85	0.55	0.41	0.01	2.31
MRDD007	54	55.7	52.7	94	1.14	0.69	0.43	0.01	3.15
MRDD007	55.7	58	51.5	91.9	1.8	1.04	0.53	0.01	4.91
MRDD007	58	60	52.7	94	1.1	0.67	0.41	0.005	2.98
MRDD007	60	62	53.8	96	0.66	0.42	0.32	0.005	1.78
MRDD007	62	64	53.9	96.2	0.63	0.4	0.34	0.005	1.62
MRDD007	64	65.5	54.4	97.1	0.74	0.48	0.37	0.005	1.98
MRDD007	65.5	68.7	49.1	87.6	2.17	1.23	0.6	0.01	6.54
MRDD007	68.7	70.2	53.3	95.1	0.81	0.53	0.4	0.005	2.41
MRDD007	70.2	72	52.3	93.3	1.19	0.74	0.48	0.005	3.6
MRDD007	72	74	52.9	94.4	1.1	0.7	0.47	0.01	3.3
MRDD007	74	76	53	94.6	1.14	0.77	0.47	0.01	3.43
MRDD007	76	78	51.3	91.5	1.56	1	0.54	0.01	4.57
MRDD007	78	79.7	52.7	94	0.99	0.79	0.5	0.01	2.8
MRDD007	79.7	81.4	53.6	95.7	0.7	0.47	0.46	0.01	1.96
MRDD007	81.4	83	53.8	96	0.55	0.43	0.42	0.005	1.7
MRDD007	83	84.5	54.2	96.7	0.39	0.45	0.37	0.01	1.2
MRDD007	84.5	86	54	96.4	0.41	0.32	0.4	0.005	1.26
MRDD007	86	88	52.6	93.9	0.93	0.68	0.49	0.01	2.9
MRDD007	88	90	52.8	94.2	0.83	0.6	0.5	0.01	2.56
MRDD007	90	91.7	53.1	94.8	0.85	0.64	0.51	0.01	2.48
MRDD007	91.7	93.5	49.8	88.9	1.84	1.23	0.77	0.02	5.39
MRDD007	93.5	95.2	49.7	88.7	1.82	1.17	0.79	0.01	5.44
MRDD008	0	2	54.5	97.3	0.36	0.22	0.29	0.005	0.84

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
MRDD008	2	4	55.2	98.5	0.31	0.23	0.34	0.005	0.81
MRDD008	4	6	54.8	97.8	0.25	0.18	0.31	0.005	0.6
MRDD008	6	8.2	55	98.2	0.34	0.3	0.34	0.005	0.86
MRDD008	8.2	10	54.6	97.4	0.31	0.25	0.33	0.005	1.07
MRDD008	10	12	54.9	98	0.31	0.24	0.34	0.005	0.79
MRDD008	12	14	54.6	97.4	0.64	0.41	0.39	0.005	1.6
MRDD008	14	16.2	54.8	97.8	0.27	0.23	0.29	0.005	0.77
MRDD008	16.2	18.2	54.8	97.8	0.39	0.27	0.33	0.005	0.94
MRDD008	18.2	20	54.3	96.9	0.55	0.35	0.33	0.005	1.32
MRDD008	20	22	55	98.2	0.5	0.35	0.32	0.005	1.21
MRDD008	22	24	54.6	97.4	0.51	0.35	0.32	0.005	1.24
MRDD008	24	26	53.4	95.3	0.59	0.47	0.32	0.005	1.41
MRDD008	26	28	53.8	96	0.76	0.47	0.34	0.005	1.81
MRDD008	28	30	53.6	95.7	0.76	0.47	0.36	0.005	1.88
MRDD008	30	32.6	53.9	96.2	0.56	0.36	0.33	0.005	1.41
MRDD008	32.6	34	54.6	97.4	0.35	0.26	0.3	0.005	0.84
MRDD008	34	36.8	54.9	98	0.35	0.27	0.3	0.005	0.84
MRDD008	36.8	39	53.5	95.5	0.84	0.53	0.39	0.005	2.05
MRDD008	39	41	52.8	94.2	1.06	0.68	0.47	0.01	2.73
MRDD008	41	43	51.6	92.1	1.62	0.99	0.53	0.01	4.14
MRDD008	43	45	53.1	94.8	1	0.66	0.45	0.005	2.53

## Annexure B – Drill hole results – Lea Lea (13 Holes)

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
LDH01	0	0.9	51.3	91.5	1.42	0.91	0.48	0.01	3.46
LDH01	0.9	3	52.3	93.3	1.06	0.64	0.46	0.005	2.72
LDH01	3	5	52.8	94.2	0.81	0.55	0.39	0.005	2.11
LDH01	5	6.8	53.4	95.3	0.92	0.61	0.42	0.01	2.75
LDH01	6.8	8.5	51.8	92.4	1.17	0.74	0.45	0.01	3.53
LDH01	8.5	10.5	53.3	95.1	0.91	0.6	0.42	0.01	2.56
LDH01	10.5	12	51.9	92.6	1.12	0.67	0.44	0.01	3.16
LDH01	12	14	52.8	94.2	1.1	0.65	0.45	0.01	3.21
LDH01	14	16	51.6	92.1	1.27	0.74	0.48	0.01	3.53
LDH01	16	18	49.9	89.1	1.72	0.97	0.54	0.01	5.17
LDH01	18	19.4	52.3	93.3	0.92	0.7	0.42	0.01	2.81
LDH01	19.4	21.5	54.1	96.5	0.57	0.53	0.35	0.01	1.79
LDH01	21.5	23.5	54.2	96.7	0.6	0.57	0.34	0.01	1.79
LDH01	23.5	25.5	53.4	95.3	0.5	0.55	0.31	0.01	1.43
LDH01	25.5	27.5	50.8	90.7	1.36	1.17	0.52	0.03	3.83
LDH01	27.5	29.5	53.5	95.5	0.76	0.73	0.39	0.03	2.25
LDH01	29.5	31.2	51.5	91.9	1.04	1.23	0.49	0.03	3.18
LDH01	31.2	33.7	47.5	84.8	2.41	1.76	0.79	0.03	8.63
LDH01	33.7	35.5	53.1	94.8	0.56	0.49	0.55	0.02	1.73
LDH01	35.5	37	54.4	97.1	0.25	0.23	0.54	0.01	0.66
LDH01	37	39	51.4	91.7	0.91	0.6	1.06	0.02	2.59
LDH01	39	41.4	51.2	91.4	1.21	0.82	0.8	0.02	3.35
LDH01	41.4	43.4	54.3	96.9	0.36	0.29	0.45	0.01	0.85
LDH01	43.4	46	52.9	94.4	0.68	0.37	0.71	0.01	1.65
LDH01	46	48	52	92.8	0.88	0.54	1.16	0.02	2.14
LDH01	48	50	52.1	93	0.59	0.39	1.56	0.01	1.54
LDH01	50	51.8	49.6	88.5	0.76	0.46	3.25	0.005	2.03
LDH01	51.8	53.6	50.1	89.4	0.84	0.47	2.8	0.005	2.33
LDH01	53.6	54.5	44.7	79.8	1.91	1.04	5.72	0.01	5.25
LDH01	54.5	56	49.9	89.1	0.78	0.47	3.24	0.005	2.13
LDH01	56	58.1	50.8	90.7	0.65	0.38	2.44	0.005	1.69
LDH01	58.1	59.3	52.8	94.2	0.4	0.24	1.56	0.005	1.13
LDH01	59.3	60.5	53.2	94.9	0.22	0.13	1.12	0.005	0.61
LDH01	60.5	62.6	52.5	93.7	0.33	0.2	1.66	0.005	0.88
LDH01	62.6	65.1	52.7	94	0.42	0.25	1.56	0.005	1.1
LDH02	0	0.7	52.3	93.3	0.74	0.42	0.4	0.005	1.54
LDH02	0.7	3.1	54.3	96.9	0.35	0.28	0.34	0.005	0.98
LDH02	3.1	5	53.5	95.5	0.49	0.34	0.33	0.005	1.36
LDH02	5	6.9	53.2	94.9	0.42	0.34	0.33	0.005	1.82
LDH02	6.9	8.5	53.4	95.3	0.48	0.4	0.41	0.01	1.25
LDH02	8.5	10.1	53.8	96	0.39	0.3	0.36	0.005	1.21



Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
LDH02	10.1	12	54.8	97.8	0.37	0.31	0.42	0.01	1.09
LDH02	12	13.9	53	94.6	0.52	0.48	0.48	0.01	1.49
LDH02	13.9	16	52.3	93.3	0.85	0.71	0.52	0.01	2.36
LDH02	16	18.3	52.1	93	0.91	0.86	0.68	0.02	2.56
LDH02	18.3	20	49	87.4	1.95	1.49	0.82	0.03	5.72
LDH02	20	22	50.2	89.6	1.31	1.07	0.76	0.03	4.05
LDH02	22	24.3	52	92.8	0.88	0.69	0.73	0.02	2.65
LDH02	24.3	26	51.6	92.1	1.15	0.8	0.54	0.01	3.69
LDH02	26	28	50.8	90.7	1.32	0.88	0.6	0.01	4.56
LDH02	28	30	45.9	81.9	2.44	1.87	0.9	0.02	9.63
LDH02	30	31.8	41.3	73.7	3.73	2.59	1.24	0.03	15.12
LDH02	31.8	32.9	38.7	69.1	4.38	2.85	1.47	0.04	18.2
LDH02	32.9	35.5	46.9	83.7	2.4	1.67	1.26	0.02	9
LDH02	35.5	37.5	46.8	83.5	2.47	1.87	1.32	0.02	8.29
LDH02	37.5	40	50.9	90.8	1.02	0.76	0.81	0.01	3.28
LDH02	40	42	50.5	90.1	1.28	0.82	1.26	0.01	4.01
LDH02	42	44	51.9	92.6	0.87	0.55	0.86	0.01	3.04
LDH02	44	46	51.9	92.6	0.83	0.59	0.82	0.01	2.73
LDH02	46	48	52.7	94	0.38	0.39	0.98	0.005	1.47
LDH02	48	50	52.3	93.3	0.49	0.43	1.09	0.01	1.79
LDH02	50	52	51.8	92.4	0.57	0.53	1.22	0.01	1.92
LDH02	52	54	52	92.8	0.52	0.55	2.15	0.01	1.78
LDH02	54	56	50.1	89.4	0.9	0.88	1.93	0.02	2.85
LDH02	56	58	48.2	86	1.34	1.19	2.59	0.04	4.03
LDH02	58	60	49.3	88	1.11	0.92	2.62	0.03	3.51
LDH02	60	61.5	49.4	88.2	1.21	1.3	1.9	0.07	3.97
LDH02	61.5	63.6	48	85.7	1.4	2.03	1.75	0.06	4.48
LDH02	63.6	65.4	48.9	87.3	1.32	1.64	1.99	0.04	4.1
LDH02	65.4	67.5	48.5	86.6	1.54	1.77	1.95	0.04	4.91
LDH02	67.5	68.8	46.5	83	1.89	2.02	2.28	0.04	6.24
LDH02	68.8	71	47.4	84.6	1.43	1.5	2.37	0.04	4.87
LDH02	71	73	48.6	86.7	1.39	2	2.16	0.06	4.83
LDH02	73	75	44.6	79.6	1.98	2.97	2.6	0.1	7.22
LDH02	75	77	45.9	81.9	1.76	2.48	1.98	0.17	6.96
LDH02	77	79	44.5	79.4	2.25	2.86	2.01	0.09	9.66
LDH02	79	81.3	45.7	81.6	2.17	2.73	1.54	0.08	8.96
LDH02	81.3	82.1	37.9	67.6	4.71	3.17	1.59	0.05	17.33
LDH03	0	1.8	54.6	97.4	0.61	0.5	0.4	0.01	1.83
LDH03	1.8	3.8	54.7	97.6	0.43	0.36	0.36	0.01	1.09
LDH03	3.8	6	55.3	98.7	0.51	0.41	0.35	0.005	1.34
LDH03	6	7.7	55.1	98.3	0.57	0.46	0.35	0.01	1.44
LDH03	7.7	9.8	54.9	98	0.43	0.36	0.32	0.005	1.11

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
LDH03	9.8	11.7	54.4	97.1	0.68	0.53	0.4	0.01	1.75
LDH03	11.7	14	54	96.4	0.6	0.45	0.38	0.01	1.81
LDH03	14	15.3	53.4	95.3	0.78	0.5	0.4	0.01	3.06
LDH03	15.3	17.3	47.5	84.8	2.59	1.82	0.73	0.03	8.2
LDH03	17.3	19.5	29.4	52.5	8.34	5.26	2.03	0.07	26.97
LDH03	19.5	22	37.7	67.3	5.71	3.42	1.42	0.06	20.04
LDH03	22	25	50.5	90.1	1.67	1.37	0.74	0.03	5.79
LDH03	25	27	51.6	92.1	1.04	0.98	0.6	0.02	3.78
LDH03	27	29	49.5	88.3	1.64	1.47	0.73	0.02	5.82
LDH03	29	31	48.5	86.6	1.91	1.54	0.83	0.02	7.33
LDH03	31	33	49.7	88.7	1.44	1.21	0.7	0.02	5.94
LDH03	33	35	50	89.2	1.53	1.3	0.73	0.02	5.47
LDH03	35	37	49.5	88.3	1.58	1.16	0.8	0.02	5.65
LDH03	37	38.5	42	75	1.41	1.35	7.8	0.02	4.88
LDH03	38.5	39.8	34.2	61	1.69	1.37	13.8	0.02	5.48
LDH03	39.8	41.5	39.3	70.1	1.73	2.67	7.98	0.03	6.56
LDH03	41.5	43.3	39.3	70.1	2.21	2.89	6.99	0.05	9
LDH03	43.3	44.8	44.3	79.1	2.15	2.62	3.23	0.04	7.51
LDH03	44.8	46.5	36.9	65.9	1.76	2.01	10.8	0.03	6.03
LDH03	46.5	48.4	43.4	77.5	1.9	2.11	4.67	0.04	6.66
LDH03	48.4	50.5	45.6	81.4	1.98	1.98	2.75	0.04	6.5
LDH03	50.5	52.5	46.3	82.6	2.01	2.08	2.21	0.04	6.72
LDH03	52.5	54	47.4	84.6	1.65	1.67	2.3	0.03	5.57
LDH03	54	56	46.2	82.4	1.95	1.9	2.57	0.04	6.42
LDH03	56	58	43.7	78	2.68	2.29	3.4	0.04	8.19
LDH03	58	60	45.1	80.5	2.3	2.11	2.71	0.04	7.46
LDH03	60	62	45.5	81.2	2.01	1.57	2.61	0.04	6.96
LDH03	62	64	46.5	83	1.7	1.54	2.65	0.07	5.95
LDH03	64	66	46.9	83.7	1.49	2.44	2.03	0.22	5.32
LDH03	66	68	46.9	83.7	1.54	2.46	2.12	0.15	5.52
LDH03	68	70.1	47.3	84.4	1.4	2.33	1.96	0.21	5
LDH04	0	2	48.9	87.3	1.69	0.99	0.7	0.01	5.99
LDH04	2	4	51.1	91.2	1.09	0.7	0.62	0.01	3.9
LDH04	4	6	49.7	88.7	1.45	0.96	0.85	0.01	5.08
LDH04	6	8	50.4	89.9	1.22	0.86	0.78	0.01	4.19
LDH04	8	10	49.2	87.8	1.61	1.09	0.93	0.01	5.64
LDH04	10	12	48.1	85.8	1.81	1.2	1.04	0.01	6.65
LDH04	12	14	49.2	87.8	1.55	1.08	1.05	0.01	5.56
LDH04	14	16	48.3	86.2	1.62	1.17	1.24	0.01	5.8
LDH04	16	18	45	80.3	2.41	1.64	2.27	0.02	8.55
LDH04	18	20	42.9	76.6	3.24	2.1	1.88	0.02	11.49
LDH04	20	22	46.5	83	2.46	1.58	1.66	0.02	8.8

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
LDH04	22	24	46.3	82.6	1.97	1.26	1.94	0.01	7.07
LDH04	24	26	46	82.1	2.25	1.41	1.82	0.02	8.21
LDH04	26	28	46.3	82.6	2.05	1.34	1.96	0.02	7.28
LDH04	28	29.4	45.7	81.6	2.3	1.47	1.88	0.02	8.69
LDH04	29.4	30.8	40.1	71.6	3.82	2.44	2.25	0.03	14.54
LDH04	30.8	31.8	37.8	67.5	4.51	2.71	2.2	0.04	17.74
LDH04	31.8	34	44.5	79.4	2.41	1.52	2.15	0.02	9.29
LDH04	34	34.9	38.8	69.2	4.07	2.41	2.43	0.02	15.56
LDH04	34.9	37	43.3	77.3	2.42	1.55	2.89	0.02	9.11
LDH04	37	39	44.7	79.8	2.52	1.58	2.21	0.02	9.39
LDH04	39	41	47	83.9	1.46	0.9	2.27	0.01	5.48
LDH04	41	43.1	47	83.9	1.38	0.91	2.89	0.01	4.99
LDH04	43.1	45.2	48.5	86.6	1.09	0.79	2.38	0.01	4.02
LDH04	45.2	47.3	41.4	73.9	3.1	2	3.11	0.02	11.58
LDH04	47.3	49	39.7	70.8	2.32	1.4	2.38	0.02	18.58
LDH04	49	51	37.6	67.1	2.03	1.02	1.69	0.03	24
LDH04	51	53	39	69.6	2.37	1.22	2.07	0.03	20.61
LDH04	53	55	40.5	72.3	2.37	1.23	2.16	0.03	17.42
LDH04	55	57	37.6	67.1	2.4	1.09	1.62	0.03	23.82
LDH04	57	59	38.8	69.2	2.2	0.93	1.62	0.02	21.88
LDH04	59	61	38.6	68.9	2.43	1.11	1.86	0.02	21.24
LDH04	61	63	38.3	68.4	2.45	1.21	1.86	0.03	21.61
LDH04	63	65	39	69.6	2.5	1.34	1.9	0.03	19.94
LDH04	65	66.7	39.8	71	2.63	1.41	1.76	0.03	19.99
LDH04	66.7	69	47.2	84.2	1.51	0.98	1.84	0.02	6.95
LDH04	69	71.1	48.1	85.8	1.49	1.1	2.08	0.02	5.34
LDH04	71.1	71.6	48.2	86	1.79	1.06	1.55	0.02	5.58
LDH05	0	2.4	52.1	93	0.94	0.54	0.6	0.01	2.52
LDH05	2.4	4.5	53.3	95.1	0.46	0.31	0.53	0.01	1.25
LDH05	4.5	6.5	54.3	96.9	0.23	0.17	0.43	0.005	0.65
LDH05	6.5	8.5	54.7	97.6	0.25	0.17	0.44	0.005	0.75
LDH05	8.5	10.5	54.1	96.5	0.23	0.14	0.39	0.005	0.61
LDH05	10.5	12.5	54.8	97.8	0.32	0.21	0.46	0.005	0.87
LDH05	12.5	14.5	54.1	96.5	0.55	0.34	0.51	0.01	1.43
LDH05	14.5	16.5	54.5	97.3	0.32	0.19	0.41	0.005	0.86
LDH05	16.5	18.5	54	96.4	0.33	0.2	0.39	0.005	0.84
LDH05	18.5	20.5	54.7	97.6	0.36	0.21	0.42	0.005	0.89
LDH05	20.5	21.4	53.1	94.8	0.61	0.37	0.44	0.005	1.6
LDH05	21.4	23.2	45.8	81.7	2.86	1.74	0.81	0.02	9.56
LDH05	23.2	25.3	13.25	23.6	13.66	6.43	2.42	0.07	45.35
LDH05	25.3	27.6	14.5	25.9	13.66	6.28	2.35	0.07	42.37
LDH05	27.6	29.9	50.4	89.9	1.41	1.01	1.24	0.02	4.53

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
LDH05	29.9	31.8	50.9	90.8	0.99	0.68	1.77	0.01	3.07
LDH05	31.8	34.1	48	85.7	1.82	0.89	2.36	0.01	5.88
LDH05	34.1	36	50.3	89.8	0.92	0.63	1.81	0.01	2.86
LDH05	36	38	50.8	90.7	0.99	0.65	1.93	0.01	3.16
LDH05	38	39.6	50.1	89.4	0.86	0.63	1.86	0.01	2.85
LDH05	39.6	41.7	51.1	91.2	0.66	0.41	1.77	0.005	2.02
LDH05	41.7	44	50.1	89.4	0.89	0.53	1.97	0.01	2.79
LDH05	44	46	50.4	89.9	0.79	0.51	1.92	0.01	2.59
LDH05	46	48.2	46.2	82.4	1.68	1.31	3.1	0.03	5.56
LDH05	48.2	50	17.7	31.6	11.99	5.72	2.78	0.06	39.61
LDH05	50	52.1	20.8	37.1	10.61	4.9	2.6	0.06	36.24
LDH05	52.1	54	25.4	45.3	9.15	4.37	2.25	0.06	32.81
LDH05	54	56	19.55	34.9	11	5.38	2.54	0.06	39.44
LDH05	56	58	20	35.7	10.54	5.28	2.56	0.06	38.78
LDH05	58	60	21	37.5	9.96	4.87	2.36	0.05	36.76
LDH05	60	62	21.3	38	9.9	5.13	2.41	0.05	36.21
LDH05	62	63.7	24.9	44.4	8.8	4.39	2.26	0.05	32.47
LDH05	63.7	65.2	29.1	51.9	7.48	3.8	1.9	0.04	28.24
LDH05	65.2	66.9	27.8	49.6	8	4.15	1.92	0.04	29.78
LDH06	0	2	53.5	95.5	0.4	0.25	0.48	0.005	0.98
LDH06	2	4	53.2	94.9	0.48	0.29	0.47	0.005	1.24
LDH06	4	6	50.5	90.1	0.41	0.25	0.46	0.005	1.06
LDH06	6	8	53	94.6	0.61	0.35	0.54	0.01	1.59
LDH06	8	10	53.4	95.3	0.71	0.42	0.6	0.01	1.9
LDH06	10	12	52.6	93.9	0.71	0.41	0.57	0.005	1.92
LDH06	12	14	52	92.8	0.75	0.42	0.86	0.005	2.09
LDH06	14	16	50.5	90.1	0.78	0.43	2.03	0.01	2.2
LDH06	16	18	49.9	89.1	0.98	0.54	2.31	0.01	3.15
LDH06	18	20	50.6	90.3	0.8	0.47	2.06	0.01	2.29
LDH06	20	22	52.1	93	0.58	0.34	1.2	0.01	1.63
LDH06	22	24	53.8	96	0.24	0.17	0.79	0.01	0.72
LDH06	24	26	53.7	95.8	0.22	0.15	0.68	0.005	0.67
LDH06	26	28	53.7	95.8	0.21	0.15	0.98	0.005	0.63
LDH06	28	30.5	51.8	92.4	0.19	0.12	2.5	0.005	0.51
LDH06	30.5	31.1	49.1	87.6	1.07	0.57	2.53	0.01	3.27
LDH06	31.1	33	46.9	83.7	2.4	1.26	2	0.02	7.46
LDH06	33	34.4	44.5	79.4	2.88	1.68	1.32	0.04	9.74
LDH06	34.4	35.7	9.55	17.05	15.04	7.22	3.2	0.06	46.76
LDH06	35.7	38	18.55	33.1	11.8	5.39	2.54	0.06	39.86
LDH06	38	40	16.65	29.7	12.22	5.51	2.52	0.06	41.76
LDH07	0	1.6	52.2	93.2	0.84	0.61	0.55	0.005	2.23
LDH07	1.6	3.3	54	96.4	0.49	0.35	0.48	0.01	1.37

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
LDH07	3.3	4.3	54.2	96.7	0.36	0.36	0.48	0.01	1.06
LDH07	4.3	6	53.3	95.1	0.39	0.49	0.49	0.005	1.06
LDH07	6	8	55.1	98.3	0.19	0.27	0.4	0.005	0.49
LDH07	8	10	54.2	96.7	0.14	0.17	0.37	0.005	0.33
LDH07	10	11.3	54	96.4	0.17	0.3	0.36	0.005	0.4
LDH07	11.3	13	53.8	96	0.3	0.25	0.44	0.005	0.7
LDH07	13	15	54.1	96.5	0.23	0.2	0.36	0.005	0.51
LDH07	15	17	54.8	97.8	0.32	0.22	0.37	0.005	0.75
LDH07	17	19	54.8	97.8	0.35	0.24	0.42	0.01	0.87
LDH07	19	21	53.9	96.2	0.35	0.27	0.42	0.01	0.88
LDH07	21	22	53.6	95.7	0.46	0.28	0.43	0.01	1.16
LDH07	22	24	53.5	95.5	0.5	0.36	0.43	0.01	1.28
LDH07	24	26	54.5	97.3	0.47	0.33	0.41	0.01	1.18
LDH07	26	28	54.3	96.9	0.83	0.54	0.53	0.01	1.9
LDH07	28	30	53.5	95.5	0.81	0.55	0.61	0.01	2.2
LDH07	30	32	52.9	94.4	0.72	0.49	0.69	0.01	2.01
LDH07	32	34	53.5	95.5	0.78	0.51	0.69	0.01	2.22
LDH07	34	36	53.7	95.8	0.79	0.53	0.5	0.01	2.3
LDH07	36	38	53.3	95.1	0.96	0.66	0.53	0.01	2.81
LDH07	38	39.9	53.5	95.5	0.54	0.35	0.43	0.01	1.53
LDH07	39.9	42	52.4	93.5	0.84	0.56	0.5	0.01	2.53
LDH07	42	44	53.5	95.5	0.46	0.32	0.4	0.01	1.25
LDH07	44	45.7	53.5	95.5	0.52	0.33	0.46	0.01	1.42
LDH07	45.7	47.3	54.6	97.4	0.37	0.26	0.39	0.01	1.02
LDH07	47.3	49.2	54.2	96.7	0.36	0.23	0.36	0.005	0.93
LDH07	49.2	51	55	98.2	0.31	0.2	0.38	0.01	0.76
LDH07	51	53	54.9	98	0.3	0.19	0.38	0.01	0.75
LDH07	53	55.2	54.1	96.5	0.33	0.2	0.38	0.005	0.82
LDH07	55.2	57	54.4	97.1	0.18	0.13	0.34	0.005	0.47
LDH07	57	59	54.4	97.1	0.2	0.13	0.35	0.005	0.48
LDH07	59	61	54	96.4	0.28	0.19	0.36	0.01	0.71
LDH07	61	62.8	54	96.4	0.29	0.22	0.36	0.01	0.75
LDH07	62.8	64.7	53.6	95.7	0.56	0.42	0.57	0.03	1.54
LDH07	64.7	67	54.3	96.9	0.28	0.19	0.35	0.01	0.78
LDH07	67	69.5	55.1	98.3	0.29	0.19	0.39	0.005	0.78
LDH07	69.5	72	54.4	97.1	0.4	0.26	0.38	0.005	1.13
LDH07	72	73.9	53.2	94.9	0.57	0.35	0.47	0.005	1.7
LDH07	73.9	76	51.7	92.3	0.88	0.53	0.83	0.005	2.86
LDH07	76	77.8	52.9	94.4	0.8	0.49	0.74	0.01	2.66
LDH07	77.8	79.5	51.5	91.9	1.23	0.75	0.85	0.01	3.98
LDH07	79.5	82.4	51.1	91.2	1.11	0.67	0.82	0.01	3.5
LDH07	82.4	84	47.9	85.5	1.28	0.74	2.86	0.01	4.24

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
LDH07	84	86	48	85.7	1.32	0.78	2.82	0.01	4.42
LDH07	86	88	47.1	84.1	1.52	0.9	3.02	0.01	5.17
LDH07	88	89.8	48.7	86.9	1.33	0.8	2.53	0.01	4.49
LDH07	89.8	92.2	48.2	86	1.43	0.85	2.48	0.01	4.69
LDH07	92.2	94.4	48.3	86.2	1.44	0.85	3.14	0.01	4.69
LDH07	94.4	96	49.6	88.5	0.83	0.49	2.71	0.01	2.71
LDH07	96	98	48.9	87.3	1.11	0.66	3.28	0.01	3.57
LDH07	98	100	47.9	85.5	1.14	0.67	3.27	0.01	3.71
LDH07	100	102	48.2	86	1.31	0.77	3.32	0.01	4.4
LDH07	102	104	50.1	89.4	0.91	0.55	2.46	0.01	3.03
LDH07	104	106	47.9	85.5	1.29	0.75	2.89	0.01	4.16
LDH07	106	107.7	51.2	91.4	0.67	0.41	1.58	0.01	2.26
LDH07	107.7	110	49.1	87.6	1.09	0.68	2.96	0.01	3.84
LDH07	110	112	48.4	86.4	1.12	0.72	3.13	0.01	4.18
LDH07	112	114	46.2	82.4	1.48	0.86	3.41	0.01	5.74
LDH07	114	116	46.7	83.3	1.38	0.81	3.02	0.01	5.47
LDH07	116	118	46.3	82.6	1.48	0.85	3.14	0.01	5.91
LDH07	118	120	45.2	80.7	1.92	1.15	2.9	0.01	7.24
LDH07	120	122	48.7	86.9	1.34	0.81	2.25	0.01	5.05
LDH07	122	124.3	48.6	86.7	1.45	0.9	1.7	0.02	5.1
LDH07	124.3	126.2	17.05	30.4	11.76	6.7	3.16	0.11	40.82
LDH07	126.2	128	8.74	15.6	13.48	7.99	4.14	0.11	49.68
LDH07	128	130	8.17	14.6	13.48	8.43	4.41	0.11	50.15
LDH08	0	2.2	52	92.8	1.45	0.75	0.52	0.01	3.26
LDH08	2.2	4.3	54.9	98	0.35	0.26	0.35	0.005	0.81
LDH08	4.3	6	44.1	78.7	5.25	2.45	0.55	0.03	11
LDH08	6	7.8	48.4	86.4	3.11	1.55	0.47	0.02	6.74
LDH08	7.8	10	55	98.2	0.31	0.21	0.33	0.005	0.72
LDH08	10	12	53.7	95.8	0.85	0.5	0.48	0.01	2
LDH08	12	14	54.5	97.3	0.54	0.36	0.44	0.005	1.26
LDH08	14	16	54.2	96.7	0.59	0.33	0.63	0.005	1.43
LDH08	16	18	52.3	93.3	0.87	0.54	1.53	0.005	2.65
LDH08	18	20	50.5	90.1	1.06	0.68	2.53	0.01	3.47
LDH08	20	22	51.2	91.4	0.91	0.63	2.16	0.005	2.69
LDH08	22	23.5	47.9	85.5	1.48	0.91	3.53	0.01	4.61
LDH08	23.5	25	47.1	84.1	1.75	1.09	3.8	0.01	5.54
LDH08	25	26.5	50.3	89.8	0.82	0.54	2.59	0.01	3.35
LDH08	26.5	28	50.1	89.4	0.91	0.63	2.41	0.01	3.82
LDH08	28	30	50.9	90.8	0.88	0.6	1.86	0.01	3.65
LDH08	30	32	49.6	88.5	1.1	0.77	2.05	0.01	4.41
LDH08	32	33.5	50	89.2	1.07	0.73	2.04	0.01	4.21
LDH08	33.5	35.2	51.2	91.4	0.82	0.55	1.72	0.005	3.25

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
LDH08	35.2	37	52.4	93.5	0.61	0.41	1.88	0.01	2.17
LDH08	37	39	50.3	89.8	0.83	0.53	2.65	0.01	3.07
LDH08	39	41	48.6	86.7	1.16	0.73	3.3	0.01	4.21
LDH08	41	43	47.6	84.9	1.45	0.91	3.63	0.01	5.08
LDH08	43	45	48.8	87.1	1.17	0.73	3.34	0.01	3.85
LDH08	45	47	49.5	88.3	1.06	0.67	3.07	0.01	3.48
LDH08	47	48.5	48.9	87.3	1.27	0.78	3.08	0.01	4.23
LDH08	48.5	50.5	48.6	86.7	1.47	0.9	2.89	0.01	4.72
LDH08	50.5	52.5	49.6	88.5	1.17	0.69	1.84	0.01	3.73
LDH08	52.5	54.2	49.1	87.6	1.42	0.89	2.5	0.01	4.71
LDH08	54.2	56.2	49.6	88.5	0.68	0.43	3.58	0.005	2.41
LDH08	56.2	58.2	50.5	90.1	0.58	0.37	2.97	0.005	2.13
LDH08	58.2	59.8	49.8	88.9	0.77	0.53	3.16	0.005	2.65
LDH08	59.8	61.2	50.1	89.4	0.86	0.56	2.84	0.005	3.01
LDH09	0	2.3	54.6	97.4	0.47	0.27	0.34	0.02	1.26
LDH09	2.3	4.5	55.1	98.3	0.47	0.29	0.35	0.02	1.04
LDH09	4.5	6.2	54.4	97.1	0.69	0.39	0.37	0.02	1.52
LDH09	6.2	8.2	54.7	97.6	0.42	0.25	0.42	0.01	0.97
LDH09	8.2	10.5	54.3	96.9	0.55	0.33	0.42	0.01	1.26
LDH09	10.5	12	54.3	96.9	0.56	0.32	0.41	0.01	1.31
LDH09	12	14	54.2	96.7	0.6	0.34	0.39	0.01	1.39
LDH09	14	16	54.5	97.3	0.49	0.33	0.37	0.02	1.09
LDH09	16	18	54.9	98	0.38	0.23	0.35	0.01	0.84
LDH09	18	20	54.7	97.6	0.43	0.25	0.35	0.01	0.95
LDH09	20	22	54.5	97.3	0.42	0.26	0.37	0.01	0.92
LDH09	22	24	55.3	98.7	0.43	0.29	0.35	0.01	0.91
LDH09	24	26	55.3	98.7	0.32	0.22	0.34	0.01	0.68
LDH09	26	28	54.7	97.6	0.35	0.22	0.35	0.01	0.74
LDH09	28	30	55	98.2	0.29	0.2	0.35	0.005	0.63
LDH09	30	31.9	54.9	98	0.27	0.16	0.37	0.005	0.57
LDH09	31.9	33.9	55.1	98.3	0.22	0.14	0.35	0.005	0.5
LDH09	33.9	35.9	54.7	97.6	0.16	0.12	0.32	0.005	0.35
LDH09	35.9	38	54.9	98	0.34	0.19	0.38	0.005	0.76
LDH09	38	40	54.9	98	0.22	0.19	0.36	0.005	0.48
LDH09	40	41.6	54.3	96.9	0.43	0.35	0.43	0.005	0.91
LDH09	41.6	43.3	54.4	97.1	0.5	0.31	0.42	0.01	1.14
LDH09	43.3	45.3	54	96.4	0.61	0.48	0.45	0.01	1.35
LDH09	45.3	47	55	98.2	0.39	0.26	0.42	0.01	0.92
LDH09	47	48.7	52.3	93.3	1.18	0.8	0.74	0.02	3.07
LDH09	48.7	51	53.1	94.8	0.83	0.51	0.68	0.01	2.25
LDH09	51	53	52.5	93.7	0.72	0.42	1.3	0.005	2.2
LDH09	53	55	50.8	90.7	0.87	0.51	2.75	0.005	2.75

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
LDH09	55	57	50.3	89.8	0.99	0.56	2.43	0.005	3.08
LDH09	57	59	51.9	92.6	0.81	0.47	1.54	0.005	2.46
LDH09	59	61	53.2	94.9	0.72	0.41	0.61	0.005	2.16
LDH09	61	63	53.4	95.3	0.66	0.39	0.59	0.01	2
LDH09	63	65	53.5	95.5	0.71	0.43	0.71	0.02	2.15
LDH09	65	67	53.9	96.2	0.6	0.38	0.55	0.01	1.69
LDH09	67	69	53.1	94.8	0.82	0.56	0.59	0.02	2.26
LDH09	69	71	53.6	95.7	0.8	0.5	0.54	0.01	2.33
LDH09	71	73	53	94.6	0.85	0.52	0.54	0.01	2.48
LDH09	73	75	54	96.4	0.55	0.32	0.44	0.01	1.45
LDH09	75	77	54.1	96.5	0.45	0.26	0.41	0.01	1.19
LDH09	77	79	54.5	97.3	0.34	0.21	0.4	0.005	0.91
LDH09	79	81	54.1	96.5	0.56	0.35	0.65	0.01	1.62
LDH09	81	83	53.8	96	0.64	0.39	0.52	0.01	1.78
LDH09	83	85	53.8	96	0.72	0.43	0.5	0.01	2.04
LDH09	85	87	53.2	94.9	0.69	0.41	0.62	0.01	1.96
LDH09	87	89	52.2	93.2	0.82	0.51	0.94	0.01	2.62
LDH09	89	91	54.6	97.4	0.56	0.36	0.55	0.01	1.66
LDH09	91	93	53.3	95.1	0.56	0.37	0.83	0.01	1.7
LDH09	93	95	53.3	95.1	0.45	0.26	0.89	0.01	1.55
LDH09	95	97	53.8	96	0.45	0.27	0.61	0.005	1.33
LDH09	97	99	50	89.2	0.93	0.55	2.71	0.005	2.88
LDH09	99	101	50.5	90.1	0.64	0.38	3.31	0.01	2.07
LDH09	101	103	49.7	88.7	0.76	0.43	3.53	0.005	2.45
LDH09	103	104.9	48.5	86.6	1.27	0.74	3.13	0.005	4.2
LDH09	104.9	107	48.8	87.1	1.02	0.6	2.98	0.005	3.36
LDH09	107	108.7	47.3	84.4	0.75	0.42	2.65	0.005	2.5
LDH09	108.7	111	48.4	86.4	1.18	0.68	3.19	0.005	4
LDH09	111	113	47.3	84.4	1.49	0.85	3.4	0.01	5.13
LDH09	113	114.5	46.7	83.3	1.54	0.92	3.74	0.01	5.41
LDH09	114.5	116	49.5	88.3	0.79	0.48	3.05	0.005	2.81
LDH09	116	118	48.2	86	1.03	0.62	3.53	0.005	3.71
LDH09	118	120.1	45.8	81.7	1.73	1.01	3.6	0.01	6.25
LDH09	120.1	122	44.8	80	2.31	1.28	3.44	0.01	7.63
LDH09	122	124	46	82.1	2.14	1.2	3.41	0.01	7.14
LDH09	124	126	48.3	86.2	1.43	0.8	2.74	0.01	4.76
LDH09	126	128	46.3	82.6	1.82	1.02	3.33	0.01	5.98
LDH09	128	129.6	47.1	84.1	1.38	0.78	4.01	0.01	4.42
LDH09	129.6	131.2	51.1	91.2	0.75	0.43	2.94	0.01	2.34
LDH09	131.2	133.2	48.9	87.3	0.77	0.45	3.79	0.005	2.35
LDH09	133.2	135	50.2	89.6	0.62	0.36	3.26	0.01	1.94
LDH09	135	137	50.2	89.6	0.77	0.42	2.65	0.005	2.36



Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
LDH09	137	139	50.5	90.1	0.76	0.43	2.69	0.01	2.32
LDH09	139	141	52.5	93.7	0.58	0.34	1.92	0.01	1.78
LDH09	141	142.4	50	89.2	0.92	0.5	2.91	0.01	2.82
LDH09	142.4	143.7	53.7	95.8	0.3	0.17	1.24	0.005	0.89
LDH09	143.7	145	51.8	92.4	0.38	0.23	2.9	0.005	1.09
LDH09	145	147	51.5	91.9	0.29	0.19	3.55	0.005	0.72
LDH09	147	149	52.8	94.2	0.23	0.16	2.39	0.005	0.59
LDH09	149	151.3	52.1	93	0.23	0.17	2.8	0.005	0.57
LDH10	0	2	45.1	80.5	3.23	3.13	0.88	0.02	9.14
LDH10	2	3.9	47.6	84.9	2.35	1.82	0.78	0.02	7.52
LDH10	3.9	5.6	44.3	79.1	3.35	2.66	0.93	0.03	10.19
LDH10	5.6	7.3	50.5	90.1	1.4	1.19	0.6	0.02	4.54
LDH10	7.3	9	50.4	89.9	1.4	1.01	0.72	0.01	4.63
LDH10	9	10.8	49.3	88	1.62	1.18	0.77	0.01	5.36
LDH10	10.8	12.5	47.5	84.8	2.06	1.76	0.83	0.01	6.6
LDH10	12.5	14.8	47.6	84.9	2.29	1.55	0.91	0.01	7.55
LDH10	14.8	17.1	46	82.1	2.73	1.94	0.86	0.02	9.06
LDH10	17.1	19.6	52.3	93.3	0.76	0.55	0.55	0.005	2.45
LDH10	19.6	22	51.4	91.7	0.89	0.84	0.48	0.01	3.19
LDH10	22	24	52.3	93.3	0.63	0.75	0.55	0.01	2.19
LDH10	24	26.3	53.3	95.1	0.7	0.54	0.56	0.01	2.29
LDH10	26.3	28.4	53.9	96.2	0.41	0.34	0.41	0.01	1.11
LDH10	28.4	30	52.1	93	0.85	0.68	0.5	0.01	2.35
LDH10	30	32	51.2	91.4	1.15	0.85	0.55	0.01	3.26
LDH10	32	34	52.3	93.3	0.65	0.54	0.46	0.01	1.8
LDH10	34	36	53.5	95.5	0.48	0.42	0.43	0.01	1.36
LDH10	36	38	52.5	93.7	0.68	0.55	0.49	0.01	2.16
LDH10	38	40	51.7	92.3	0.94	0.67	0.6	0.01	3.09
LDH10	40	42	51.9	92.6	0.82	0.68	0.66	0.01	2.38
LDH10	42	44.1	52.2	93.2	0.69	0.54	0.66	0.01	2
LDH10	44.1	46.1	53.6	95.7	0.57	0.37	0.68	0.01	1.68
LDH10	46.1	48	53.7	95.8	0.37	0.26	0.6	0.01	1.15
LDH10	48	50	53.5	95.5	0.37	0.29	0.56	0.005	1.04
LDH10	50	52	52.9	94.4	0.63	0.33	0.61	0.005	1.71
LDH10	52	54	52.3	93.3	0.77	0.37	0.57	0.005	2.25
LDH10	54	55.3	52.3	93.3	0.61	0.3	0.52	0.005	2.04
LDH10	55.3	57	53.3	95.1	0.35	0.23	0.52	0.01	2.16
LDH10	57	59	52.1	93	0.45	0.28	0.53	0.01	2.77
LDH10	59	61	52.5	93.7	0.43	0.31	0.64	0.01	2.16
LDH10	61	63	52.9	94.4	0.34	0.25	0.54	0.005	1.61
LDH10	63	64.5	51.5	91.9	0.69	0.4	0.93	0.005	3
LDH10	64.5	66.5	49.6	88.5	0.89	0.58	1.94	0.01	3.83

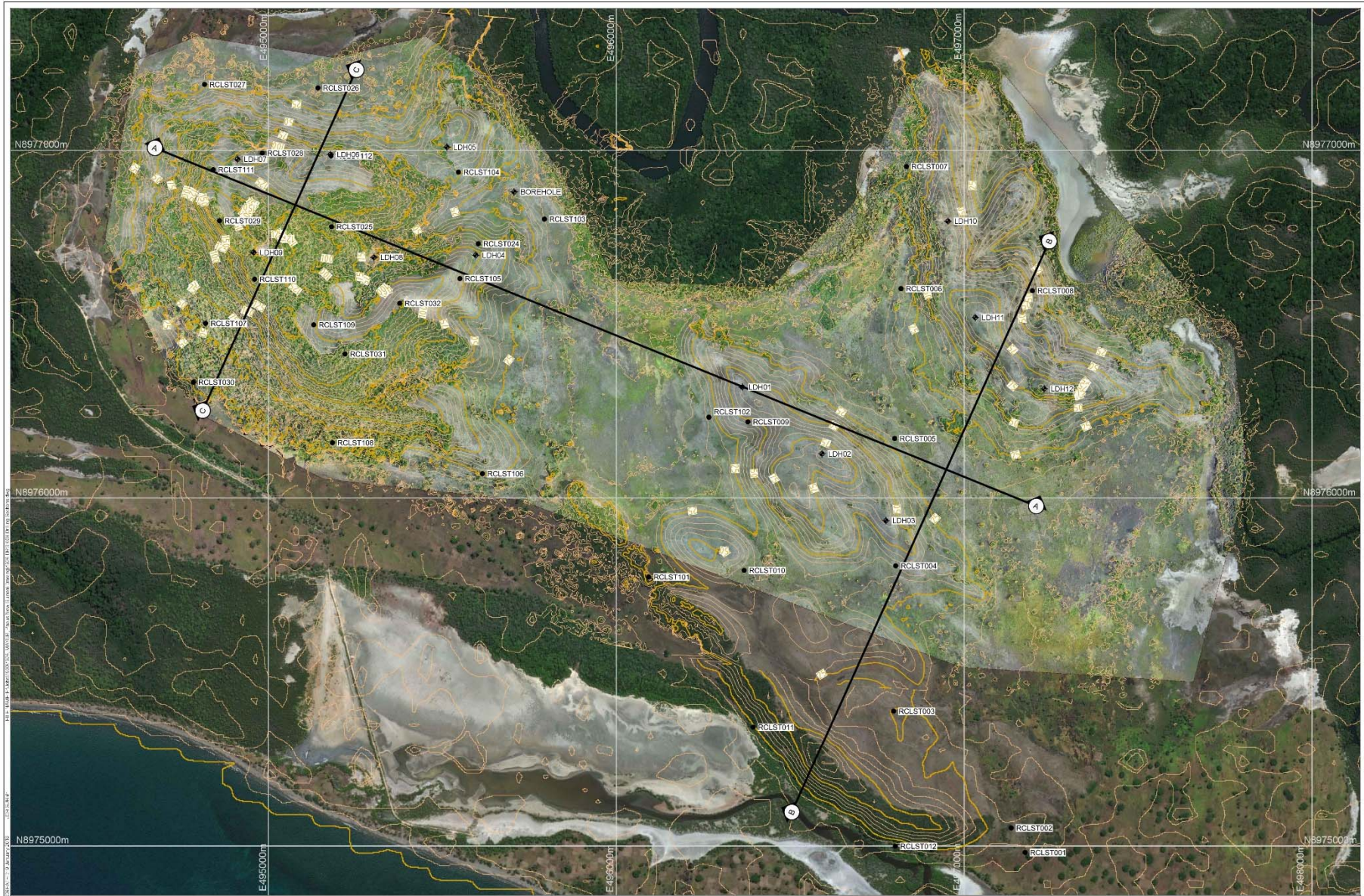
Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
LDH10	66.5	68	42.7	76.2	2.83	1.53	3.16	0.02	10.5
LDH10	68	70	48.7	86.9	1.56	1.07	1.22	0.02	6.02
LDH10	70	72.1	45.8	81.7	2.37	1.69	1.6	0.04	9.28
LDH10	72.1	73.2	34.7	61.9	5.35	3.5	1.84	0.04	21.11
LDH10	73.2	74.8	31.4	56	6.35	4.07	1.98	0.04	25.01
LDH11	0	3.2	54.5	97.3	0.52	0.31	0.49	0.005	1.37
LDH11	3.2	4.6	53.5	95.5	0.29	0.18	0.56	0.005	0.76
LDH11	4.6	6.6	54	96.4	0.45	0.3	0.55	0.005	1.27
LDH11	6.6	8.7	54.4	97.1	0.5	0.35	0.51	0.005	1.29
LDH11	8.7	11	54.8	97.8	0.35	0.36	0.49	0.005	0.93
LDH11	11	13	54.8	97.8	0.33	0.29	0.49	0.005	0.88
LDH11	13	15.1	54.8	97.8	0.38	0.32	0.48	0.005	0.91
LDH11	15.1	17	54.4	97.1	0.55	0.42	0.52	0.01	1.34
LDH11	17	19	54.4	97.1	0.58	0.46	0.49	0.005	1.44
LDH11	19	21	54.2	96.7	0.54	0.46	0.54	0.01	1.41
LDH11	21	22.3	54	96.4	0.67	0.5	0.55	0.005	1.74
LDH11	22.3	24	54.7	97.6	0.36	0.35	0.45	0.005	0.89
LDH11	24	26.2	53.7	95.8	0.73	0.67	0.52	0.02	2.05
LDH11	26.2	28	53.2	94.9	0.83	0.75	0.56	0.01	2.67
LDH11	28	30	54.6	97.4	0.4	0.38	0.49	0.01	1.04
LDH11	30	32	54.2	96.7	0.6	0.44	0.57	0.02	1.48
LDH11	32	34	54	96.4	0.7	0.55	0.61	0.02	1.72
LDH11	34	36	53.4	95.3	0.86	0.62	0.62	0.02	2.21
LDH11	36	38	53.9	96.2	0.6	0.44	0.56	0.02	1.48
LDH11	38	40.2	54.1	96.5	0.7	0.49	0.57	0.02	1.76
LDH11	40.2	42	54.2	96.7	0.6	0.43	0.54	0.01	1.57
LDH11	42	44	53.6	95.7	0.81	0.46	0.61	0.02	2.25
LDH11	44	46	54	96.4	0.64	0.45	0.54	0.01	1.9
LDH11	46	47.5	54.9	98	0.34	0.27	0.48	0.01	0.91
LDH11	47.5	49.2	54.7	97.6	0.46	0.3	0.45	0.01	1.33
LDH11	49.2	51	52.2	93.2	1.2	0.73	0.5	0.01	3.75
LDH11	51	53	52.2	93.2	1.22	0.73	0.55	0.005	4
LDH11	53	55	51.1	91.2	1.14	0.7	1.62	0.01	3.94
LDH11	55	57	47.9	85.5	1.61	0.94	3.21	0.01	5.85
LDH11	57	59	51.6	92.1	1.36	0.81	0.67	0.005	4.99
LDH11	59	60.7	52.8	94.2	0.85	0.51	0.52	0.005	3.52
LDH11	60.7	61.9	56.1	100	0.02	0.03	0.12	0.005	0.09
LDH11	61.9	64	49.6	88.5	1.93	1.07	0.72	0.01	6.78
LDH11	64	66.1	50.8	90.7	1.52	0.94	0.59	0.01	5.47
LDH11	66.1	68	48.4	86.4	2.14	1.46	0.61	0.03	8.12
LDH11	68	70	46.8	83.5	2.58	1.91	0.75	0.03	9.53
LDH11	70	72	37.2	66.4	5.46	3.34	1.12	0.04	20.37

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
LDH11	72	73.5	45.2	80.7	3.09	2.51	0.78	0.05	11.47
LDH11	73.5	75.4	34.9	62.3	5.91	3.85	1.29	0.05	23.68
LDH11	75.4	77.4	47.5	84.8	2.07	1.26	1.02	0.01	9.34
LDH11	77.4	79.2	46.5	83	2.35	1.22	1.14	0.02	10.78
LDH11	79.2	81	11.9	21.2	13.16	6.58	2.93	0.06	47.11
LDH11	81	83	11.6	20.7	13.16	6.69	3	0.06	47.5
LDH11	83	85.1	11.1	19.8	13.14	6.56	3.25	0.06	47.59
LDH12	0	1.4	51.5	91.9	1.21	0.64	0.61	0.02	3.17
LDH12	1.4	3.5	52.5	93.7	0.69	0.42	0.67	0.01	1.79
LDH12	3.5	5.5	51.9	92.6	0.93	0.51	0.68	0.03	2.42
LDH12	5.5	7.5	52.1	93	0.88	0.53	0.61	0.02	2.21
LDH12	7.5	9.4	52.3	93.3	0.77	0.45	0.62	0.02	1.89
LDH12	9.4	11.6	53.1	94.8	0.75	0.43	0.6	0.01	1.79
LDH12	11.6	13.3	53.2	94.9	0.51	0.29	0.43	0.01	1.2
LDH12	13.3	15	54.5	97.3	0.49	0.28	0.42	0.01	1.16
LDH12	15	16.5	54.4	97.1	0.5	0.28	0.41	0.01	1.28
LDH12	16.5	17.7	54.3	96.9	0.44	0.24	0.45	0.01	1.01
LDH12	17.7	19.5	53.5	95.5	0.46	0.31	0.48	0.01	1.04
LDH12	19.5	21.5	53.9	96.2	0.66	0.36	0.45	0.01	1.52
LDH12	21.5	23.5	53.9	96.2	0.31	0.23	0.34	0.01	0.69
LDH12	23.5	25.5	53.6	95.7	0.47	0.26	0.41	0.02	1.02
LDH12	25.5	27	53.4	95.3	0.47	0.25	0.42	0.01	1.03
LDH12	27	29	54.4	97.1	0.43	0.24	0.41	0.01	0.91
LDH12	29	31	53.8	96	0.3	0.2	0.4	0.01	0.66
LDH12	31	33	54.7	97.6	0.32	0.2	0.47	0.01	0.73
LDH12	33	35	54.2	96.7	0.46	0.23	0.52	0.01	1.02
LDH12	35	37	54.5	97.3	0.28	0.17	0.4	0.01	0.64
LDH12	37	39	53.8	96	0.37	0.2	0.43	0.01	0.86
LDH12	39	41	54.5	97.3	0.35	0.23	0.5	0.01	0.81
LDH12	41	43	53.6	95.7	0.28	0.18	0.62	0.01	0.67
LDH12	43	45	53.7	95.8	0.38	0.23	0.5	0.01	0.84
LDH12	45	47.4	53.8	96	0.28	0.15	0.46	0.01	0.66
LDH12	47.4	49.4	53	94.6	0.28	0.2	1.13	0.01	0.68
LDH12	49.4	50.8	51.4	91.7	0.44	0.23	2.29	0.005	0.92
LDH12	50.8	52.4	52.3	93.3	0.42	0.2	2.25	0.01	0.84
LDH12	52.4	53.9	53.5	95.5	0.3	0.27	0.59	0.005	0.71
LDH12	53.9	55.7	54.4	97.1	0.27	0.18	0.89	0.005	0.64
LDH12	55.7	57.5	53.6	95.7	0.37	0.21	0.59	0.005	0.86
LDH12	57.5	58.7	54.3	96.9	0.28	0.17	0.73	0.01	0.69
LDH12	58.7	59.8	52.2	93.2	0.67	0.31	1.1	0.01	1.57
LDH12	59.8	61.5	52.8	94.2	0.46	0.23	1.03	0.01	1.08
LDH12	61.5	63	53.6	95.7	0.36	0.2	1.11	0.01	0.85

Hole_No	From	To	CaO	CaCO3	Al2O3	Fe2O3	MgO	MnO	SiO2
LDH12	63	64.5	52.4	93.5	0.53	0.26	1.09	0.01	1.26
LDH12	64.5	66.6	53.3	95.1	0.45	0.29	1.26	0.01	1.09
LDH12	66.6	68.5	52.8	94.2	0.48	0.32	1.59	0.01	1.15
LDH12	68.5	69.8	51.1	91.2	0.55	0.46	2.01	0.01	1.38
LDH12	69.8	72	11.25	20.1	13.59	7.12	3.1	0.07	47.29
LDH12	72	74	16	28.6	11.86	6.31	3.21	0.09	42.52
LDH12	74	75.5	15.35	27.4	11.14	5.72	4.9	0.07	39.11
LDH12	75.5	77.5	50.6	90.3	0.68	0.43	2.7	0.01	1.96
LDH12	77.5	79.5	51.6	92.1	0.44	0.31	1.78	0.01	1.4
LDH12	79.5	81.5	47.6	84.9	1.09	0.61	3.44	0.01	3.78
LDH12	81.5	82.5	46.7	83.3	1.4	0.8	3.31	0.01	5.02
LDH12	82.5	84.2	45.5	81.2	2.01	1.31	3.22	0.02	7.48
LDH12	84.2	86	10	17.85	13.08	6.79	3.92	0.07	47
LDH12	86	88.2	14.2	25.3	12.1	6.28	3.15	0.08	43.65
LDHB01	0	2.6	44.1	78.7	4.07	1.93	1.03	0.04	11.62
LDHB01	2.6	4.1	47.4	84.6	2.59	1.09	0.59	0.01	8.15
LDHB01	4.1	5.6	48.2	86	2.18	0.95	0.72	0.02	6.92
LDHB01	5.6	8.5	50.6	90.3	1.33	0.72	0.64	0.01	4.25
LDHB01	8.5	10.3	47.5	84.8	2.38	1.25	0.62	0.03	8.46
LDHB01	10.3	10.5	54.5	97.3	0.27	0.2	0.51	0.02	0.72
LDHB01	10.5	12	43.5	77.6	3.47	2.05	0.84	0.04	14.2
LDHB01	12	14	48.5	86.6	1.65	0.94	0.86	0.02	6.69
LDHB01	14	16	49.8	88.9	1.41	0.94	1.04	0.02	5.68
LDHB01	16	18	50.7	90.5	1.06	0.73	1.32	0.02	4.5
LDHB01	18	20	49	87.4	1.02	0.7	1.96	0.01	4.49
LDHB01	20	22	50.2	89.6	0.91	0.67	2.05	0.01	4.12
LDHB01	22	24	49.5	88.3	0.82	0.62	1.81	0.01	4.07
LDHB01	24	26	48.6	86.7	0.94	0.66	1.97	0.01	5.06
LDHB01	26	28	49.5	88.3	0.83	0.61	1.82	0.01	4.98
LDHB01	28	29.1	48.2	86	1.05	0.76	2.12	0.02	6.95
LDHB01	29.1	30.7	47.5	84.8	0.99	0.68	1.62	0.02	8.02

---

**Annexure C – Plans and Cross Sections (Lea Lea and Kido)**



REV	DESCRIPTION	DATE	BY

**Data Sources:**  
 Photogrammetry UAV Survey, Conducted November 2017, EOP, World Street View (Satellite, Dec 2017)  
 Topographic UAV Survey, Conducted November 2017, EOP, World Street View (Satellite, Dec 2017)  
 Contouring  
 Copyright: © 2017

**WARNING:** THESE DATA ARE UNCLASSIFIED AND ARE NOT TO BE USED FOR PERMISSIONS.  
 MAPS TO BE USED FOR PERMITS MUST BE CHECKED BY THE APPLICANT AND THE APPLICANT MUST OBTAIN THE WRITTEN PERMISSION OF  
 GROUNDWORK AUSTRALIA PTY LTD. 08 839 62 00

- Legend:**
- Limestone Rock Samples
  - ◆ Limestone Drill Pad



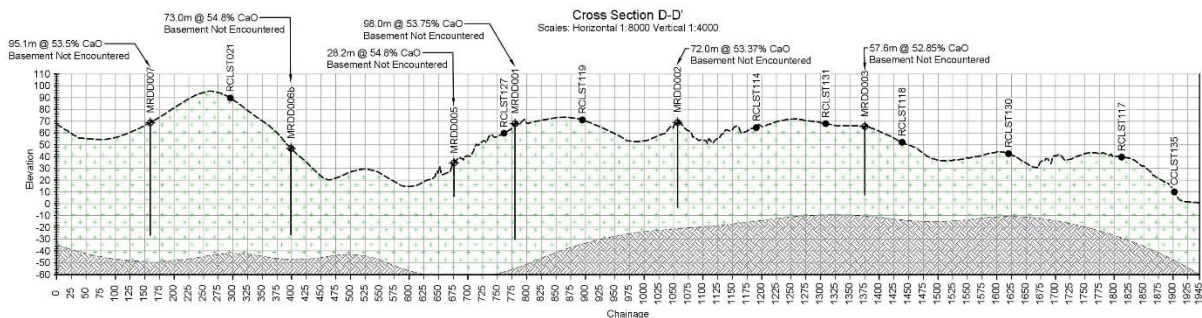
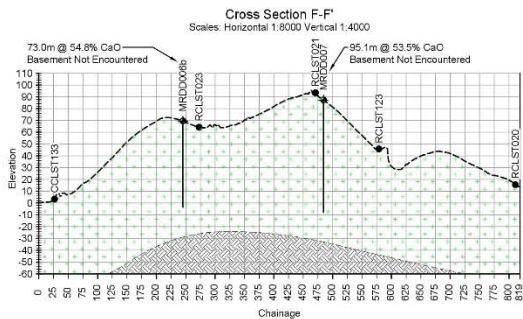
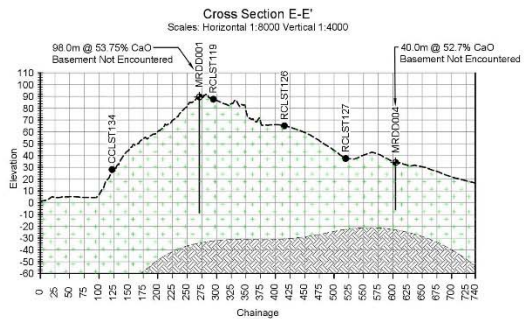
**PROJECT:** Port Moresby Limestone Project - Lea Lea Prospect  
**TITLE:** Drilling Section Location Plan  
**CLIENT:** Mayur Resources Ltd

**GROUNDWORK**  
 1:10,000  
 0 200m  
 1924.DRG.008A  
 DATE: 9 March 2018  
 DRAWN: [Name]  
 CHECKED: [Name]  
 DATUM: WGS84, VERTICAL: ZONE  
 USA / N 8 1 11









PROJECT: 1924 DRG 008D - Kido - Port Moresby Limestone Resource  
 SHEET: 1924 DRG 008D - Kido - Port Moresby Limestone Resource

NO.	DESCRIPTION	UNIT	QTY

MR SOURCE:  
 PROPERTY: UAV Survey, Conducted Nov-2017. BSR: Mole Server, Burmud, 24-2017  
 PROPERTY: UAV Survey, Conducted November 24, 2017. BSR: Mole Server, Burmud, 24-2017  
 EXISTING:

THESE DESIGNS AND PLANS ARE COPYRIGHT AND ARE NOT TO BE USED OR REPRODUCED  
 WITHOUT THE WRITTEN PERMISSION OF  
 GROUNDWORK PLS PTY LTD. MRN: 13 89 412 72

**Legend:**

- Limestone Rock Samples
- ◆ Limestone Drill Pad
- ▨ Interpreted Limestone Resource
- ▩ Basement

PROJECT: Port Moresby Limestone  
 Project - Kido Prospect  
 MAYUR RESOURCES LTD

Drilling Sections D-D' to F-F'  
 Kido

SCALE: 1:8,000  
 0 160m

DRAWN: 1924 DRG 008D  
 DATE: 3 January 2018  
 CHECKED: 3 January 2018

GROUNDWORK  
 P L S  
 PH: +61 7 3071 0411  
 WWW.GROUNDWORKPLS.COM.AU

Annexure D - JORC Table 1

Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
<b>Sampling techniques</b>	<ul style="list-style-type: none"> <li>• Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</li> <li>• Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</li> <li>• Aspects of the determination of mineralisation that are Material to the Public Report.</li> <li>• In cases where ‘industry standard’ work has been done this would be relatively simple (eg ‘reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay’). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</li> </ul>	<ul style="list-style-type: none"> <li>• 64 Rock chip samples selected on a grid pattern.</li> <li>• The core samples were logged by the supervising field geologist and photographed for future reference.</li> <li>• All HQ Diamond drill core sampled on lithological boundaries on two metre sample lengths. The drill core was cut using an industry standard diamond core saw.</li> <li>• Samples when cut were sampled and bagged up with an independent reference number with half of the core retained for future reference.</li> <li>• All samples sent to ALS Laboratory in Brisbane and assayed for CaCO<sub>3</sub>, Al<sub>2</sub>O<sub>3</sub>, CaO, Fe<sub>2</sub>O<sub>3</sub>, MgO, MnO, SiO<sub>2</sub> and a suite of other elements.</li> <li>• Hole numbers were generally designated in incremental order as ‘for Kido MRDD or Lea Lea LDH.</li> </ul>
<b>Drilling techniques</b>	<ul style="list-style-type: none"> <li>• Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</li> </ul>	<ul style="list-style-type: none"> <li>• HQ triple tube core drill was used for resource assessment.</li> <li>• Core logging used a supervising Geologist to log the hole, a trained drilling foreman to supervise drilling activities and 3-4 field hands to assist with operating the rig.</li> </ul>
<b>Drill sample recovery</b>	<ul style="list-style-type: none"> <li>• Method of recording and assessing core and chip sample recoveries and results assessed.</li> <li>• Measures taken to maximise sample recovery and ensure representative nature of the samples.</li> <li>• Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</li> </ul>	<p>Rock chip surface samples</p> <ul style="list-style-type: none"> <li>• HQ half core 2m samples sent to ALS Global for crushing, pulverizing and assay analysis.</li> <li>• Drilled triple tube to maximize core recovery.</li> <li>• Some core loss of finer and infill clay material has occurred. Core recoveries were noted on the drill logs. Further work is required to determine the impacts of core loss on grade although the material if not high grade is likely to be suitable for blending in clinker production.</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>Logging</b>	<ul style="list-style-type: none"> <li>• <i>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</i></li> <li>• <i>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</i></li> <li>• <i>The total length and percentage of the relevant intersections logged.</i></li> </ul>	<ul style="list-style-type: none"> <li>• All rock chip samples visually inspected and recorded.</li> </ul> <p>Drill Core</p> <ul style="list-style-type: none"> <li>• All core geologically logged.</li> <li>• The drill rig had its own Geologist. Each sample was logged by the Geologist supervising that specific rig. Two logging forms were used – one was the ‘Sample Run Sheet’ and the ‘Lithology Log Sheet’. These forms were filled in by hand, and then later photographed and digitised into an Excel spreadsheet. The ‘Sample Run Sheet’ was recorded with the date, drillhole number, sample number, from and to depths, the hole co-ordinates, the sample recovery and magnetic susceptibility information. A ‘comments’ column was also provided.</li> <li>• The ‘Lithology Log Sheet’ was recorded with the Drillhole number, the proposed hole number, the date, the co-ordinates in WGS84, the hole depth, the sampler and the Geologist’s name.</li> <li>• The columns consisted of the ‘from-to’ depths, the Lith codes, the colour, weathering, CaCO3 content, and sand size. A ‘comments’ column was also provided. · A logging and sampling protocols procedure booklet was provided to each geologist with assigned logging codes for them to use.</li> </ul>
<b>Sub-sampling techniques and sample preparation</b>	<ul style="list-style-type: none"> <li>• <i>If core, whether cut or sawn and whether quarter, half or all core taken.</i></li> <li>• <i>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</i></li> <li>• <i>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</i></li> <li>• <i>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</i></li> <li>• <i>Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.</i></li> <li>• <i>Whether sample sizes are appropriate to the grain size of the material being sampled.</i></li> </ul>	<ul style="list-style-type: none"> <li>• All samples were collected at either lithological boundaries if shorter than two metres or on 2m intervals.</li> <li>• The core was cut in half along an orientation line left half to the lab right side of core remaining for future reference.</li> <li>• Representative samples retained.</li> <li>• Field duplicate samples were collected roughly every 20 samples. Duplicate samples were split and placed into two separate sample bags after the sample was thoroughly homogenised. The sample was marked as a duplicate sample on the sample run sheet.</li> <li>• HQ core is halved and sent to laboratory. Half core retained by Mayur.</li> <li>• Insertion of blinds and blanks samples occurred approximately every 20 samples.</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>Quality of assay data and laboratory tests</b>	<ul style="list-style-type: none"> <li><i>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</i></li> <li><i>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</i></li> <li><i>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</i></li> </ul>	<ul style="list-style-type: none"> <li>Once dry, the samples were packed into labelled polyweave bags with approximately 10 samples per bag.</li> <li>All samples sent to a suitably qualified Assay Laboratory in Brisbane. Namely ALS, Brisbane. Quality control done by laboratory where they were dried / crushed / split and pulverised.</li> <li>All assays done using the ME-ICP86 method.</li> <li>Blanks and standards inserted by Mayur. ALS also duplicated samples for assay regularly.</li> </ul>
<b>Verification of sampling and assaying</b>	<ul style="list-style-type: none"> <li><i>The verification of significant intersections by either independent or alternative company personnel.</i></li> <li><i>The use of twinned holes.</i></li> <li><i>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</i></li> <li><i>Discuss any adjustment to assay data.</i></li> </ul>	<ul style="list-style-type: none"> <li>One twinned hole was drilled.</li> <li>A total of 22 holes were completed during the field programme, with good correlations. The hand written drillhole logs prepared by the field geologists were input into two Excel files that were proofread by the supervising Geologist for errors in data entry, logic and formatting.</li> </ul>
<b>Location of data points</b>	<ul style="list-style-type: none"> <li><i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i></li> <li><i>Specification of the grid system used.</i></li> <li><i>Quality and adequacy of topographic control.</i></li> </ul>	<ul style="list-style-type: none"> <li>Location of rock chip samples done using Garmin hand held GPS. Accuracy within 4m<sup>2</sup></li> <li>Table of rock sample locations – refer to table 1 of accompanying ASX announcement.</li> <li>Drill holes are all vertical. Collar locations are tabulated in accompanying ASX announcement.</li> <li>Hole number, from and to for drill core samples – refer to accompanying ASX announcement.</li> <li>Drill Collar points have been rectified back to detailed survey data</li> <li>The data has been projected to UTM WGS84 55S.</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>Data spacing and distribution</b>	<ul style="list-style-type: none"> <li>• <i>Data spacing for reporting of Exploration Results.</i></li> <li>• <i>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</i></li> <li>• <i>Whether sample compositing has been applied.</i></li> </ul>	<ul style="list-style-type: none"> <li>• High level drillhole planning and layout was guided by the extent of urace outcrop and geological and topographic features patterns that showed the limestone unit.</li> <li>• The drill pattern was based on holes 200 - 300 metres apart.</li> <li>• All holes were situated perpendicular to the orientation of the limestone and where practical at 900 to the dip of the strata.</li> <li>• The data density in the majority of areas is sufficient to establish grade and thickness continuity of the mineralised units. In some.</li> <li>• Sample compositing has been applied on two metre intervals.</li> </ul>
<b>Orientation of data in relation to geological structure</b>	<ul style="list-style-type: none"> <li>• <i>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</i></li> <li>• <i>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</i></li> </ul>	<ul style="list-style-type: none"> <li>• No geological interpretation or relationships have been observed which bias the sampling. That said core loss will be further assessed by comparison of the bulk sample results with nearby core assay results</li> <li>• Basic flat lying to moderately dipping limestone formation, allowing for majority of vertical holes with several angled holes.</li> </ul>
<b>Sample security</b>	<ul style="list-style-type: none"> <li>• <i>The measures taken to ensure sample security.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Mayur developed a 'chain of custody' flowsheet prior to the of the commencement of the programme that was strictly adhered to.</li> <li>• All drill sample/core trays were supervised for collection and logged onsite.</li> <li>• Following this they were repacked into polyweave bags ready for dispatch from site. The Polybags were then transported to Port Moresby with Mayur staff members on board. The samples were then trucked to Port Moresby under the supervision of Mayur staff, either stored temporarily in the Mayur Container or taken directly to Mayur's freight forwarder in Port Moresby, Pacific Cargo Services, where a dispatch inventory was prepared and the samples either airfreighted by pallet or sea freighted FCL by container to Port of Brisbane.</li> <li>• The company's Australian freight logistics representative Aussie Freight then cleared the samples through customs and quarantine and transported them to the ALS Laboratory in Brisbane.</li> </ul>
<b>Audits or reviews</b>	<ul style="list-style-type: none"> <li>• <i>The results of any audits or reviews of sampling techniques and data.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Field checks have been completed and the data has been audited</li> </ul>

## Section 2 Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
<b>Mineral tenement and land tenure status</b>	<ul style="list-style-type: none"> <li>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</li> <li>The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.</li> </ul>	<ul style="list-style-type: none"> <li>The tenement (EL2303) comprising the Port Moresby Limestone Project is 100% owned by Mayur Iron PNG Ltd, a 100% owned subsidiary of Mayur Resources Limited. EL2303 is valid until 13 May 2018</li> </ul>
<b>Exploration done by other parties</b>	<ul style="list-style-type: none"> <li>Acknowledgment and appraisal of exploration by other parties.</li> </ul>	<ul style="list-style-type: none"> <li>None known at this stage.</li> </ul>
<b>Geology</b>	<ul style="list-style-type: none"> <li>Deposit type, geological setting and style of mineralisation.</li> </ul>	<ul style="list-style-type: none"> <li>Early Tertiary Limestone deposit.</li> <li>Partially recrystallized.</li> <li>Flat lying to gently dipping massive homogeneous limestone.</li> <li>Slightly weathered and unaltered.</li> </ul>
<b>Drill hole Information</b>	<ul style="list-style-type: none"> <li>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> <li>easting and northing of the drill hole collar</li> <li>elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar</li> <li>dip and azimuth of the hole</li> <li>down hole length and interception depth</li> <li>hole length.</li> </ul> </li> <li>If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.</li> </ul>	<ul style="list-style-type: none"> <li>All rock chip samples taken at surface with coordinates and RL recorded.</li> <li>All drill hole collar locations including easting, northing and RL are recorded in accompanying ASX announcement.</li> <li>All drill core samples record the from and to distance from the collar location down hole.</li> </ul>
<b>Data aggregation methods</b>	<ul style="list-style-type: none"> <li>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.</li> <li>Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</li> <li>The assumptions used for any reporting of metal equivalent values should be clearly stated.</li> </ul>	<ul style="list-style-type: none"> <li>Refer to Section 3 for cut off grades</li> <li>Weighted average i.e. length x grade samples used for initial assessment.</li> <li>Inverse Distance weighted (power 3) used for resource estimation purposes.</li> <li>Sample compositing completed on two metre intervals.</li> <li>No high grade or low grade cut values applied as all high grade and low grade values are considered real and reflect localized changes in sedimentation.</li> <li>No metal equivalents being reported.</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>Relationship between mineralisation widths and intercept lengths</b>	<ul style="list-style-type: none"> <li>• <i>These relationships are particularly important in the reporting of Exploration Results.</i></li> <li>• <i>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</i></li> <li>• <i>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').</i></li> </ul>	<ul style="list-style-type: none"> <li>• Rock chip samples collected over a gridded pattern.</li> <li>• Drill holes on each prospect are spaced on nominal 250m centres.</li> <li>• The mineralisation is flay lying to modestly dipping shallow dipping thus downhole widths are considered as the 'true thickness'</li> </ul>
<b>Diagrams</b>	<ul style="list-style-type: none"> <li>• <i>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</i></li> </ul>	<ul style="list-style-type: none"> <li>• See location maps in accompanying ASX announcement.</li> </ul>
<b>Balanced reporting</b>	<ul style="list-style-type: none"> <li>• <i>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Location and assay results only reported.</li> </ul>
<b>Other substantive exploration data</b>	<ul style="list-style-type: none"> <li>• <i>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</i></li> </ul>	<ul style="list-style-type: none"> <li>• A 3D drone topographic survey was completed on site at Kido and Lea Lea</li> <li>• 4 bulk samples (2 pits at Lea Lea and 2 at Kido) have been completed</li> </ul>
<b>Further work</b>	<ul style="list-style-type: none"> <li>• <i>The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).</i></li> <li>• <i>Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Bulk samples (2 pits at Lea Lea and 2 at Kido) will undergo relevant testing.</li> <li>• See diagrams in accompanying ASX announcement</li> </ul>

### Section 3 Estimation and Reporting of Mineral Resources

Criteria	JORC Code explanation	Commentary
<b>Database integrity</b>	<ul style="list-style-type: none"> <li>• <i>Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.</i></li> <li>• <i>Data validation procedures used.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Data collated by Mayur from digital hardcopy reports and appendices</li> <li>• Digital geological logging information was compiled by Groundwork from hard copy logs for all available holes and core photographs</li> <li>• Checks completed by Groundwork include: <ul style="list-style-type: none"> <li>• Data was imported into an Access database with indexed fields, including checks for duplicate entries, sample overlap, unusual assay</li> </ul> </li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>values and missing data.</p> <ul style="list-style-type: none"> <li>• Additional error checking using the Surpac database audit option for incorrect hole depth, sample/logging overlaps and missing downhole surveys.</li> <li>• Manual checking of logging codes for consistency, plausibility of drill hole trajectories and assay grades.</li> <li>• Assessment of the data confirms that it is suitable for resource estimation.</li> </ul>
<b>Site visits</b>	<ul style="list-style-type: none"> <li>• <i>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</i></li> <li>• <i>If no site visits have been undertaken indicate why this is the case.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Groundwork Plus visited the site.</li> </ul>
<b>Geological interpretation</b>	<ul style="list-style-type: none"> <li>• <i>Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.</i></li> <li>• <i>Nature of the data used and of any assumptions made.</i></li> <li>• <i>The effect, if any, of alternative interpretations on Mineral Resource estimation.</i></li> <li>• <i>The use of geology in guiding and controlling Mineral Resource estimation.</i></li> <li>• <i>The factors affecting continuity both of grade and geology.</i></li> </ul>	<ul style="list-style-type: none"> <li>• A simple geological model exists being two large hills of geologically consistent and relatively homogenous grade biomicritic limestone. These are large topographic features.</li> <li>• Geological modelling has used Surpac 3D software to generate solids and surfaces from 200m space cross sections which have then been incorporated in to a block model.</li> <li>• Drilling suggests the limestone is laterally open in horizontal directions and at depth. Some drillholes have terminated in limestone.</li> <li>• Geological understanding is high and appropriate for resource estimation</li> <li>• Alternative interpretations are possible but not considered likely due to the straight forward nature of the limestone. Any alternative is unlikely to affect the estimates.</li> <li>• The style of mineralisation and the orebody type means sedimentation processes along with structural deformation and later groundwater movements control calcium grades.</li> <li>• There is an obvious structural control to mineralisation being bedding and larger scale sedimentary controls.</li> </ul>
<b>Dimensions</b>	<ul style="list-style-type: none"> <li>• <i>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The resources at a cut-off of 48% CaO form two consistent limestone hills, both with a strike length of over 1000m in an NW-SE orientation. Limestone occurs at surface and continues to at least -</li> </ul>



Criteria	JORC Code explanation	Commentary
		20 RL in the Kido area.
<b>Estimation and modelling techniques</b>	<ul style="list-style-type: none"> <li>• <i>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</i></li> <li>• <i>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</i></li> <li>• <i>The assumptions made regarding recovery of by-products.</i></li> <li>• <i>Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).</i></li> <li>• <i>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</i></li> <li>• <i>Any assumptions behind modelling of selective mining units.</i></li> <li>• <i>Any assumptions about correlation between variables.</i></li> <li>• <i>Description of how the geological interpretation was used to control the resource estimates.</i></li> <li>• <i>Discussion of basis for using or not using grade cutting or capping.</i></li> <li>• <i>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The limestone block grade was estimated using inverse Distance Weighting (power3) using Surpac software. Groundwork considers inverse Distance Weighting (power3) to be an appropriate estimation technique for this type of mineralisation.</li> <li>• The base of the limestone at Lea Lea was treated as a hard boundary during estimation</li> <li>• The relatively modest CV for CaO and absence of extreme values precluded the need for top-cutting.</li> <li>• A total of 806 samples were used to estimate the limestone resource area.</li> <li>• No assumptions were made regarding the recovery of by-products, although it is considered likely that the bulk of the by products will be used as either raw feed for clinker or as quarry products.</li> <li>• Variography was performed for the limestone. Grade continuity was high for the directional variograms.</li> <li>• Drill holes are on an irregular grid with a nominal spacing of 250 x 250m.</li> <li>• Composites have been taken using 2 metre intervals.</li> <li>• Block dimensions are 50x50x10m (E, N, RL respectively) for parent block sizes and 25x 25 x10 for grade resolution. The block dimensions were chosen as they are representative of grade continuity, which is homogenous and were as large as could be practically achieved.</li> <li>• The vertical dimension was shortened to reflect downhole data spacing</li> <li>• The initial search ellipse (isotropic) was 200m increasing to 600m for the second pass and 1200m for the third. The minimum number of composites used was 3 with a maximum of 25. The maximum number of composites per drill hole was set to 8 to ensure at least 3 drill holes were used for the resource estimate.</li> <li>• The maximum extrapolation of the estimates is 300m.</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>The estimation procedure was reviewed as part of an internal Groundwork peer review. Inverse Distance Squared check models were produced by Groundwork. The tonnage, grade and classification of the check estimates agreed well with the primary resource estimate.</li> <li>No deleterious elements or acid mine drainage has been factored in the resource estimate as none are known.</li> <li>The final block model was reviewed visually, and it was concluded that the block model fairly represents the grades observed in the drill holes. Groundwork also validated the block model statistically using a variety of histograms, boxplots, swathe plots and summary statistics.</li> <li>No production has taken place, so no reconciliation data is available.</li> </ul>
<b>Moisture</b>	<ul style="list-style-type: none"> <li>Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.</li> </ul>	<ul style="list-style-type: none"> <li>Tonnages are estimated on a dry weight basis; moisture not determined.</li> </ul>
<b>Cut-off parameters</b>	<ul style="list-style-type: none"> <li>The basis of the adopted cut-off grade(s) or quality parameters applied.</li> </ul>	<ul style="list-style-type: none"> <li>48% CaO cut off for Inferred Resources 50% for Indicated and 52% for Measured Resources. The cut-off grade at which the resource is quoted reflects an intended bulk-mining approach.</li> </ul>
<b>Mining factors or assumptions</b>	<ul style="list-style-type: none"> <li>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</li> </ul>	<ul style="list-style-type: none"> <li>Groundworks understanding of a bulk mining scenario is based on information supplied by Mayur and considers typical industry standards.</li> <li>Mining will be completed by conventional bulk drill and blast extraction using ANFO or equivalent explosives.</li> <li>The sub block model block size (25x25x10m) is the effective minimum mining dimension for this estimate.</li> <li>No internal dilution has been factored into the modelling due to resource homogeneity.</li> </ul>
<b>Metallurgical factors or assumptions</b>	<ul style="list-style-type: none"> <li>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this</li> </ul>	<ul style="list-style-type: none"> <li>Some metallurgical test work including Sibelco kiln suitability and decrepitation testing and geochemical sampling by ALS Global has been completed. These results demonstrate material suitability.</li> <li>A lime kiln of yet to be determined specifications is envisaged and is assumed that there will be no significant problems with grade or</li> </ul>

Criteria	JORC Code explanation	Commentary
	<p><i>should be reported with an explanation of the basis of the metallurgical assumptions made.</i></p>	<p>material strength of the limestone given the results returned to date.</p> <ul style="list-style-type: none"> <li>No penalty elements have been identified in the testing so far however silica levels will require detailed grade control management to allow for effective incorporation into the kiln feed. The silica is likely to be of benefit for clinker production, and also the production of quarry materials.</li> <li>Bulk samples have been taken for crushing and materials assessment to determine kiln and other product yields along with general material suitability.</li> </ul>
<p><b>Environmental factors or assumptions</b></p>	<ul style="list-style-type: none"> <li><i>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a Greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</i></li> </ul>	<ul style="list-style-type: none"> <li>The area lies adjacent to the coastline and accordingly hydraulic issues along with coastal geomorphology and other potential coast line impacts will need to be considered.</li> <li>Waste materials will be in so far as is practical used and sold as construction materials. Material surplus to this will be placed in overburden storage dumps or used for progressive rehabilitation of the site. The limestone while having a natural alkalinity does not contain sulfides or other minerals which are likely to impact deleteriously upon the local environment provided industry standard control measures are used.</li> <li>The area is covered with sparse vegetation typical of this part of PNG.</li> <li>No significant environmental sites of importance have yet been recognized.</li> <li>Detailed environmental works will be commenced to further assess the potential impacts of the area on mining.</li> </ul>
<p><b>Bulk density</b></p>	<ul style="list-style-type: none"> <li><i>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</i></li> <li><i>The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.</i></li> <li><i>Discuss assumptions for bulk density estimates used in the evaluation</i></li> </ul>	<ul style="list-style-type: none"> <li>Density of the limestone has been measured at 2.7 t/m<sup>3</sup> and is consistent with limestone values from around the world. Apparent Particle Densities have been used pursuant to the relevant Australian standard.</li> <li>That said more density test work is required to further confirm density values on site and for reserve purposes.</li> <li>Density values for soil and clay used are 1.8 t/m<sup>3</sup>.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<p><i>process of the different materials.</i></p>	<ul style="list-style-type: none"> <li>• Density values for marl and siltstone used are 2.6 t/m<sup>3</sup>.</li> <li>• Density values for distinctly weathered limestone used are 2.2 t/m<sup>3</sup>. Further density measurements are required on the various categories of more weathered material.</li> </ul>
<p><b>Classification</b></p>	<ul style="list-style-type: none"> <li>• <i>The basis for the classification of the Mineral Resources into varying confidence categories.</i></li> <li>• <i>Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</i></li> <li>• <i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The deposit consists of Measured, Indicated and Inferred Resources. The classification is based on the grade continuity exhibited in the variography and the search passes used in the grade interpolation subject to assessment of other impacting factors such as core handling and sampling procedures, QAQC outcomes, density measurements along with the geological model.</li> <li>• Search Pass 1 is used to classify Measured Resources in the area of the drilling over the main areas of clear and discernable limestone outcrop. Pass 2, is classed as Indicated and Pass 3 and 4 as an Inferred Mineral Resources.</li> <li>• The classification appropriately reflects the Competent Person's view of the deposit.</li> </ul>
<p><b>Audits or reviews</b></p>	<ul style="list-style-type: none"> <li>• <i>The results of any audits or reviews of Mineral Resource estimates.</i></li> </ul>	<ul style="list-style-type: none"> <li>• No audits or reviews have been completed.</li> </ul>
<p><b>Discussion of relative accuracy/ confidence</b></p>	<ul style="list-style-type: none"> <li>• <i>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</i></li> <li>• <i>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i></li> <li>• <i>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The relative accuracy and confidence level in the Mineral resource estimates is considered to be in line with the generally accepted accuracy and confidence of the nominated Mineral Resource categories for this type of material. This has been determined on a qualitative, rather than quantitative, basis, and is based on the Competent Person's experience with similar deposits.</li> <li>• The geological nature of the deposit, composite/block grade comparison and the coefficient of variation for CaO lend themselves to a reasonable level of confidence in the resource estimates.</li> <li>• The Mineral Resource estimates are considered to be accurate globally, but there is some uncertainty in the local estimates due to the current drillhole spacing and a more detailed lack of geological definition.</li> <li>• No mining of the deposit has taken place and resultantly no production data is available for comparison.</li> </ul>