1 September 2020

UPDATED RUPICE MINERAL RESOURCE ESTIMATE AND DRILLING RESULTS

ABOUT ADRIATIC METALS (ASX:ADT, LSE:ADT1)

Adriatic Metals Plc is focused on the development of the 100%-owned, Vares high-grade silver project in Bosnia & Herzegovina.

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HIGHLIGHTS

- **Indicated and Inferred Mineral Resource estimate ("MRE") for Adriatic Metals' 100%-owned Rupice silver-gold-zinc-lead deposit in Bosnia & Herzegovina, now stands at:**
  - 12.0Mt @ 149g/t Ag, 1.4g/t Au, 4.1% Zn, 2.6% Pb, 0.5% Cu, 25% $BaSO_4$ (reported above a cut-off grade of 50g/t AgEq) containing 58Moz Ag, 527koz Au, 489kt Zn & 312kt Pb
- **This represents a 32% increase in tonnes compared to the maiden 2019 Rupice MRE (using a 50g/t AgEq cut-off).**
- **79% of the updated Mineral Resource is classified as Indicated.**
- **The updated MRE will provide the foundation to the PFS, which will incorporate ongoing metallurgical test work results and mining studies designed to optimise and improve the planned development configuration of the project compared with that outlined in the November 2019 Scoping Study.**
- **Recent drilling has also intersected high-grade massive sulphide mineralisation at Rupice – with the system remaining open towards the north and down-dip to the south.**

Adriatic Metals Plc (ASX:ADT, LSE:ADT1) ("Adriatic" or the "Company") is pleased to announce the updated Mineral Resource estimate for the Rupice Silver Deposit in the Vares Silver Project, in Bosnia & Herzegovina, which has been completed by CSA Global Pty Ltd ("CSA Global").

Paul Cronin, Adriatic's Managing Director and CEO commented, "*I am thrilled that we have substantially increased our resource base as we go into the next stage of project development. This updated MRE shows the world class nature of the deposit and positions the Company as one of the leading silver developers in the industry.*" He also added *"During the COVID-19 pandemic, I have been impressed by the resolve of our Vares based team to deliver results in a timely and safe manner. Rupice is an exceptionally high-grade silver dominant deposit, and the increase in tonnes will expand on the results of our 2019 Scoping Study, as we seek to finalise a Pre-Feasibility Study in the coming weeks."*

MRE UPDATE

The updated Indicated and Inferred Mineral Resource estimate was prepared by CSA Global in Perth and comprises 12.0 Mt at 149 g/t Ag, 1.4g/t Au, 4.1% Zn and 2.6% Pb, as set out in Table 1.

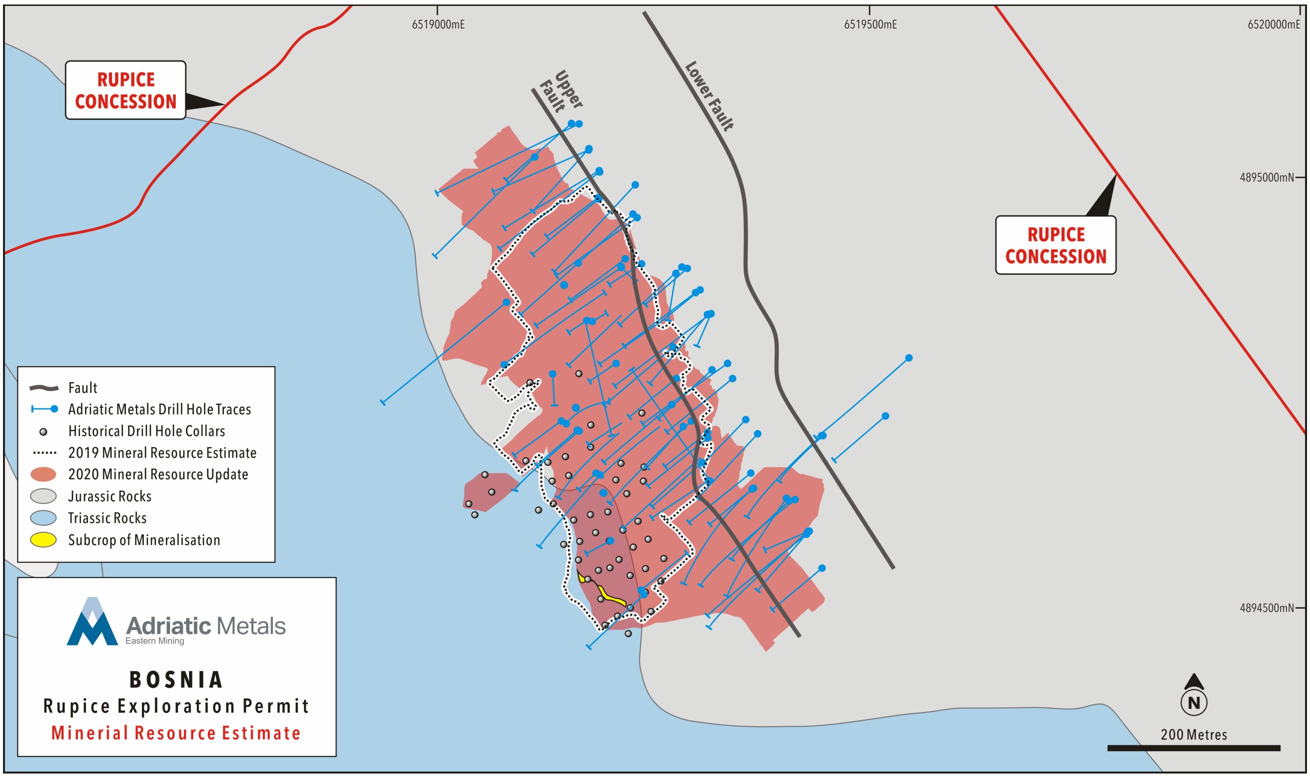
Table 1 - Rupice updated MRE by Classification

Rupice Mineral Resources, August 2020																
JORC Classification	Tonnes (mt)	Grades							Contained metal							
		Ag	Zn	Pb	Au	Cu	Sb	$BaSO_4$	Ag	Zn	Pb	Au	Cu	Sb	$BaSO_4$
		g/t	%	%	g/t	%	%	%	Moz	Kt	Kt	Koz	Kt	kt	Kt
Indicated	9.5	176	4.9	3.1	1.6	0.5	0.2	29	54	466	294	500	52	22	2,732
Inferred	2.5	49	0.9	0.7	0.3	0.2	0.1	9	4	23	18	27	4	3	218
Total	**12.0**	**149**	**4.1**	**2.6**	**1.4**	**0.5**	**0.2**	**25**	**58**	**488**	**312**	**526**	**56**	**24**	**2,949**

Notes:

- *Mineral Resources are based on JORC Code definitions.*
- *A cut-off grade of 50g/t silver equivalent has been applied.*
- *AgEq – Silver equivalent was calculated using conversion factors of 31.1 for Zn, 24.88 for Pb, 80.0 for Au, 1.87 for $BaSO_4$, 80.87 for Cu and 80.87 for Sb, and recoveries of 90% for all elements. Metal prices used were US$2,500/t for Zn, US$2,000/t for Pb, $150/t for $BaSO_4$, $2,000/oz for Au, $25/oz for Ag, $6500/t for Sb and $6,500 for Cu.*
- *The applied formula was: AgEq = Ag(g/t) * 90% + 31.1 * Zn(%) * 90% + 24.88 * Pb(%) * 90% + 1.87 * $BaSO_4$% * 90% + 80 * Au(g/t) * 90% + 80.87 * Sb(%) * 90% + 80.87 * Cu(%)* 90%*
- *It is the opinion of Adriatic Metals and the Competent Persons that all elements and products included in the metal equivalent formula have a reasonable potential to be recovered and sold.*
- *Metallurgical recoveries of 90% have been applied in the metal equivalent formula based on recent and ongoing test work results.*
- *A bulk density was calculated for each model cell using regression formula BD = 2.745 + $BaSO_4$ * 0.01793 + Pb * 0.06728 - Zn * 0.01317 + Cu * 0.1105 for the halo domain, BD = 2.7341 + $BaSO_4$ * 0.01823 + Pb * 0.04801 + Zn * 0.03941 - Cu * 0.01051 for the fault zones and BD = 2.7949 + $BaSO_4$ * 0.01599 + Pb * 0.05419 + Zn * 0.01169 + Cu * 0.06303 for the low grade domain. Bulk density values were interpolated to the combined high-grade domain from 631 BD measurements.*
- *Rows and columns may not add up exactly due to rounding.*

Figure 1 – Plan View of the New Ore Block Model Outline of Rupice vs 2019 Ore Block Model



RUPICE DRILLING AND SAMPLING

For the Mineral Resource estimate, a total of 167 diamond drill holes (46 historical drill holes and 121 drill holes from the Company's drilling programmes in 2017 (8 holes), 2018 (39 holes), 2019 (52 holes) and 2020 (22 holes)) for 38,135m define the current limits of the known mineralisation. The deposit was drilled and sampled using diamond drill holes at a nominal 20m by 20m spacing.

Drill holes drilled by the Company were generally angled –50° to –80° mostly towards the southwest with dip angles set to optimally intersect the mineralised bodies. Additional drill holes were drilled from the opposite direction, and perpendicular to the mineralised trend. All the historical holes were vertical and focussed on the up-dip portion of the Rupice mineralisation.

The drill core was sampled for assay; whole core for the historical drilling and half core (HQ and PQ) for the recent drilling. Recent assays were sent to ALS in Bor, Serbia for multi-element analyses.

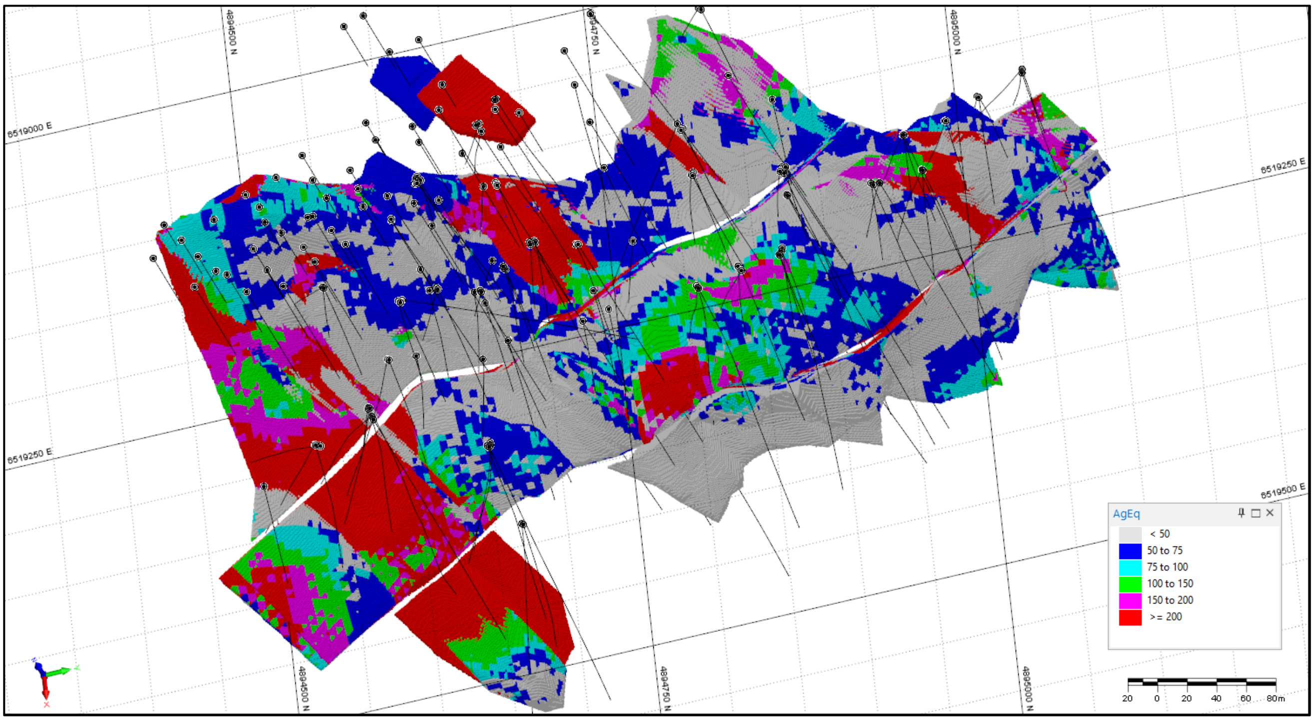
RUPICE GEOLOGY AND MINERALISATION

The host rocks at Rupice comprises Middle Triassic limestone, dolostone, calcareous and dolomitic marl, and a range of mostly fine-grained siliciclastic rocks including cherty mudstone, mudstone, siltstone and fine-grained sandstone. The main mineralised horizon is a brecciated dolomitic unit that dips at around 50° to the northeast and has been preferentially mineralised with base, precious and transitional metals. The Triassic sequence has been intensely deformed both by early stage ductile shearing and late stage brittle faulting.

The Rupice polymetallic mineralisation consists of sphalerite, galena, barite and chalcopyrite with silver, gold, tetrahedrite, boulangerite and bournonite, with pyrite. The majority of the high-grade mineralisation is hosted within the brecciated dolomitic unit, which is offset and cut by northwest striking, westerly dipping syn-post mineral faulting. This faulting displaces the mineralised body up to 20 metres in places. Thickening of the central portion of the orebody occurs where these faults flexure and deform. Mineralised widths up to 65 metres true thickness are seen in the central portion of the orebody.

To date, the massive sulphide mineralisation at Rupice has a defined strike length of 650 metres, with an average true-width thickness of around 20 metres. However, mineralisation at Rupice still remains open towards the north and down-dip to the south.

Figure 2 - Rupice Ore Block Model by AgEq Grade Ranges



RUPICE MODELLING AND GRADE INTERPOLATION

The main geological features that control the polymetallic mineralisation at Rupice were interpreted using geological and structural data collected. Three main domains were interpreted and wireframed individually; the main mineralised brecciated dolomitic units, that hosts the high-grade mineralisation; the fault zones that off-set and displace these main mineralised bodies; and a lower-grade halos peripheral and in the footwall of the main mineralised bodies.

Statistical analysis of modelled domains showed that the main mineralised brecciated dolomite has a bimodal population for the majority of the elements being modelled. The higher-grade populations clustered spatially and were subsequently individually interpreted and wireframed.

Ten elements were modelled; Ag, Zn, Pb, $BaSO_4$, Cu, Au, Sb, Hg, As and S, and the higher-grade populations were interpreted and wireframed for all elements except Hg, As and Sb.

All the domains were interpreted on a section by section basis and were used to generate 3D 'solid' wireframes. The same methodology was applied for the individual high-grade populations.

Once mineralisation for each element was interpreted and wireframed, classical statistical analysis was repeated for the samples within the interpreted domains. Drill data was composited to 2m down hole intervals. Boundary statistical analyses and top cuts were determined and applied.

The geostatistical analysis generated a series of semi-variograms that were used during grade estimation using Ordinary Kriging ("OK"). The semi-variogram ranges determined from the analysis contribute heavily to the determination of the search neighbourhood dimensions. All variograms were calculated and modelled for the composited sample file, constrained by the corresponding mineralised envelopes for each element. Where low-grade and high-grade domains were modelled, samples were combined for both domains to make sure that the number of samples was sufficient for robust geostatistical analysis. It was found that absolute semi-variograms were difficult to model for most of elements, and therefore, relative semi-variograms were modelled for Pb, $BaSO_4$, Ag, Au, Sb, Hg, As and Cu. Absolute variograms were modelled for Zn and S.

The density values were calculated for each model cell using a regression formula for all the domains except the combined high-grade domain. The formula was calculated using scattergrams for density versus $BaSO_4$, Pb, Cu and Zn grades. Density values were interpolated within the limits of the combined high-grade domain.

A block model was constructed, constrained by the interpreted mineralised envelopes. A parent cell size of 5 m(E) x 5 m(N) x 5 m(RL) was adopted with standard sub-celling to 1 m(E) x 1 m(N) x 1 m(RL) to maintain the volumetric resolution of the mineralised lenses.

Grades for all ten elements were interpolated into the empty block model using the Ordinary Kriging method and a "parent block estimation" technique, i.e. all sub-cells within a parent cell were populated with the same grade. The OK process was performed at different search radii until all cells were interpolated. The search radii were determined by means of the evaluation of the semi-variogram parameters, which determined the kriging weights to be applied to samples at specified distances.

Block grades were validated both visually and statistically and all modelling was completed using Micromine software.

RUPICE CLASSIFICATION AND REPORTING

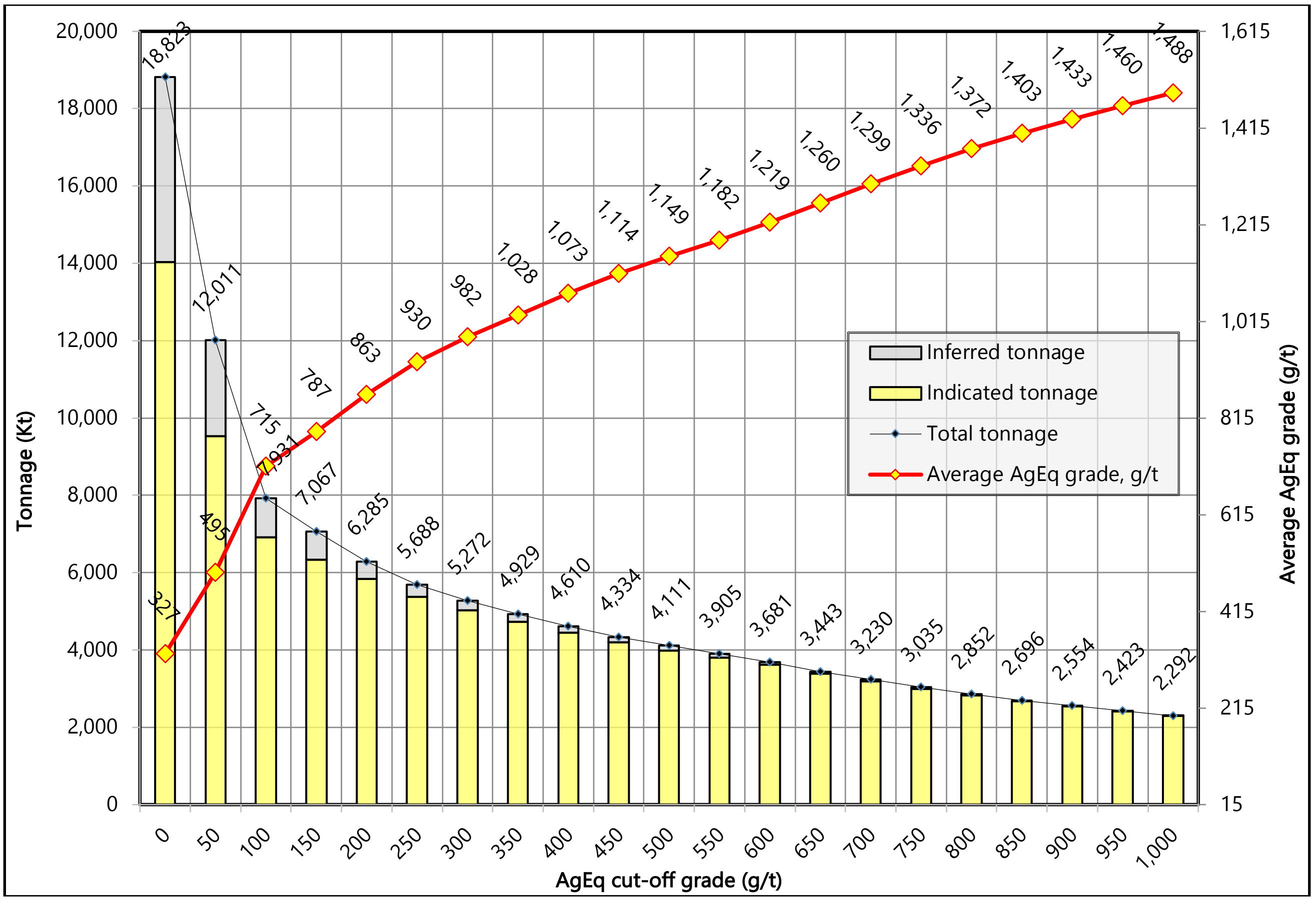
Clause 20 of the JORC (2012) Code requires that all reports of Mineral Resources must have reasonable prospects for eventual economic extraction, regardless of the classification of the resource. The Rupice deposit has reasonable prospects for eventual economic extraction on the following basis:

- Metallurgical test work by WAI has confirmed that the Rupice mineralisation is amenable to flotation processes;
- Preliminary metallurgical test work has confirmed that a barite concentrate should meet API specifications;
- A marketing study by a leading consultant in the field of barite confirmed that there is an opportunity to enter the market as a niche player levering any logistical advantages for a supplier in Bosnia & Herzegovina;
- The cut-off grade adopted for reporting (50g/t Ag equivalent) is considered reasonable given the Mineral Resource will most likely be exploited by underground mining methods and processed using flotation techniques.

The Scoping Study demonstrated that the deposit potentially has a positive net present value (NPV), and that the mineralised zone is potentially mineable using underground methods under the given economic scenario and parameters. CSA Global did not estimate Ore Reserves for the deposit. The deposit appears to have reasonable prospects of eventual economic extraction under a realistic set of criteria.

The Rupice Mineral Resource has been classified based on the guidelines specified in the JORC Code. The classification level is based upon an assessment of geological understanding of the deposit, geological and mineralisation continuity, drill hole spacing, QC results, search and interpolation parameters and an analysis of available density information. The MRE is reported by classification in Table 1, above a cut-off grade of 50g/t silver equivalent.

Figure 3 – Grade Tonnage Curve with AgEq Grades



RECENT DRILL RESULTS

The Company is pleased to announce that it has received assay results from BR-10-20, BR-11-20, BR-12-20, BR-13-20, BR-17-20, BR-18-20, BR-20-20, BR-22-20 and BR-23-20, which have been incorporated into the recent Mineral Resource estimate.

Drillhole BR-20-20 (Figure 7) is the most southern drill hole drilled at Rupice to date. It was designed to test the extension of the Rupice orebody along strike to the southeast. The results from this hole have shown that the massive sulphide mineralisation continues southwards. Follow up drilling will test the continuity of mineralisation to the south, up-dip and down-dip from this intercept.

Drillholes BR-11-20, BR-12-20 (Figure 5) and BR-13-20 (Figure 5) successfully intersected mineralisation. They were designed to test the shallower part of the deposit to the south-west, and to confirm historic drilling results.

BR-17-20 and BR-18-20 (Figure 6) were designed to test the up-dip continuation of the known massive sulphide mineralisation in the central part of the deposit. They were also designed to test potential massive sulphide mineralisation in the footwall of the main mineralised body. Higher grade mineralisation was intercepted in two shorter intervals up-dip from the main mineralised body in BR-17-20, followed by a wider low-grade halo in the footwall of the deposit.

For BR-18-20, massive sulphide mineralisation was encountered up-dip from the main mineralised body, confirming continuity of the known mineralised zone.

Drill hole BR-14-20 in the northern part Rupice, and BR-15-20 in the south-western part of Rupice were also drilled. These were designed as investigate continuity of mineralised zone. Mineralisation was encountered, however of a weaker tenor.

Mineralisation still remains open down-dip and to the south and north, into previously untested ground outside of the current ore block model.

The mineralised intervals of the drill holes are shown in Table 2 with further information in Appendix 1.

Table 2 – Drill Hole Results for the Reported Holes; Lead or Zinc greater than 1%,

Hole	From (m)	To (m)	Interval (m)	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$ %
BR-10-20	204.0	206.0	2.0	2.45	1.24	0.45	16	0.07	0
BR-11-20	62.2	67.0	4.8	1.68	1.73	0.66	150	0.51	56
BR-12-20	113.5	116.4	2.9	4.52	3.44	1.29	224	0.29	32
BR-13-20	123.5	134.9	11.4	2.39	1.58	0.69	54	0.55	14
BR-17-20	204.0	206.0	2.0	1.85	0.82	0.89	141	0.27	26
BR-18-20	174.7	183.7	9.0	1.85	1.39	0.99	152	0.82	51
BR-20-20	228.2	238	9.8	1.62	1.50	0.55	106	0.45	24
BR-22-20	307.0	311.0	4.0	1.28	0.32	0.04	28	0.01	4
BR-23-20	329.0	338.6	9.6	5.01	5.03	1.28	431	0.60	57

Figure 4: Plan Map showing the Location of the Rupice Drill Holes

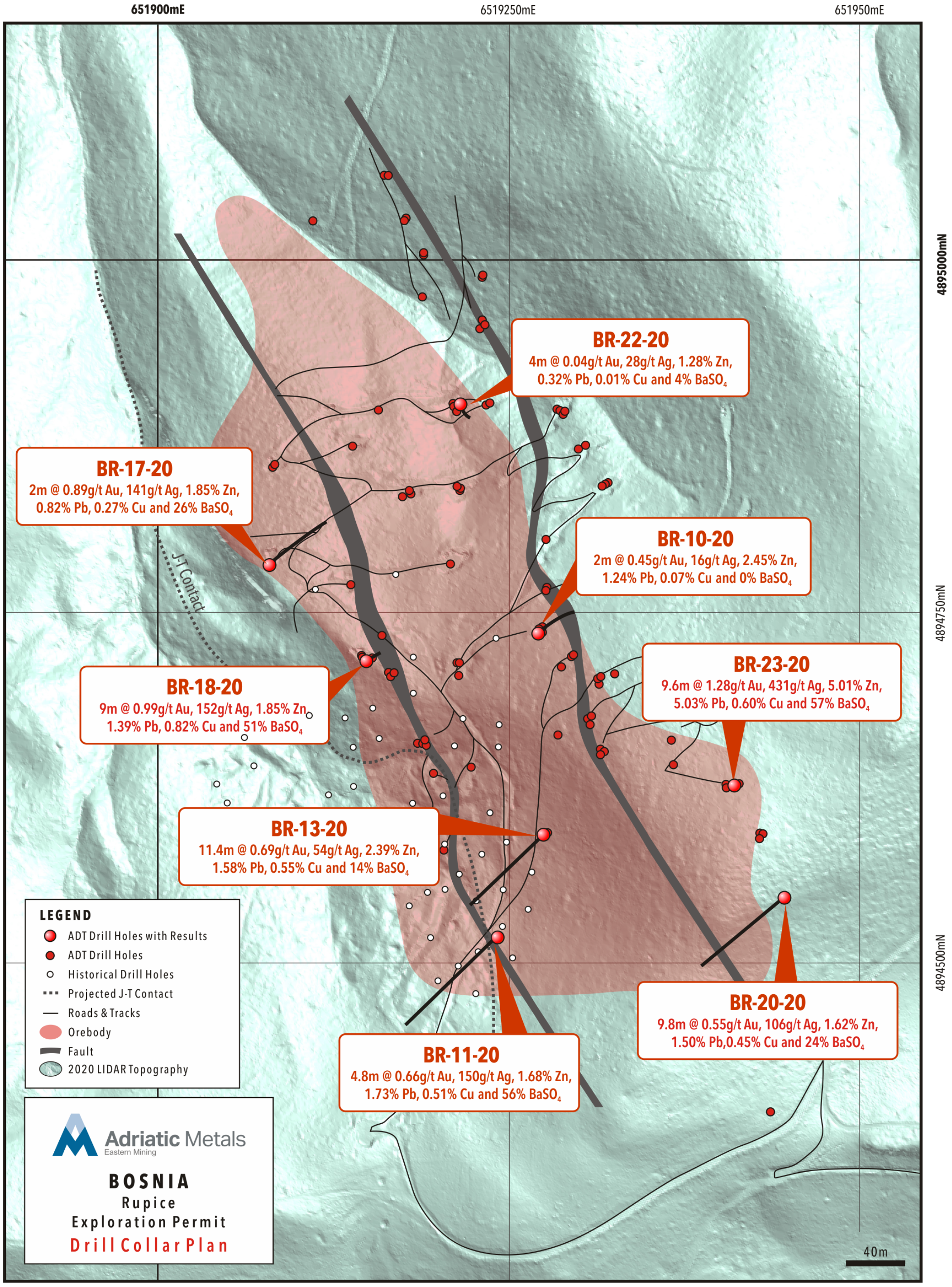


Figure 5: Cross Section illustrating Drill Hole BR-13-20

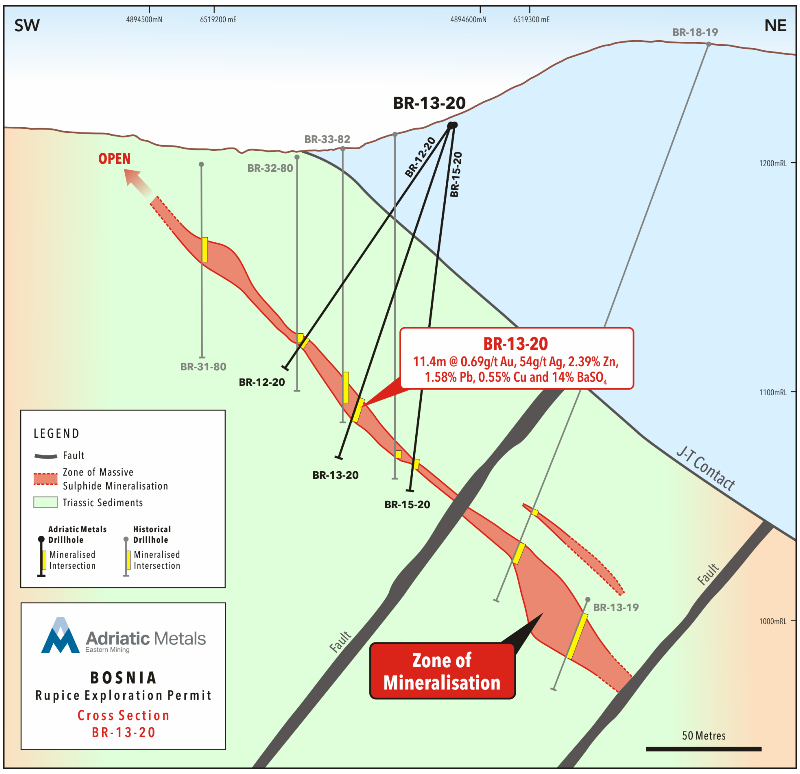


Figure 6: Cross Section illustrating Drill Hole BR-18-20

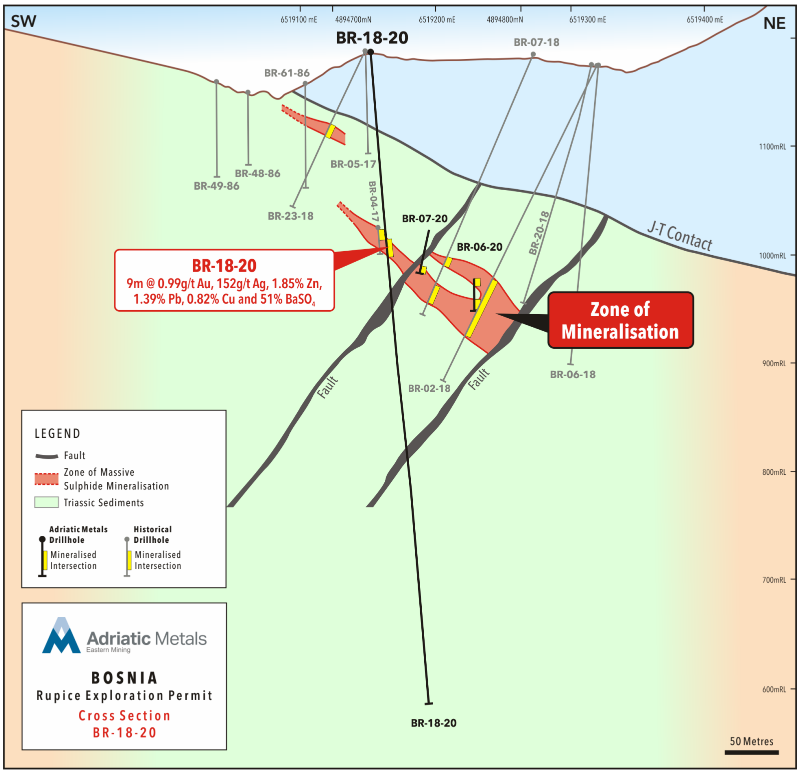


Figure 7: Cross Section illustrating Drill Hole BR-20-20

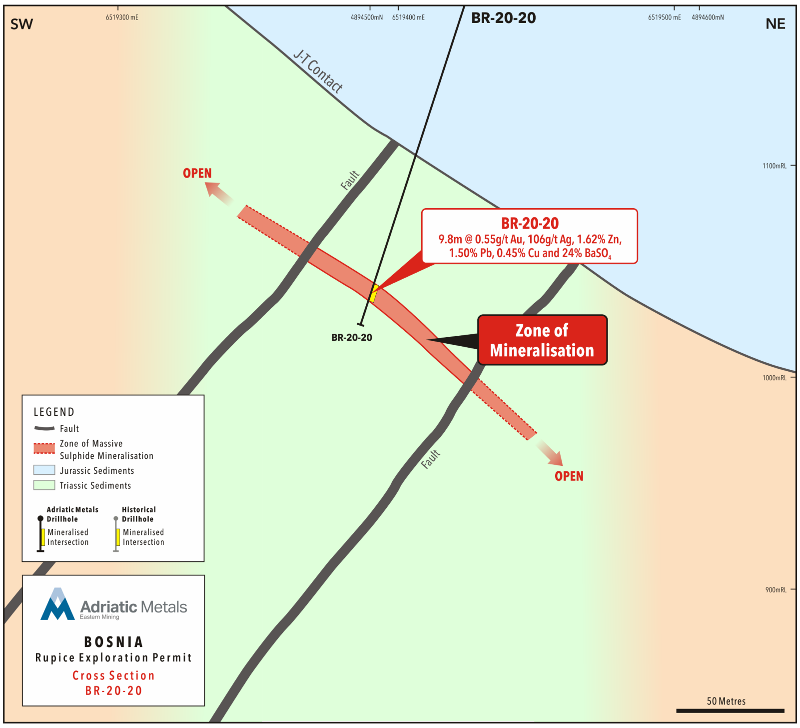
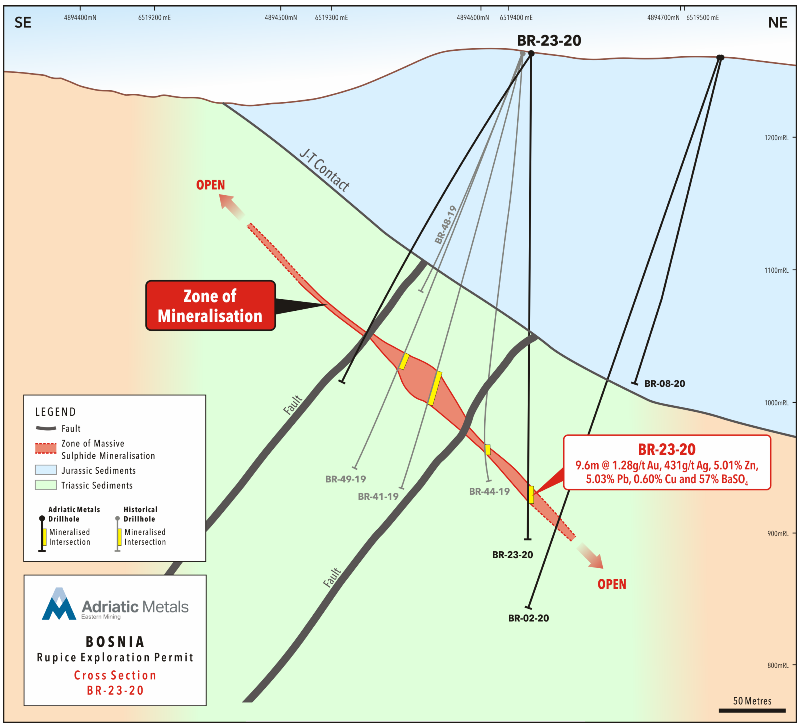


Figure 8: Cross Section illustrating Drill Hole BR-23-20



Drilling at Jurasevac-Brestic was also conducted, designed to test the gravity anomaly defined after data reprocessing in March this year. Five diamond drill holes targeted the main gravity high, and massive and patchy pyrite, and weak lead, zinc and barite mineralisation was encountered. Drilling proved the validity of the gravity anomaly, however, economic mineralisation has not been encountered so far.

Exploration and hydrological drilling works continue on the Vares Silver Project with two rigs testing the mineralisation further southward at Rupice, and one at Veovaca drilling geotechnical and hydrological holes. More drillholes are planned for testing the extensions of Rupice deposit to the south and down-dip.

Authorised by, and for further information, please contact:

Paul Cronin

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MARKET ABUSE REGULATION DISCLOSURE

The information contained within this announcement is deemed by the Company (LEI: 549300OHAH2GL1DP0L61) to constitute inside information as stipulated under the Market Abuse Regulations (EU) No. 596/2014. The person responsible for arranging and authorising the release of this announcement on behalf of the Company is Paul Cronin, Managing Director and CEO.

For further information please visit www.adriaticmetals.com, @AdriaticMetals on Twitter, or contact:

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COMPETENT PERSONS REPORT

The information in this report that relates to the Mineral Resources is based on and fairly represents information and supporting information compiled by Dmitry Pertel. Dmitry Pertel is a full-time employee of CSA Global and is a Member of the Australian Institute of Geoscientists. Dmitry Pertel has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the Australasian Code for the Reporting of Exploration Results, Mineral Resources, and Ore Reserves (JORC Code). Dmitry Pertel consents to the disclosure of information in this report in the form and context in which it appears.

The information in this report which relates to Exploration Results is based on and fairly represents information and supporting information compiled by Mr Phillip Fox, who is a member of the Australian Institute of Geoscientists (AIG). Mr Fox is a consultant to Adriatic Metals Plc, and has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activity he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the "Australian Code of Reporting of Exploration Results, Mineral Resources and Ore Reserves". Mr Fox consents to the inclusion in this report of the matters based on that information in the form and context in which it appears.

ABOUT ADRIATIC METALS

Adriatic Metals Plc (ASX:ADT, LSE:ADT1) is a precious and base metals explorer and developer that owns the world-class advanced Vares Silver Project in Bosnia & Herzegovina.

The Vares Silver Project consists of two high-grade deposits, located at Rupice and Veovaca. Bosnia & Herzegovina is well-positioned in central Europe and boasts a strong mining history, pro-mining environment, highly-skilled workforce as well as extensive existing infrastructure and logistics.

The Vares Silver Project's captivating economics and impressive resource inventory have attracted Adriatic's highly experienced team, which is expediting efforts to fast-track the project to production. Results of from the 2019 scoping study indicate an NPV8 of US$917 million and IRR of 107%. Leveraging its first-mover advantage, Adriatic is rapidly advancing the project into the development phase and through to production. There have been no material adverse changes in the assumptions underpinning the forecast financial information or material assumptions and technical parameters underpinning the Maiden Mineral Resource estimate since the original relevant market announcements which continue to apply.

DISCLAIMER

Table 3 – Collar Information for reported drill holes (MGI Balkans Z6)

Drill Hole	Easting	Northing	Elevation	Average Azimuth (TN)	Average Dip	Depth (m)
BR-10-20	6519271	4894736	1206	58	-85	373.6
BR-11-20	6519241	4894518	1212	226	-61	184.0
BR-12-20	6519275	4894592	1217	227	-55	130.1
BR-13-20	6519275	4894592	1217	228	-71	155.2
BR-17-20	6519079	4894785	1162	54	-73	498.5
BR-18-20	6519151	4894717	1187	64	-85	607.0
BR-20-20	6519446	4894547	1265	231	-73	252.2
BR-22-20	6519216	4894898	1124	149	-86	312.7
BR-23-20	6519411	4894627	1264	223	-90	368.0

Table 4 - Assay Results for reported drill holes

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-10-20	0	1	1	0.0054	0.0011	0.0025	<0.5	0.0044	0.015
BR-10-20	1	2.5	1.5	0.0071	0.001	<0.005	<0.5	0.0044	0.015
BR-10-20	2.5	4.5	2	0.0166	0.0053	<0.005	<0.5	0.0034	0.015
BR-10-20	4.5	6.5	2	0.008	0.0026	<0.005	<0.5	0.0027	0.015
BR-10-20	6.5	7.5	1	0.0055	0.0012	0.008	<0.5	0.0038	0.015
BR-10-20	7.5	9.5	2	0.01	0.001	<0.005	<0.5	0.0045	0.015
BR-10-20	9.5	11.5	2	0.0164	0.0015	<0.005	<0.5	0.0042	0.015
BR-10-20	11.5	13.5	2	0.019	0.0059	<0.005	<0.5	0.0038	0.015
BR-10-20	13.5	14.4	0.9	0.0257	0.0092	<0.005	<0.5	0.0037	0.015
BR-10-20	14.4	16.4	2	0.0075	0.0062	<0.005	<0.5	0.0015	0.015
BR-10-20	16.4	17.6	1.2	0.0079	0.0068	<0.005	<0.5	0.0022	0.015
BR-10-20	17.6	19	1.4	0.0139	0.0167	0.005	<0.5	0.006	0.03
BR-10-20	19	21	2	0.0174	0.0327	0.011	<0.5	0.0048	0.015
BR-10-20	21	23	2	0.0112	0.0217	<0.005	<0.5	0.003	0.015
BR-10-20	23	25	2	0.006	0.0045	0.006	<0.5	0.0035	0.03
BR-10-20	25	27	2	0.0103	0.0195	<0.005	<0.5	0.0037	0.03
BR-10-20	27	28.2	1.2	0.0101	0.0224	0.007	<0.5	0.0041	0.03
BR-10-20	28.2	30	1.8	0.0088	0.0122	0.005	<0.5	0.0036	0.015
BR-10-20	30	32	2	0.0083	0.0101	0.007	<0.5	0.004	0.03
BR-10-20	32	34	2	0.0081	0.0107	0.01	<0.5	0.0037	0.015
BR-10-20	34	36	2	0.0075	0.0176	0.005	<0.5	0.0038	0.015
BR-10-20	36	38	2	0.0086	0.0212	<0.005	<0.5	0.0042	0.015
BR-10-20	38	40	2	0.01	0.0091	0.006	<0.5	0.0057	0.015
BR-10-20	40	42	2	0.027	0.0222	0.005	<0.5	0.0041	0.015
BR-10-20	42	43.3	1.3	0.0292	0.0276	<0.005	<0.5	0.0032	0.015
BR-10-20	43.3	44.9	1.6	0.0132	0.0426	<0.005	<0.5	0.0067	0.03
BR-10-20	44.9	46	1.1	0.0138	0.0169	<0.005	<0.5	0.0021	0.015
BR-10-20	46	48	2	0.0234	0.0155	0.006	<0.5	0.0039	0.015
BR-10-20	48	50	2	0.0227	0.0231	<0.005	<0.5	0.003	0.03
BR-10-20	50	51.9	1.9	0.0124	0.0121	<0.005	<0.5	0.0013	0.046
BR-10-20	51.9	53	1.1	0.0094	0.0098	<0.005	<0.5	0.0011	0.015
BR-10-20	53	55	2	0.0109	0.0371	<0.005	<0.5	0.0033	0.03
BR-10-20	55	57	2	0.0066	0.0042	<0.005	<0.5	0.0017	0.03
BR-10-20	57	59	2	0.0231	0.0244	<0.005	<0.5	0.0128	0.046

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-10-20	59	60.3	1.3	0.0528	0.0179	0.005	<0.5	0.0033	0.046
BR-10-20	60.3	63.2	2.9	No sample					
BR-10-20	63.2	65	1.8	0.0067	0.0132	<0.005	<0.5	0.012	0.106
BR-10-20	65	67	2	0.0095	0.0232	0.011	<0.5	0.0063	0.213
BR-10-20	67	69	2	0.0067	0.0175	0.008	<0.5	0.0031	0.061
BR-10-20	69	71	2	0.0063	0.0061	0.009	<0.5	0.0041	0.046
BR-10-20	71	73	2	0.0055	0.0036	<0.005	<0.5	0.0026	0.046
BR-10-20	73	74.4	1.4	0.0101	0.0115	<0.005	<0.5	0.0037	0.046
BR-10-20	74.4	74.9	0.5	No sample					
BR-10-20	74.9	76.6	1.7	0.0074	0.0059	0.005	<0.5	0.0042	0.03
BR-10-20	76.6	78	1.4	0.0175	0.0069	0.007	<0.5	0.0117	0.046
BR-10-20	78	80	2	0.0119	0.0055	<0.005	<0.5	0.0059	0.03
BR-10-20	80	82	2	0.0153	0.0076	<0.005	<0.5	0.0057	0.03
BR-10-20	82	84	2	0.0266	0.0434	0.006	<0.5	0.0096	0.03
BR-10-20	84	85	1	0.0182	0.0282	<0.005	<0.5	0.0083	0.046
BR-10-20	85	86.5	1.5	0.0179	0.0136	0.006	0.5	0.0091	0.03
BR-10-20	86.5	88	1.5	0.0195	0.0029	0.006	<0.5	0.0073	0.03
BR-10-20	88	90	2	0.0114	0.0063	0.011	<0.5	0.0078	0.03
BR-10-20	90	91.4	1.4	0.0119	0.0079	0.008	<0.5	0.0082	0.015
BR-10-20	91.4	93	1.6	0.0139	0.0048	0.008	<0.5	0.0068	0.03
BR-10-20	93	95	2	0.0117	0.0035	<0.005	<0.5	0.0046	0.03
BR-10-20	95	95.9	0.9	0.0109	0.0026	<0.005	<0.5	0.0041	0.015
BR-10-20	95.9	97	1.1	0.0082	0.0021	<0.005	<0.5	0.0027	0.015
BR-10-20	97	99	2	0.0087	0.002	<0.005	<0.5	0.0024	0.015
BR-10-20	99	100.7	1.7	0.0094	0.003	0.007	<0.5	<0.005	0.015
BR-10-20	100.7	102	1.3	0.0072	0.0065	<0.005	<0.5	0.0021	0.015
BR-10-20	102	104	2	0.0097	0.0071	<0.005	<0.5	0.0013	0.015
BR-10-20	104	106	2	0.0097	0.007	<0.005	<0.5	0.0014	0.015
BR-10-20	106	108	2	0.0113	0.0087	<0.005	<0.5	0.002	0.015
BR-10-20	108	110	2	0.0141	0.0095	<0.005	<0.5	0.0023	0.015
BR-10-20	110	111	1	0.0247	0.0121	<0.005	<0.5	0.0039	0.03
BR-10-20	111	112.2	1.2	0.0234	0.0271	<0.005	<0.5	0.0048	0.046
BR-10-20	112.2	117.8	5.6	No sample					
BR-10-20	117.8	119	1.2	0.0778	0.0479	0.007	1	0.0286	0.046
BR-10-20	119	121	2	0.0368	0.0942	<0.005	0.6	0.009	0.228
BR-10-20	121	123	2	0.0144	0.0353	<0.005	<0.5	0.0014	0.015
BR-10-20	123	125	2	0.0119	0.038	<0.005	<0.5	0.0009	0.015
BR-10-20	125	127	2	0.006	0.0524	<0.005	<0.5	0.001	0.076
BR-10-20	127	129	2	0.0226	0.172	0.005	1.1	0.0155	0.015
BR-10-20	129	131	2	0.0303	0.2	<0.005	1.3	0.0091	0.03
BR-10-20	131	132.8	1.8	0.0318	0.15	<0.005	1.2	0.0037	0.03
BR-10-20	132.8	134	1.2	0.0164	0.0563	<0.005	<0.5	0.004	0.046
BR-10-20	134	136	2	0.0229	0.0501	<0.005	<0.5	<0.005	0.061
BR-10-20	136	138	2	0.012	0.0428	<0.005	0.6	0.0024	0.061
BR-10-20	138	138.5	0.5	0.0123	0.0942	<0.005	<0.5	0.0024	0.03
BR-10-20	138.5	139	0.5	No sample					
BR-10-20	139	141	2	0.0148	0.028	<0.005	<0.5	0.0008	0.015
BR-10-20	141	143	2	0.0178	0.0226	<0.005	<0.5	0.0009	0.015
BR-10-20	143	145	2	0.0134	0.0331	<0.005	<0.5	0.0015	0.046
BR-10-20	145	147	2	0.0103	0.0088	<0.005	<0.5	0.0007	0.137
BR-10-20	147	149	2	0.0195	0.005	<0.005	<0.5	0.0021	0.137

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-10-20	149	151	2	0.0191	0.0047	<0.005	<0.5	0.0021	0.091
BR-10-20	151	153	2	0.0122	0.0032	<0.005	<0.5	0.0016	0.548
BR-10-20	153	153.8	0.8	0.018	0.0066	<0.005	<0.5	<0.005	0.046
BR-10-20	153.8	155	1.2	0.0105	0.0035	<0.005	<0.5	0.0018	0.03
BR-10-20	155	157	2	0.0287	0.008	<0.005	<0.5	0.0021	0.03
BR-10-20	157	159	2	0.0127	0.0043	<0.005	<0.5	0.0019	0.061
BR-10-20	159	161	2	0.0157	0.004	<0.005	<0.5	0.0024	0.137
BR-10-20	161	162.2	1.2	0.0079	0.001	0.009	<0.5	0.0013	0.213
BR-10-20	162.2	164	1.8	0.0085	0.0003	<0.005	<0.5	0.0003	0.106
BR-10-20	164	165.6	1.6	0.0094	0.0011	0.04	<0.5	0.0033	0.106
BR-10-20	165.6	167	1.4	0.0093	0.0044	0.014	1.8	0.0109	0.669
BR-10-20	167	169	2	0.017	0.005	<0.005	<0.5	0.0015	0.715
BR-10-20	169	171	2	0.0267	0.0026	<0.005	<0.5	0.0013	0.73
BR-10-20	171	173	2	0.043	0.0651	<0.005	1.7	0.0055	0.167
BR-10-20	173	175	2	0.0526	0.123	0.005	1.9	0.0067	0.548
BR-10-20	175	175.9	0.9	0.0059	<0.005	0.013	<0.5	0.001	0.335
BR-10-20	175.9	177	1.1	0.0114	0.0012	<0.005	<0.5	0.0007	0.167
BR-10-20	177	178.4	1.4	0.0131	0.0022	0.01	<0.5	0.002	0.472
BR-10-20	178.4	180	1.6	0.0429	0.0078	0.014	0.6	0.0027	0.183
BR-10-20	180	182	2	0.0167	0.0082	0.026	1.1	0.0019	0.228
BR-10-20	182	184	2	0.0311	0.0102	0.029	2.3	0.0017	0.38
BR-10-20	184	186	2	0.0796	0.0727	0.047	5.2	0.0064	0.304
BR-10-20	186	188	2	0.0557	0.0348	0.033	23.3	0.0083	0.487
BR-10-20	188	189.9	1.9	0.241	0.0682	0.034	15.7	0.0068	0.593
BR-10-20	189.9	191	1.1	0.0832	0.0343	0.012	3.6	0.0119	0.487
BR-10-20	191	192	1	0.0088	0.004	0.032	0.7	0.0016	0.152
BR-10-20	192	193	1	0.0116	0.0045	0.027	0.5	0.0015	1.034
BR-10-20	193	194	1	0.01	0.0054	0.013	0.6	0.0032	0.441
BR-10-20	194	195	1	0.0106	0.016	0.013	0.7	0.004	0.487
BR-10-20	195	196	1	0.0086	0.0413	<0.005	0.5	0.0034	1.156
BR-10-20	196	197	1	0.0147	0.0103	<0.005	2.3	0.0036	0.228
BR-10-20	197	198	1	0.0082	0.0018	0.007	1	0.001	0.046
BR-10-20	198	199	1	0.217	0.127	0.028	6.5	0.0088	8.276
BR-10-20	199	200	1	0.0192	0.017	0.02	6.6	0.0263	1.491
BR-10-20	200	201	1	0.0091	0.0064	<0.005	1.4	0.0009	1.004
BR-10-20	201	202	1	0.0427	0.0281	0.021	3	0.0045	0.517
BR-10-20	202	203	1	0.0331	0.493	0.165	13.2	0.13	0.578
BR-10-20	203	204	1	0.022	0.0195	0.172	1.1	0.002	0.213
BR-10-20	204	205	1	1.295	0.615	0.354	7.3	0.0351	0.456
BR-10-20	205	206	1	3.6	1.86	0.545	24.8	0.101	0.198
BR-10-20	206	206.9	0.9	0.0594	0.034	0.027	1.5	0.0022	0.806
BR-10-20	206.9	208	1.1	0.0139	0.0235	0.095	0.5	0.0028	1.78
BR-10-20	208	209	1	0.0261	0.0139	0.06	<0.5	0.0021	0.061
BR-10-20	209	210	1	0.0265	0.0088	0.032	<0.5	0.0104	0.152
BR-10-20	210	211	1	0.0109	0.0105	0.037	<0.5	0.002	0.046
BR-10-20	211	212	1	0.024	0.0069	0.027	<0.5	0.0012	0.046
BR-10-20	212	213	1	0.0113	0.0275	0.023	<0.5	0.0028	0.046
BR-10-20	213	214	1	0.038	0.222	0.031	1.5	0.0099	0.03
BR-10-20	214	215	1	0.0403	0.288	0.049	2	0.0071	0.061
BR-10-20	215	216	1	0.0451	0.0182	0.055	<0.5	0.002	0.183
BR-10-20	216	217	1	0.0619	0.0137	0.026	<0.5	0.0013	0.091

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-10-20	217	218	1	0.0847	0.014	0.034	<0.5	0.0016	0.076
BR-10-20	218	219	1	0.0963	0.015	0.187	0.8	0.0033	0.046
BR-10-20	219	220	1	0.173	0.007	0.189	1.2	0.0068	0.015
BR-10-20	220	221	1	0.0986	0.007	0.183	1.4	0.005	0.03
BR-10-20	221	222	1	0.13	0.0075	0.194	1.3	0.0048	0.015
BR-10-20	222	223	1	0.124	0.0062	0.152	0.7	0.0029	0.015
BR-10-20	223	224	1	0.682	0.0389	0.688	10.9	0.119	0.015
BR-10-20	224	225	1	0.0527	0.0086	0.167	1.8	0.0169	0.015
BR-10-20	225	226	1	0.161	0.0126	0.272	2.8	0.0113	0.03
BR-10-20	226	227	1	0.813	0.057	0.764	12.4	0.348	0.122
BR-10-20	227	228	1	0.435	0.0548	0.216	3.2	0.0336	0.35
BR-10-20	228	229	1	0.514	0.081	0.235	3.7	0.0413	0.03
BR-10-20	229	230	1	0.0689	0.0583	0.11	1.5	0.0118	0.472
BR-10-20	230	231	1	0.0708	0.0048	0.042	<0.5	0.0015	0.578
BR-10-20	231	232	1	0.0466	0.0047	0.056	0.5	0.0036	0.106
BR-10-20	232	233	1	0.0435	<0.005	0.063	<0.5	0.0015	0.03
BR-10-20	233	234	1	0.0359	0.0345	0.069	0.5	0.0043	0.015
BR-10-20	234	235	1	0.0402	0.0097	0.056	0.7	0.0017	1.171
BR-10-20	235	236	1	0.0195	0.028	0.116	0.6	0.0027	0.061
BR-10-20	236	237	1	0.0113	0.0069	0.086	<0.5	0.0016	0.015
BR-10-20	237	238	1	0.0181	0.0049	0.095	<0.5	0.0015	0.015
BR-10-20	238	239	1	0.0534	0.0051	0.039	<0.5	0.001	0.03
BR-10-20	239	240	1	0.0118	0.0093	0.051	<0.5	0.0103	0.03
BR-10-20	240	241	1	0.0279	0.0108	0.055	0.5	0.0022	0.243
BR-10-20	241	242	1	0.0198	0.0259	0.009	<0.5	0.0004	0.03
BR-10-20	242	243	1	0.0037	0.0106	0.026	<0.5	0.0002	0.061
BR-10-20	243	244	1	0.154	0.0414	0.026	<0.5	0.0411	2.601
BR-10-20	244	244.8	0.8	0.0384	0.0066	0.012	<0.5	0.0007	0.289
BR-10-20	244.8	246	1.2	0.0234	0.006	0.016	<0.5	0.0017	0.03
BR-10-20	246	247.3	1.3	0.022	0.0005	<0.005	<0.5	0.0004	0.015
BR-10-20	247.3	249	1.7	0.013	0.0006	<0.005	<0.5	0.0008	0.008
BR-10-20	249	251	2	0.0161	0.0008	<0.005	<0.5	0.0002	0.015
BR-10-20	251	253	2	0.0113	0.0005	0.012	<0.5	0.0001	0.008
BR-10-20	253	255	2	0.0165	0.0008	0.007	<0.5	0.0002	0.061
BR-10-20	255	257	2	0.017	0.0005	0.007	<0.5	0.0001	0.008
BR-10-20	257	258.3	1.3	0.0226	0.0004	<0.005	<0.5	0.0001	0.008
BR-10-20	258.3	260	1.7	0.0179	0.0011	<0.005	<0.5	0.001	0.008
BR-10-20	260	262	2	0.0272	0.002	<0.005	<0.5	0.0511	0.046
BR-10-20	262	262.5	0.5	0.0189	0.0007	<0.005	<0.5	0.0002	0.03
BR-10-20	262.5	264	1.5	0.0165	0.0006	<0.005	<0.5	0.0002	0.03
BR-10-20	264	266	2	0.0491	0.001	<0.005	<0.5	0.0006	0.061
BR-10-20	266	266.9	0.9	0.0096	0.001	<0.005	<0.5	0.0008	0.046
BR-10-20	266.9	268	1.1	0.0156	0.0008	<0.005	<0.5	0.0011	0.03
BR-10-20	268	270	2	0.0138	0.0007	0.005	<0.5	0.0023	0.046
BR-10-20	270	272	2	0.0223	0.001	<0.005	<0.5	0.0007	0.015
BR-10-20	272	273.4	1.4	0.0146	0.0008	<0.005	<0.5	0.0003	0.015
BR-10-20	273.4	275	1.6	0.0113	0.0007	<0.005	<0.5	0.0005	0.046
BR-10-20	275	277	2	0.0106	0.0012	<0.005	<0.5	0.0002	0.046
BR-10-20	277	279	2	0.0093	0.0008	<0.005	<0.5	0.0002	0.046
BR-10-20	279	281	2	0.0109	0.0004	<0.005	<0.5	0.0001	0.03
BR-10-20	281	283	2	0.0111	0.0004	<0.005	<0.5	0.0001	0.046

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-10-20	283	283.8	0.8	0.0106	0.0008	<0.005	<0.5	0.0001	0.046
BR-10-20	283.8	285	1.2	0.0123	0.0005	<0.005	<0.5	0.0001	0.03
BR-10-20	285	287	2	0.0082	0.0007	<0.005	<0.5	0.0001	0.122
BR-10-20	287	289	2	0.0073	0.001	<0.005	<0.5	0.0017	0.38
BR-10-20	289	291	2	0.0241	0.0017	0.007	<0.5	0.0003	0.122
BR-10-20	291	293	2	0.0192	0.0098	0.048	1.6	0.0045	0.274
BR-10-20	293	294	1	0.014	0.0107	0.037	1.3	0.0023	0.289
BR-10-20	294	295	1	0.0133	0.0056	0.013	0.7	0.0046	0.152
BR-10-20	295	296	1	0.104	0.0503	0.068	3.1	0.0036	0.259
BR-10-20	296	297	1	0.0526	0.0683	0.033	4.5	0.0078	0.243
BR-10-20	297	298	1	0.262	0.18	0.112	7.9	0.0121	0.046
BR-10-20	298	299	1	0.331	0.124	0.174	8.6	0.0139	0.183
BR-10-20	299	300	1	0.191	0.0993	0.066	3.7	0.0054	0.137
BR-10-20	300	301	1	0.0702	0.0156	0.071	2.8	0.0032	0.076
BR-10-20	301	302	1	0.373	0.079	0.122	3.2	0.0051	0.152
BR-10-20	302	303	1	0.0253	0.0047	0.024	1.3	0.0008	0.061
BR-10-20	303	304	1	0.159	0.251	0.085	4.5	0.0063	0.578
BR-10-20	304	305	1	0.235	0.135	0.049	3.5	0.0072	0.365
BR-10-20	305	306	1	0.254	0.345	0.106	6.4	0.0228	0.517
BR-10-20	306	307.2	1.2	0.0908	0.0632	0.078	2.9	0.0091	0.517
BR-10-20	307.2	308.4	1.2	0.135	0.0273	0.021	1.4	0.0009	0.198
BR-10-20	308.4	309.4	1	0.0472	0.0573	0.044	2.4	0.0015	0.882
BR-10-20	309.4	310.6	1.2	0.308	0.114	0.051	4	0.003	0.38
BR-10-20	310.6	311.7	1.1	0.132	0.0393	0.042	4.3	0.0049	0.289
BR-10-20	311.7	312.8	1.1	0.264	0.133	0.08	14	0.0191	0.943
BR-10-20	312.8	314	1.2	0.363	0.324	0.133	23	0.0344	1.978
BR-10-20	314	315	1	0.183	0.0626	0.08	5	0.0065	0.608
BR-10-20	315	316.2	1.2	0.127	0.0218	0.031	1.4	0.0019	0.106
BR-10-20	316.2	317.4	1.2	0.416	0.181	0.119	7.8	0.0217	0.35
BR-10-20	317.4	318.6	1.2	0.29	0.178	0.142	28.4	0.0907	0.152
BR-10-20	318.6	319.8	1.2	0.145	0.0964	0.138	12.7	0.0604	0.091
BR-10-20	319.8	321	1.2	0.599	0.608	0.195	14.4	0.0714	0.548
BR-10-20	321	322	1	0.742	0.432	0.319	18.1	0.0746	0.335
BR-10-20	322	323.2	1.2	0.478	0.224	0.161	6.3	0.015	0.593
BR-10-20	323.2	324	0.8	0.0914	0.0216	0.036	1.2	0.005	0.228
BR-10-20	324	325	1	0.0524	0.0238	0.063	1.1	0.0095	0.396
BR-10-20	325	326	1	0.101	0.0769	0.04	1.3	0.0045	0.685
BR-10-20	326	327	1	0.149	0.0196	0.058	0.7	0.0019	0.137
BR-10-20	327	328	1	0.127	0.0802	0.165	3.9	0.0501	0.608
BR-10-20	328	329	1	0.0658	0.0779	0.104	1.9	0.0155	0.274
BR-10-20	329	330	1	0.0294	0.0806	0.158	1.3	0.0086	0.076
BR-10-20	330	331	1	0.0714	0.0215	0.088	1	0.0051	0.091
BR-10-20	331	332	1	0.0487	0.071	0.075	1.6	0.0143	0.198
BR-10-20	332	333	1	0.0316	0.0447	0.058	1	0.0047	0.122
BR-10-20	333	334	1	0.211	0.317	0.322	6.9	0.108	1.4
BR-10-20	334	335	1	0.142	0.452	0.178	6.5	0.0792	0.487
BR-10-20	335	336	1	0.281	0.653	0.121	9	0.13	0.974
BR-10-20	336	337	1	0.0504	0.0131	0.051	<0.5	0.0014	0.152
BR-10-20	337	338	1	0.148	0.0659	0.081	1.4	0.0121	0.076
BR-10-20	338	339	1	0.249	0.453	1.655	7.9	0.112	0.091
BR-10-20	339	340	1	0.223	0.311	0.164	13.1	0.296	1.993

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-10-20	340	341	1	0.264	0.213	0.29	3.8	0.0657	0.532
BR-10-20	341	342	1	0.028	0.0188	0.093	0.5	0.0073	0.091
BR-10-20	342	343.8	1.8	0.0086	0.0075	0.037	<0.5	0.0004	0.061
BR-10-20	343.8	345	1.2	0.0171	0.0623	0.025	0.6	0.0023	0.061
BR-10-20	345	347	2	0.0795	0.035	0.023	1.4	0.0067	0.259
BR-10-20	347	349	2	0.168	0.0828	0.007	2.7	0.0033	0.654
BR-10-20	349	351	2	0.0095	0.0013	<0.005	0.6	0.0028	0.532
BR-10-20	351	353	2	0.0085	0.0008	<0.005	<0.5	0.0003	0.152
BR-10-20	353	355	2	0.0104	0.0007	<0.005	<0.5	0.0005	0.198
BR-10-20	355	357	2	0.0096	0.0014	<0.005	0.8	0.0034	0.091
BR-10-20	357	359	2	0.0111	0.0015	<0.005	0.6	0.0014	0.198
BR-10-20	359	361	2	0.0099	0.0014	<0.005	1.4	0.0044	0.213
BR-10-20	361	363	2	0.0106	0.0012	<0.005	<0.5	0.0003	0.167
BR-10-20	363	365	2	0.011	0.0011	<0.005	<0.5	0.0005	0.122
BR-10-20	365	367	2	0.0114	0.002	<0.005	3.7	0.0093	0.228
BR-10-20	367	369	2	0.0118	0.0015	<0.005	1.4	0.004	0.274
BR-10-20	369	371	2	0.0124	0.0032	<0.005	0.9	0.0006	0.152
BR-10-20	371	373	2	0.0117	0.0013	<0.005	0.8	0.0005	0.152
BR-10-20	373	373.6	0.6	0.012	0.0051	<0.005	1.2	0.0005	0.243

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-11-20	0	1.8	1.8	0.0263	0.019	0.01	<0.5	0.0082	0.076
BR-11-20	1.8	3	1.2	0.0037	0.0015	<0.005	<0.5	0.0021	0.015
BR-11-20	3	5	2	0.0038	0.0015	<0.005	<0.5	0.0018	0.008
BR-11-20	5	6.5	1.5	No sample					
BR-11-20	6.5	8.1	1.6	0.006	0.0085	<0.005	<0.5	0.005	0.015
BR-11-20	8.1	10	1.9	0.0297	0.263	0.005	5.5	0.024	0.046
BR-11-20	10	11.3	1.3	0.0243	0.197	0.006	1.5	0.0102	0.076
BR-11-20	11.3	12.6	1.3	0.0138	0.0059	<0.005	<0.5	0.0006	0.03
BR-11-20	12.6	13.5	0.9	No sample					
BR-11-20	13.5	15	1.5	0.0103	0.0023	<0.005	<0.5	0.002	0.03
BR-11-20	15	15.7	0.7	0.011	0.0033	<0.005	<0.5	0.0017	0.015
BR-11-20	15.7	17	1.3	0.0121	0.0035	<0.005	<0.5	0.0019	0.015
BR-11-20	17	18.4	1.4	0.0122	0.0029	<0.005	<0.5	0.0005	0.015
BR-11-20	18.4	20	1.6	0.0075	0.0013	<0.005	<0.5	0.0001	0.03
BR-11-20	20	22	2	0.0122	0.0012	<0.005	<0.5	<0.0001	0.046
BR-11-20	22	24	2	0.0069	0.001	<0.005	<0.5	<0.0001	0.03
BR-11-20	24	26	2	0.0101	0.0045	0.007	<0.5	0.0057	0.015
BR-11-20	26	28	2	0.0085	0.0125	<0.005	<0.5	<0.005	0.03
BR-11-20	28	30	2	0.0101	0.0017	<0.005	<0.5	0.0003	0.03
BR-11-20	30	31	1	0.0099	0.0013	<0.005	<0.5	0.0003	0.015
BR-11-20	31	32.3	1.3	0.0093	0.0034	<0.005	<0.5	0.0035	0.015
BR-11-20	32.3	34	1.7	0.0107	0.0023	<0.005	<0.5	0.0002	0.076
BR-11-20	34	35.5	1.5	0.0113	0.0024	<0.005	<0.5	0.0001	0.03
BR-11-20	35.5	37	1.5	0.0121	0.0022	<0.005	<0.5	0.0063	0.03
BR-11-20	37	39	2	0.0172	0.0036	<0.005	<0.5	0.0003	0.106
BR-11-20	39	41	2	0.0147	0.0018	<0.005	<0.5	0.0001	0.03
BR-11-20	41	43	2	0.0129	0.002	<0.005	<0.5	<0.0001	0.061
BR-11-20	43	45	2	0.0123	0.0018	<0.005	<0.5	0.0009	0.046
BR-11-20	45	47	2	0.013	0.0015	<0.005	<0.5	0.0042	0.061
BR-11-20	47	49	2	0.0102	0.0015	<0.005	<0.5	0.0001	0.076

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-11-20	49	50.2	1.2	0.0097	0.0011	<0.005	<0.5	0.0001	0.046
BR-11-20	50.2	52	1.8	0.0103	0.0011	<0.005	0.5	0.0002	0.061
BR-11-20	52	53	1	0.018	0.0015	<0.005	2	0.0017	0.137
BR-11-20	53	55	2	0.0094	0.0013	<0.005	<0.5	0.0004	0.122
BR-11-20	55	56.5	1.5	0.0095	0.0009	<0.005	<0.5	0.0002	0.076
BR-11-20	56.5	57.5	1	0.171	0.0336	<0.005	0.7	0.0035	0.091
BR-11-20	57.5	58.6	1.1	0.0917	0.0184	0.008	5	0.0022	0.837
BR-11-20	58.6	59.6	1	0.137	0.0436	0.043	18	0.0087	2.115
BR-11-20	59.6	60.6	1	0.371	0.13	0.078	134	0.002	12.368
BR-11-20	60.6	61.6	1	0.15	0.0949	0.057	27.2	0.0012	5.811
BR-11-20	61.6	62.2	0.6	0.115	0.0715	0.226	10.1	0.0385	15.669
BR-11-20	62.2	63.2	1	2.22	2.86	0.596	204	0.567	75.149
BR-11-20	63.2	64.2	1	1.145	1.18	0.534	120	1.07	86.559
BR-11-20	64.2	64.8	0.6	3.09	3.42	1.925	283	0.778	83.212
BR-11-20	64.8	65.6	0.8	0.0621	0.0913	0.093	9.6	0.0362	7.454
BR-11-20	65.6	65.9	0.3	4.42	3.76	1.165	303	0.582	81.082
BR-11-20	65.9	67	1.1	1.315	0.926	0.43	118	0.133	23.883
BR-11-20	67	68	1	0.0795	0.0599	0.028	1.4	0.0193	0.593
BR-11-20	68	68.5	0.5	0.0276	0.0558	0.028	0.8	0.0075	0.228
BR-11-20	68.5	69.2	0.7	0.0255	0.0544	0.042	0.5	0.0276	0.73
BR-11-20	69.2	71	1.8	0.0041	0.0015	<0.005	<0.5	0.001	0.03
BR-11-20	71	73	2	0.0062	0.0017	<0.005	<0.5	0.002	0.015
BR-11-20	73	75	2	0.0044	0.0012	<0.005	<0.5	0.0008	0.03
BR-11-20	75	76	1	0.0114	0.0036	<0.005	<0.5	0.008	0.015
BR-11-20	76	77.3	1.3	0.0116	0.0938	<0.005	<0.5	0.0397	0.046
BR-11-20	77.3	79	1.7	0.0041	0.0041	<0.005	<0.5	0.0029	0.046
BR-11-20	79	81	2	0.0041	0.0007	<0.005	<0.5	0.0021	0.015
BR-11-20	81	83	2	0.0061	0.0007	<0.005	<0.5	0.0018	0.015
BR-11-20	83	85	2	0.0037	0.0005	<0.005	<0.5	0.0018	0.015
BR-11-20	85	87	2	0.0053	<0.005	<0.005	<0.5	0.0019	0.015
BR-11-20	87	89	2	0.0074	0.0023	<0.005	<0.5	0.001	0.046
BR-11-20	89	91	2	0.0052	0.0017	0.006	<0.5	0.001	0.03
BR-11-20	91	93	2	0.0053	0.001	<0.005	<0.5	0.0017	0.046
BR-11-20	93	95	2	0.0065	0.002	<0.005	<0.5	0.002	0.046
BR-11-20	95	97	2	0.0077	0.0048	<0.005	<0.5	0.0029	0.015
BR-11-20	97	99	2	0.0062	0.0038	<0.005	<0.5	0.0019	0.259
BR-11-20	99	100	1	0.006	0.0037	<0.005	<0.5	0.0021	0.03
BR-11-20	100	102	2	0.0059	0.0017	<0.005	<0.5	0.0011	0.015
BR-11-20	102	104	2	0.0088	0.0018	<0.005	<0.5	0.0009	0.015
BR-11-20	104	106	2	0.009	0.0012	<0.005	<0.5	0.0014	0.03
BR-11-20	106	108	2	0.0052	0.0019	<0.005	<0.5	0.0016	0.03
BR-11-20	108	110	2	0.008	0.0021	<0.005	<0.5	0.0012	0.015
BR-11-20	110	112	2	0.0104	0.0016	<0.005	<0.5	0.0022	0.03
BR-11-20	112	114	2	0.0078	0.002	<0.005	<0.5	0.0013	0.03
BR-11-20	114	116	2	0.0074	0.002	<0.005	<0.5	0.0009	0.243
BR-11-20	116	118	2	0.0072	0.0027	<0.005	<0.5	0.0017	0.015
BR-11-20	118	120	2	0.0189	0.0014	<0.005	<0.5	0.0011	0.183
BR-11-20	120	122	2	0.0107	0.0021	<0.005	<0.5	0.0013	0.03
BR-11-20	122	123.8	1.8	0.0068	0.0063	<0.005	<0.5	0.0021	0.046
BR-11-20	123.8	125	1.2	0.006	0.0017	<0.005	<0.5	0.0046	0.03
BR-11-20	125	127	2	0.009	0.0022	0.008	<0.5	0.0031	0.015

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-11-20	127	128.9	1.9	0.0336	0.0082	<0.005	<0.5	0.0042	0.091
BR-11-20	128.9	130.2	1.3	0.0109	0.0695	0.006	<0.5	0.0055	0.578
BR-11-20	130.2	132.2	2	0.0195	0.012	0.006	<0.5	0.0005	0.015
BR-11-20	132.2	134.2	2	0.0113	0.0103	<0.005	<0.5	0.0046	0.03
BR-11-20	134.2	135	0.8	0.0109	0.006	0.009	0.5	0.0039	0.198
BR-11-20	135	136	1	0.013	0.0106	<0.005	0.5	0.0032	0.046
BR-11-20	136	137	1	0.0096	0.03	0.005	0.5	0.0054	0.076
BR-11-20	137	138	1	0.0087	0.029	<0.005	<0.5	0.0044	0.076
BR-11-20	138	139	1	0.0063	0.0178	0.01	<0.5	0.0047	0.122
BR-11-20	139	140	1	0.01	0.0137	0.014	<0.5	0.0064	0.517
BR-11-20	140	141	1	0.0141	0.0511	0.008	<0.5	0.0167	0.152
BR-11-20	141	142.2	1.2	0.0216	0.0553	0.007	<0.5	0.0129	0.106
BR-11-20	142.2	143	0.8	0.0246	0.0212	<0.005	0.5	0.0027	0.411
BR-11-20	143	144	1	0.006	0.0032	<0.005	<0.5	0.0005	0.137
BR-11-20	144	145	1	0.0051	0.0033	<0.005	<0.5	0.0015	0.106
BR-11-20	145	146	1	0.0268	0.0051	<0.005	<0.5	0.0007	0.183
BR-11-20	146	146.8	0.8	0.0122	0.0047	<0.005	<0.5	0.0013	0.046
BR-11-20	146.8	147.3	0.5	0.0153	0.0026	<0.005	<0.5	0.0012	0.152
BR-11-20	147.3	148.5	1.2	0.0148	0.0021	0.007	<0.5	0.0014	0.046
BR-11-20	148.5	150.5	2	0.0104	0.0017	<0.005	<0.5	0.0005	0.061
BR-11-20	150.5	152.5	2	0.0093	0.0029	<0.005	<0.5	0.0026	0.046
BR-11-20	152.5	154	1.5	0.0235	0.0103	<0.005	<0.5	0.002	0.03
BR-11-20	154	156	2	0.0149	0.0043	<0.005	<0.5	0.0019	0.046
BR-11-20	156	158	2	0.01	0.0032	<0.005	<0.5	0.0012	0.046
BR-11-20	158	159	1	0.0077	0.003	<0.005	<0.5	0.0015	0.03
BR-11-20	159	161	2	0.0119	0.0019	<0.005	<0.5	0.0012	0.061
BR-11-20	161	163	2	0.0128	0.0035	<0.005	<0.5	0.0008	0.137
BR-11-20	163	163.7	0.7	0.0146	0.0018	<0.005	<0.5	0.0002	0.061
BR-11-20	163.7	165.4	1.7	0.0139	0.0027	<0.005	<0.5	0.0031	0.106
BR-11-20	165.4	167.4	2	0.008	0.0017	<0.005	<0.5	0.0019	0.243
BR-11-20	167.4	169.4	2	0.0079	0.0016	<0.005	<0.5	<0.005	0.137
BR-11-20	169.4	171	1.6	0.0077	0.0011	<0.005	<0.5	0.0034	0.061
BR-11-20	171	173	2	0.0068	0.001	<0.005	<0.5	0.0004	0.076
BR-11-20	173	175	2	0.0059	0.0007	<0.005	<0.5	0.0013	0.076
BR-11-20	175	177	2	0.0067	0.0009	<0.005	<0.5	0.0018	0.076
BR-11-20	177	179	2	0.0062	0.0012	<0.005	<0.5	0.0012	0.091
BR-11-20	179	181	2	0.0052	0.0012	0.005	<0.5	0.0014	0.061
BR-11-20	181	182	1	0.0121	0.0058	0.017	<0.5	0.0028	0.061
BR-11-20	182	183	1	0.0059	0.0036	0.013	<0.5	0.0007	0.061
BR-11-20	183	184	1	0.0075	0.0009	0.005	<0.5	0.0018	0.213

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-12-20	0	1	1	0.0099	0.0053	<0.005	<0.5	0.0109	0.046
BR-12-20	1	2.6	1.6	0.0095	0.0018	<0.005	<0.5	0.0074	0.03
BR-12-20	2.6	3.1	0.5	No sample					
BR-12-20	3.1	5	1.9	0.0085	0.0021	0.005	<0.5	0.0073	0.046
BR-12-20	5	7	2	0.0101	0.0018	0.006	<0.5	0.0107	0.046
BR-12-20	7	9.6	2.6	No sample					
BR-12-20	9.6	10.4	0.8	0.0088	0.0016	0.007	<0.5	0.0058	0.03
BR-12-20	10.4	12	1.6	0.0076	0.0042	0.005	<0.5	0.0038	0.046
BR-12-20	12	12.1	0.1	No sample					

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-12-20	12.1	14	1.9	0.0079	0.0044	0.005	<0.5	0.0045	0.03
BR-12-20	14	17.8	3.8	No sample					
BR-12-20	17.8	19.8	2	0.0069	0.002	0.006	<0.5	0.0075	0.03
BR-12-20	19.8	21.5	1.7	0.0068	0.0018	0.008	<0.5	0.0077	0.015
BR-12-20	21.5	24.3	2.8	No sample					
BR-12-20	24.3	25.3	1	0.0056	0.0012	0.022	<0.5	0.006	0.015
BR-12-20	25.3	25.8	0.5	0.0081	0.0018	0.013	<0.5	0.01	0.03
BR-12-20	25.8	31	5.2	No sample					
BR-12-20	31	33	2	0.0103	0.0034	0.008	<0.5	0.0063	0.015
BR-12-20	33	35	2	0.0096	0.0048	0.009	<0.5	0.0087	0.015
BR-12-20	35	37	2	0.0099	0.0016	0.01	<0.5	0.0072	0.03
BR-12-20	37	38.6	1.6	0.008	0.0029	0.005	<0.5	0.0055	0.015
BR-12-20	38.6	40	1.4	0.0038	0.0009	<0.005	<0.5	<0.005	0.015
BR-12-20	40	41.8	1.8	0.0086	0.0017	<0.005	<0.5	0.0015	0.046
BR-12-20	41.8	42.6	0.8	0.0106	0.0024	<0.005	<0.5	0.0013	0.046
BR-12-20	42.6	45.7	3.1	No sample					
BR-12-20	45.7	47.2	1.5	0.0156	0.0058	<0.005	<0.5	0.0015	0.076
BR-12-20	47.2	47.7	0.5	No sample					
BR-12-20	47.7	49	1.3	0.0109	0.0022	<0.005	<0.5	0.001	0.015
BR-12-20	49	50.2	1.2	0.0067	0.0089	<0.005	<0.5	0.002	0.015
BR-12-20	50.2	51.4	1.2	0.002	0.0085	<0.005	<0.5	0.0009	0.015
BR-12-20	51.4	59.5	8.1	No sample					
BR-12-20	59.5	60.7	1.2	0.0109	0.0035	<0.005	<0.5	0.0004	0.03
BR-12-20	60.7	62.5	1.8	0.0113	0.0062	<0.005	<0.5	0.0016	0.061
BR-12-20	62.5	64	1.5	0.0098	0.0009	<0.005	<0.5	0.0001	0.091
BR-12-20	64	66	2	0.01	0.001	<0.005	<0.5	0.0048	0.061
BR-12-20	66	68	2	0.0097	0.0009	<0.005	<0.5	0.0001	0.076
BR-12-20	68	70	2	0.0095	0.0015	<0.005	<0.5	0.0002	0.046
BR-12-20	70	72	2	0.0098	0.0012	<0.005	<0.5	0.0001	0.03
BR-12-20	72	74	2	0.0112	0.0009	<0.005	<0.5	0.0001	0.091
BR-12-20	74	76	2	0.0156	0.0012	<0.005	0.6	0.0041	0.061
BR-12-20	76	78	2	0.017	0.0006	<0.005	<0.5	0.0023	0.046
BR-12-20	78	80	2	0.0161	0.0011	<0.005	<0.5	0.0001	0.061
BR-12-20	80	82	2	0.0164	0.0009	<0.005	1.9	0.0076	0.061
BR-12-20	82	84	2	0.0162	0.0012	<0.005	0.6	0.0028	0.061
BR-12-20	84	86	2	0.0127	0.0016	<0.005	1.4	0.0062	0.091
BR-12-20	86	88	2	0.0092	0.0012	<0.005	<0.5	0.0003	0.061
BR-12-20	88	90	2	0.0086	0.0012	<0.005	<0.5	0.0001	0.03
BR-12-20	90	92	2	0.0079	0.0013	<0.005	<0.5	0.0001	0.046
BR-12-20	92	94	2	0.009	0.001	<0.005	<0.5	0.0008	0.061
BR-12-20	94	96	2	0.0127	0.001	<0.005	<0.5	0.0006	0.122
BR-12-20	96	98	2	0.01	0.0013	<0.005	<0.5	0.0001	0.046
BR-12-20	98	100	2	0.0115	0.0014	<0.005	<0.5	0.0001	0.076
BR-12-20	100	102	2	0.0123	0.001	<0.005	2.8	0.0027	0.167
BR-12-20	102	102.7	0.7	0.0142	0.0012	<0.005	13.6	0.0134	0.091
BR-12-20	102.7	103.5	0.8	0.208	0.0242	0.005	6.4	0.0041	1.978
BR-12-20	103.5	104.5	1	0.1805	0.0276	0.033	14.6	0.0016	3.24
BR-12-20	104.5	105.5	1	0.511	0.257	0.037	13.9	0.0059	1.217
BR-12-20	105.5	106.5	1	0.0863	0.0153	0.013	1.1	0.0028	0.38
BR-12-20	106.5	107.5	1	0.0578	0.0113	0.009	2.1	0.0029	2.54
BR-12-20	107.5	108.5	1	0.047	0.0089	<0.005	3.9	0.0006	0.867

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-12-20	108.5	109	0.5	0.1425	0.103	0.006	65.7	0.0061	0.35
BR-12-20	109	109.7	0.7	0.1685	0.0647	0.009	34.6	0.0034	0.335
BR-12-20	109.7	110.5	0.8	0.0117	0.011	0.028	1.9	0.0018	1.46
BR-12-20	110.5	111.5	1	0.1185	0.446	0.059	8.4	0.0491	3.499
BR-12-20	111.5	112.5	1	0.376	0.165	0.2	6.8	0.0213	3.636
BR-12-20	112.5	113.5	1	0.683	0.339	0.3	31	0.131	6.587
BR-12-20	113.5	114	0.5	4.75	3.78	1.455	220	0.549	70.89
BR-12-20	114	114.7	0.7	11.6	6.39	2.56	520	0.59	69.216
BR-12-20	114.7	116.4	1.7	1.53	2.12	0.717	104	0.0878	4.822
BR-12-20	116.4	118.4	2	0.016	0.0174	0.005	<0.5	0.0038	0.563
BR-12-20	118.4	118.9	0.5	No sample					
BR-12-20	118.9	120.8	1.9	0.0755	0.0649	0.005	<0.5	0.0077	0.152
BR-12-20	120.8	122.8	2	0.0239	0.0157	0.01	<0.5	0.0177	0.046
BR-12-20	122.8	124.5	1.7	0.0063	0.0035	<0.005	<0.5	0.0014	0.046
BR-12-20	124.5	126.5	2	0.0075	0.003	<0.005	<0.5	0.0015	0.03
BR-12-20	126.5	128.5	2	0.0091	0.0038	0.005	<0.5	0.0018	0.03
BR-12-20	128.5	130.1	1.6	0.0096	0.0036	<0.005	<0.5	0.0013	0.03

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-13-20	0	1.5	1.5	0.0095	0.0024	0.006	<0.5	0.0074	0.061
BR-13-20	1.5	4.8	3.3	No sample					
BR-13-20	4.8	6.7	1.9	0.0094	0.0021	0.005	<0.5	0.0053	0.046
BR-13-20	6.7	8.2	1.5	0.0105	0.0027	<0.005	<0.5	0.0066	0.046
BR-13-20	8.2	10.2	2	0.0097	0.0014	<0.005	<0.5	0.0066	0.046
BR-13-20	10.2	12.2	2	0.0099	0.0017	0.005	<0.5	0.0064	0.046
BR-13-20	12.2	14.2	2	0.0113	0.0026	0.006	<0.5	0.0077	0.091
BR-13-20	14.2	16.2	2	0.0073	0.002	<0.005	<0.5	0.007	0.03
BR-13-20	16.2	18.2	2	0.0085	0.0019	0.007	<0.5	0.0047	0.046
BR-13-20	18.2	19.8	1.6	0.0031	0.0013	<0.005	<0.5	0.0016	0.015
BR-13-20	19.8	21.8	2	0.0035	0.001	<0.005	<0.5	0.0018	0.015
BR-13-20	21.8	23.7	1.9	0.0066	0.0013	0.005	<0.5	0.0062	0.015
BR-13-20	23.7	25.7	2	0.0067	0.0023	0.006	<0.5	0.005	0.015
BR-13-20	25.7	27.2	1.5	0.0169	0.0204	0.01	<0.5	0.0089	0.03
BR-13-20	27.2	28.2	1	0.0284	0.0559	0.015	<0.5	0.0119	0.03
BR-13-20	28.2	30	1.8	0.0113	0.0078	0.012	<0.5	0.0103	0.091
BR-13-20	30	32	2	0.007	0.0024	0.009	<0.5	0.007	0.015
BR-13-20	32	34	2	0.0084	0.0022	0.009	<0.5	0.0076	0.03
BR-13-20	34	36	2	0.0104	0.0023	0.017	<0.5	0.0079	0.03
BR-13-20	36	38	2	0.0075	0.0026	0.011	<0.5	0.0066	0.015
BR-13-20	38	40	2	0.0084	0.0022	<0.005	<0.5	0.0049	0.03
BR-13-20	40	42	2	0.0056	0.002	<0.005	<0.5	0.0036	0.061
BR-13-20	42	44	2	0.0089	0.0038	<0.005	<0.5	0.0058	0.03
BR-13-20	44	44.9	0.9	0.0095	0.0075	<0.005	<0.5	0.0027	0.015
BR-13-20	44.9	46.9	2	0.0064	0.0039	<0.005	<0.5	0.0015	0.03
BR-13-20	46.9	48.3	1.4	0.0067	0.0054	<0.005	<0.5	0.001	0.03
BR-13-20	48.3	49.5	1.2	0.0099	0.0022	<0.005	<0.5	0.0009	0.015
BR-13-20	49.5	50.6	1.1	0.015	0.0027	<0.005	<0.5	0.0015	0.015
BR-13-20	50.6	52.6	2	0.007	0.0009	<0.005	<0.5	0.0013	0.03
BR-13-20	52.6	54.6	2	0.0114	0.0018	<0.005	<0.5	0.0009	0.015
BR-13-20	54.6	56.6	2	0.0138	0.005	0.006	<0.5	0.0029	0.03
BR-13-20	56.6	57.3	0.7	0.0119	0.0017	<0.005	<0.5	0.0012	0.046

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-13-20	57.3	59	1.7	0.0105	0.0011	<0.005	<0.5	0.0012	0.061
BR-13-20	59	60.5	1.5	0.0129	0.002	<0.005	<0.5	0.0036	0.046
BR-13-20	60.5	62.5	2	0.0118	0.003	<0.005	<0.5	0.0015	0.046
BR-13-20	62.5	64.5	2	0.0138	0.0019	<0.005	<0.5	0.0044	0.061
BR-13-20	64.5	66.5	2	0.0121	0.0009	<0.005	<0.5	0.0011	0.152
BR-13-20	66.5	68.5	2	0.0182	0.0088	<0.005	4.4	0.0033	0.243
BR-13-20	68.5	70	1.5	0.0108	0.0013	<0.005	0.8	0.0006	0.502
BR-13-20	70	70.9	0.9	0.0101	0.0014	<0.005	0.9	0.0013	0.046
BR-13-20	70.9	72	1.1	0.0067	0.0058	<0.005	3	0.0021	0.122
BR-13-20	72	74	2	0.0114	0.0014	<0.005	1.7	0.0019	0.122
BR-13-20	74	76	2	0.0086	0.0163	<0.005	5.4	0.0018	0.624
BR-13-20	76	77	1	0.0054	0.0036	<0.005	1.1	0.0008	0.289
BR-13-20	77	78.1	1.1	0.0064	0.0024	<0.005	5.1	0.002	0.228
BR-13-20	78.1	80	1.9	0.0084	0.0008	0.007	16.6	0.0036	0.304
BR-13-20	80	82	2	0.0153	0.0041	0.006	5.4	0.0015	0.502
BR-13-20	82	84	2	0.0173	0.0067	<0.005	23	0.0048	0.213
BR-13-20	84	86	2	0.0105	0.0015	<0.005	2.2	0.0008	0.639
BR-13-20	86	87	1	0.0099	0.0009	<0.005	<0.5	0.0005	0.456
BR-13-20	87	88.4	1.4	0.0091	0.0012	<0.005	1	0.001	1.293
BR-13-20	88.4	90	1.6	0.0092	0.0035	<0.005	2.4	0.0014	0.167
BR-13-20	90	92	2	0.0072	0.0033	<0.005	3.1	0.0022	0.122
BR-13-20	92	94	2	0.0098	0.0009	<0.005	0.5	0.0004	0.243
BR-13-20	94	96	2	0.0091	0.0013	<0.005	2	0.0014	1.947
BR-13-20	96	96.8	0.8	0.0455	0.0185	<0.005	8.3	0.0029	2.54
BR-13-20	96.8	98	1.2	0.0123	0.0066	<0.005	3.3	0.0015	0.441
BR-13-20	98	99.1	1.1	0.0205	0.0096	<0.005	9.3	0.0023	0.183
BR-13-20	99.1	100.6	1.5	0.0291	0.0167	<0.005	26.6	0.0058	1.323
BR-13-20	100.6	102.1	1.5	0.0117	0.0064	<0.005	3.4	0.003	0.183
BR-13-20	102.1	104	1.9	0.0139	0.0013	<0.005	<0.5	0.0001	0.091
BR-13-20	104	106	2	0.0142	0.0013	<0.005	2.3	0.004	0.076
BR-13-20	106	108	2	0.0154	0.0012	<0.005	<0.5	0.0004	0.456
BR-13-20	108	110	2	0.0111	0.0011	<0.005	<0.5	0.0001	0.122
BR-13-20	110	112	2	0.01	0.0009	<0.005	<0.5	0.0002	0.183
BR-13-20	112	114	2	0.0096	0.0021	<0.005	2.2	0.0014	0.106
BR-13-20	114	116	2	0.0278	0.0159	<0.005	11.3	0.0107	0.624
BR-13-20	116	118	2	0.0198	0.0038	<0.005	2.3	0.003	0.167
BR-13-20	118	120	2	0.0091	0.0014	<0.005	2.2	0.0007	0.304
BR-13-20	120	121.65	1.65	0.0104	0.0035	0.009	3.5	0.0002	0.243
BR-13-20	121.65	122.5	0.85	0.125	0.0482	0.044	22.1	0.0033	2.343
BR-13-20	122.5	123.5	1	0.371	0.143	0.085	35.7	0.0067	3.134
BR-13-20	123.5	124.5	1	1.275	1.495	0.172	33.3	<0.53	1.384
BR-13-20	124.5	125.5	1	1.08	0.325	0.263	18.8	0.797	4.168
BR-13-20	125.5	126.5	1	1.28	0.377	0.532	23.5	1.105	0.882
BR-13-20	126.5	127	0.5	0.209	0.0229	0.296	2	0.0154	0.106
BR-13-20	127	127.5	0.5	0.1685	0.0049	0.076	0.5	0.002	0.532
BR-13-20	127.5	128.5	1	0.824	0.66	0.188	15.4	0.267	2.83
BR-13-20	128.5	129.5	1	12	8.32	1.29	160	2.02	1.171
BR-13-20	129.5	130.5	1	5.49	2.84	0.751	69.4	0.491	7.013
BR-13-20	130.5	131.5	1	0.65	0.502	0.36	25.3	0.116	6.648
BR-13-20	131.5	132.6	1.1	0.935	0.398	0.325	55	0.157	13.113
BR-13-20	132.6	133.7	1.1	1.075	0.392	0.21	22.5	0.29	15.441

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-13-20	133.7	134	0.3	1.665	2.13	2.27	106	0.51	84.429
BR-13-20	134	134.9	0.9	1.905	2.23	3.18	174	0.584	84.277
BR-13-20	134.9	136	1.1	0.174	0.226	0.196	9.2	0.016	7.606
BR-13-20	136	137	1	0.287	0.176	0.028	11.3	0.0124	0.654
BR-13-20	137	138	1	0.286	0.101	0.014	10.3	0.0106	0.03
BR-13-20	138	139.1	1.1	0.37	0.26	0.012	9.4	0.0078	1.582
BR-13-20	139.1	141	1.9	0.0732	0.132	0.007	1	0.0039	1.171
BR-13-20	141	143	2	0.144	0.022	0.009	<0.5	0.0068	0.076
BR-13-20	143	145	2	0.0529	0.0265	0.018	<0.5	0.0093	0.03
BR-13-20	145	147	2	0.0128	0.0322	0.023	<0.5	0.012	0.061
BR-13-20	147	149	2	0.0265	0.0362	0.024	<0.5	0.008	0.03
BR-13-20	149	149.5	0.5	No sample					
BR-13-20	149.5	151.5	2	0.0229	0.0115	<0.005	<0.5	0.0035	0.03
BR-13-20	151.5	153.5	2	0.005	0.006	<0.005	<0.5	0.0017	0.03
BR-13-20	153.5	155.2	1.7	0.0083	0.0081	<0.005	<0.5	0.0007	0.03

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-17-20	0	118.8	No sample						
BR-17-20	118.8	119.8	1	0.261	0.342	0.017	2.6	0.026	0.213
BR-17-20	119.8	120.8	1	0.161	0.0628	<0.005	3	0.0046	0.015
BR-17-20	120.8	121.8	1	0.0132	0.0056	<0.005	<0.5	0.0004	0.015
BR-17-20	121.8	122.8	1	0.0247	0.0081	<0.005	<0.5	0.0009	0.015
BR-17-20	122.8	123.8	1	0.0276	0.0037	0.006	<0.5	0.0004	0.03
BR-17-20	123.8	124.8	1	0.0074	0.0017	<0.005	<0.5	0.0001	0.008
BR-17-20	124.8	125.8	1	0.0052	0.0016	<0.005	<0.5	0.0004	0.008
BR-17-20	125.8	126.5	0.7	0.343	0.0791	0.005	1.1	0.0035	0.015
BR-17-20	126.5	127	0.5	0.369	0.104	0.008	5.6	0.0074	0.015
BR-17-20	127	127.5	0.5	0.257	0.0508	0.006	6.8	0.0058	0.015
BR-17-20	127.5	128	0.5	0.123	0.0312	0.008	1.2	0.0021	0.015
BR-17-20	128	128.5	0.5	0.287	0.0628	0.007	<0.5	0.003	0.015
BR-17-20	128.5	129	0.5	0.102	0.159	0.009	4.9	0.0052	0.015
BR-17-20	129	129.5	0.5	0.138	0.0238	<0.005	2.6	0.0031	0.008
BR-17-20	129.5	130.5	1	0.029	0.0062	0.005	0.5	0.0003	0.008
BR-17-20	130.5	131	0.5	0.0371	0.0329	<0.005	1	0.001	0.008
BR-17-20	131	132	1	0.0424	0.0646	0.006	0.9	0.0009	0.008
BR-17-20	132	133	1	0.0754	0.0806	0.013	0.9	0.0007	0.008
BR-17-20	133	133.5	0.5	0.019	0.0444	0.007	0.8	0.0006	0.008
BR-17-20	133.5	134	0.5	0.0151	0.0501	<0.005	<0.5	0.0005	0.008
BR-17-20	134	134.5	0.5	0.0074	0.0157	0.005	<0.5	0.0001	0.008
BR-17-20	134.5	135	0.5	0.0029	0.0096	<0.005	<0.5	0.0005	0.008
BR-17-20	135	136	1	0.0055	0.0086	<0.005	<0.5	0.0003	0.008
BR-17-20	136	137	1	0.0029	0.0106	<0.005	<0.5	0.0003	0.008
BR-17-20	137	138	1	0.0138	0.0073	<0.005	<0.5	0.0002	0.008
BR-17-20	138	139	1	0.02	0.0084	0.005	<0.5	0.0001	0.008
BR-17-20	139	140	1	0.0226	0.0105	<0.005	<0.5	0.0001	0.008
BR-17-20	140	141	1	0.0064	0.0079	0.038	<0.5	0.0001	0.015
BR-17-20	141	142	1	0.022	0.0449	0.02	1.4	0.0007	0.008
BR-17-20	142	143	1	0.0199	0.0464	<0.005	0.5	0.0004	0.008
BR-17-20	143	144	1	0.0205	0.0842	<0.005	<0.5	0.0003	0.008
BR-17-20	144	145	1	0.0156	0.0529	<0.005	<0.5	0.0004	0.008
BR-17-20	145	146	1	0.0159	0.12	<0.005	0.5	0.0003	0.008

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-17-20	146	147	1	0.0181	0.0711	<0.005	<0.5	0.0003	0.008
BR-17-20	147	148	1	0.011	0.0497	<0.005	<0.5	0.0002	0.015
BR-17-20	148	149	1	0.0132	0.12	<0.005	0.6	0.0004	0.076
BR-17-20	149	150	1	0.0039	0.1	<0.005	<0.5	0.0001	0.03
BR-17-20	150	151	1	0.0141	0.295	<0.005	1.1	0.0003	0.015
BR-17-20	151	152	1	0.0037	0.0534	0.006	<0.5	0.0002	0.015
BR-17-20	152	153	1	0.0273	0.026	<0.005	<0.5	0.0002	0.03
BR-17-20	153	154	1	0.0071	0.0058	0.005	<0.5	0.0001	0.008
BR-17-20	154	155	1	0.0033	0.0037	0.006	<0.5	0.0003	0.008
BR-17-20	155	156	1	0.0022	0.0011	<0.005	<0.5	0.0006	0.03
BR-17-20	156	157	1	<0.005	0.0004	<0.005	<0.5	0.0002	0.106
BR-17-20	157	158	1	0.0033	0.0004	0.005	<0.5	0.0001	0.076
BR-17-20	158	159	1	0.0041	0.0018	<0.005	<0.5	0.0016	0.03
BR-17-20	159	160	1	0.0084	0.0012	<0.005	<0.5	0.0003	0.015
BR-17-20	160	161	1	0.0086	0.0026	<0.005	<0.5	0.001	0.015
BR-17-20	161	162	1	0.0052	0.002	<0.005	<0.5	0.0021	0.03
BR-17-20	162	163	1	0.0038	0.0019	<0.005	<0.5	0.0007	0.015
BR-17-20	163	163.6	0.6	0.0028	0.0009	0.005	<0.5	0.0006	0.015
BR-17-20	163.6	164.5	0.9	0.012	0.0037	<0.005	<0.5	0.0038	0.03
BR-17-20	164.5	165.5	1	0.0106	0.0018	<0.005	<0.5	0.002	0.061
BR-17-20	165.5	166.5	1	0.01	0.002	<0.005	<0.5	0.0012	0.076
BR-17-20	166.5	167.5	1	0.0147	0.0036	<0.005	<0.5	0.0022	0.091
BR-17-20	167.5	168	0.5	0.0219	0.0124	<0.005	<0.5	0.013	0.061
BR-17-20	168	168.9	0.9	0.0134	0.0035	<0.005	<0.5	0.0013	0.061
BR-17-20	168.9	170.8	1.9	0.0123	<0.005	0.005	<0.5	0.0004	0.046
BR-17-20	170.8	172.8	2	0.0128	0.0021	<0.005	<0.5	0.0004	0.046
BR-17-20	172.8	174.8	2	0.0087	0.0065	<0.005	<0.5	0.0039	0.076
BR-17-20	174.8	176	1.2	0.0104	0.0016	<0.005	<0.5	0.0003	0.076
BR-17-20	176	178	2	0.0136	0.001	<0.005	<0.5	0.002	0.061
BR-17-20	178	179	1	0.013	0.0013	<0.005	<0.5	0.0002	0.03
BR-17-20	179	180.1	1.1	0.0134	0.001	<0.005	<0.5	0.0056	0.061
BR-17-20	180.1	182.1	2	0.0197	0.007	<0.005	<0.5	0.0015	0.73
BR-17-20	182.1	183	0.9	0.0398	0.0114	<0.005	<0.5	0.0022	0.061
BR-17-20	183	184	1	0.009	0.0033	<0.005	<0.5	0.002	0.411
BR-17-20	184	185	1	0.0099	0.0023	<0.005	0.9	0.0009	0.472
BR-17-20	185	186	1	0.0121	0.0073	0.011	1.7	0.0019	0.335
BR-17-20	186	187	1	0.0697	0.0267	0.015	19	0.0064	0.396
BR-17-20	187	188	1	0.013	0.0016	0.01	0.7	0.0004	0.198
BR-17-20	188	189	1	0.0149	0.0042	0.008	3.5	0.0017	0.548
BR-17-20	189	190	1	0.0092	0.0063	0.006	4.9	0.0011	0.806
BR-17-20	190	191	1	0.0219	0.017	0.021	6.7	0.0019	1.019
BR-17-20	191	192	1	0.38	0.261	0.027	49.6	0.0147	2.83
BR-17-20	192	192.9	0.9	0.0161	0.0252	0.018	4.2	0.0016	2.221
BR-17-20	192.9	193.5	0.6	1.67	0.288	0.966	279	0.585	36.206
BR-17-20	193.5	194	0.5	4.13	2.81	1.75	137	1.29	54.46
BR-17-20	194	194.5	0.5	2.23	0.754	2.01	124	0.324	38.944
BR-17-20	194.5	195	0.5	0.606	0.221	0.692	19.3	0.0881	11.546
BR-17-20	195	196	1	0.229	0.0482	0.157	4.5	0.0239	1.034
BR-17-20	196	196.5	0.5	0.226	0.0879	0.151	4	0.0407	3.59
BR-17-20	196.5	197	0.5	0.0818	0.0327	0.227	6.7	0.0211	0.578
BR-17-20	197	198	1	0.0633	0.0098	0.095	2.4	0.0058	0.532

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-17-20	198	199	1	0.0993	0.0126	0.084	1.2	0.0035	0.106
BR-17-20	199	200	1	0.0483	0.0233	0.082	1.2	0.0047	0.061
BR-17-20	200	201	1	0.0182	0.0104	0.062	1.1	0.0021	0.046
BR-17-20	201	202	1	0.0127	0.0034	0.021	<0.5	0.001	0.03
BR-17-20	202	203	1	0.0333	0.0157	0.069	0.9	0.0065	0.806
BR-17-20	203	203.5	0.5	0.105	0.0455	0.077	0.9	0.0129	0.274
BR-17-20	203.5	204	0.5	0.043	0.0089	0.056	<0.5	0.0023	0.487
BR-17-20	204	204.5	0.5	1.315	0.414	0.883	112	0.235	19.852
BR-17-20	204.5	205	0.5	1.135	0.493	0.774	151	0.249	31.642
BR-17-20	205	205.5	0.5	0.734	0.322	0.682	79.2	0.0916	15.288
BR-17-20	205.5	206	0.5	4.21	2.05	1.21	223	0.506	36.966
BR-17-20	206	206.7	0.7	0.21	0.372	0.532	42.3	0.0483	4.503
BR-17-20	206.7	208	1.3	0.0053	0.0019	0.006	<0.5	0.001	0.076
BR-17-20	208	210	2	0.0039	0.0008	0.016	<0.5	0.0037	0.015
BR-17-20	210	212	2	0.0037	0.0008	<0.005	<0.5	0.0023	0.015
BR-17-20	212	214	2	0.0057	0.002	<0.005	<0.5	0.0024	0.03
BR-17-20	214	216	2	0.006	0.0017	0.01	<0.5	0.0018	0.015
BR-17-20	216	218	2	0.0036	0.0016	0.005	<0.5	0.0012	0.03
BR-17-20	218	220	2	0.0062	0.0017	<0.005	<0.5	0.0015	0.091
BR-17-20	220	222	2	0.008	0.0028	<0.005	<0.5	0.0512	0.106
BR-17-20	222	222.9	0.9	0.0123	0.0034	0.012	<0.5	0.0066	0.441
BR-17-20	222.9	223.5	0.6	0.243	0.302	0.028	1.1	0.031	1.308
BR-17-20	223.5	224	0.5	0.31	0.226	0.063	1.5	0.0259	1.354
BR-17-20	224	224.5	0.5	0.207	0.172	0.05	0.8	0.0246	0.73
BR-17-20	224.5	225	0.5	0.204	0.0557	0.038	1.1	0.0182	0.426
BR-17-20	225	225.5	0.5	0.0601	0.0244	0.033	1.8	0.0256	0.213
BR-17-20	225.5	226	0.5	0.0103	0.013	0.02	0.7	0.0091	0.517
BR-17-20	226	226.5	0.5	0.0164	0.012	0.01	0.6	0.0047	0.472
BR-17-20	226.5	227.2	0.7	0.0194	0.0654	0.015	0.6	0.0095	1.034
BR-17-20	227.2	228.9	1.7	0.0098	0.0063	0.007	<0.5	0.0164	0.761
BR-17-20	228.9	229.7	0.8	0.0701	0.15	0.03	0.6	0.025	11.637
BR-17-20	229.7	230.5	0.8	0.0823	0.231	0.231	9.1	0.0252	9.371
BR-17-20	230.5	231	0.5	8.63	6.12	3.12	341	0.334	38.335
BR-17-20	231	231.5	0.5	5.67	4.11	1.74	266	0.492	13.737
BR-17-20	231.5	232	0.5	1.515	2.26	1.36	67.4	0.383	7.226
BR-17-20	232	232.9	0.9	0.177	0.409	0.515	8.1	0.11	4.716
BR-17-20	232.9	234	1.1	0.0107	0.0149	0.052	13.3	0.0093	0.821
BR-17-20	234	235	1	0.0494	0.0177	0.054	18.1	0.003	1.156
BR-17-20	235	236	1	0.0829	0.0406	0.063	4.5	0.0015	<0.59
BR-17-20	236	237	1	0.0501	0.0315	0.036	3.2	0.0105	1.308
BR-17-20	237	237.8	0.8	0.278	0.0564	0.139	2.1	0.007	0.061
BR-17-20	237.8	238.8	1	0.266	0.453	0.396	22.2	0.0264	0.091
BR-17-20	238.8	239.8	1	0.502	0.213	0.14	9.5	0.013	0.061
BR-17-20	239.8	240.8	1	0.182	0.121	0.153	15.7	0.0299	0.03
BR-17-20	240.8	241.8	1	0.0401	0.013	0.104	5.1	0.0023	0.046
BR-17-20	241.8	242.5	0.7	0.127	0.0363	0.124	9.3	0.0046	0.046
BR-17-20	242.5	243	0.5	0.188	0.0829	0.137	10.2	0.0087	0.046
BR-17-20	243	243.5	0.5	0.417	0.43	0.207	140	0.0319	0.289
BR-17-20	243.5	244	0.5	0.225	0.141	0.189	130	0.0366	0.167
BR-17-20	244	244.5	0.5	0.719	0.349	0.233	124	0.0361	0.791
BR-17-20	244.5	245	0.5	1.05	0.498	0.313	262	0.0839	1.719

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-17-20	245	245.5	0.5	0.203	0.0423	0.127	8.7	0.0026	0.152
BR-17-20	245.5	246	0.5	0.118	0.067	0.182	7.2	0.0037	0.106
BR-17-20	246	246.5	0.5	0.694	0.264	0.459	29	0.0174	2.297
BR-17-20	246.5	247	0.5	0.892	0.512	0.457	41.1	0.0229	1.004
BR-17-20	247	247.5	0.5	1.11	0.541	0.388	84.1	0.0446	1.491
BR-17-20	247.5	248	0.5	1.07	0.341	0.372	48.9	0.0291	0.791
BR-17-20	248	248.5	0.5	0.872	0.383	0.548	49.6	0.0354	0.259
BR-17-20	248.5	249	0.5	0.253	0.1005	0.423	12	0.0102	0.274
BR-17-20	249	249.5	0.5	0.595	0.1215	0.464	14.3	0.015	0.502
BR-17-20	249.5	250	0.5	1.415	0.699	0.42	49.7	0.0408	1.05
BR-17-20	250	250.5	0.5	2.11	0.855	0.427	79.1	0.0779	1.536
BR-17-20	250.5	251	0.5	0.852	0.404	0.462	25.8	0.0364	0.624
BR-17-20	251	252	1	0.97	0.53	0.498	32.6	0.0446	0.852
BR-17-20	252	253	1	0.568	0.319	0.295	13.2	0.022	0.898
BR-17-20	253	254	1	0.411	0.285	0.355	8.4	0.0245	0.7
BR-17-20	254	255	1	0.191	0.352	0.242	17.3	0.0233	0.837
BR-17-20	255	256	1	0.0438	0.672	0.338	29.7	0.0299	0.38
BR-17-20	256	257	1	0.735	0.426	0.275	19.9	0.0211	0.304
BR-17-20	257	258	1	0.325	0.146	0.267	4.2	0.0084	0.73
BR-17-20	258	259	1	0.125	0.0665	0.423	3.8	0.0056	0.076
BR-17-20	259	260	1	0.335	0.18	0.282	7	0.0241	0.076
BR-17-20	260	261	1	0.33	0.152	0.304	4.7	0.0108	0.046
BR-17-20	261	262	1	0.154	0.279	0.303	23.6	0.0642	0.365
BR-17-20	262	263	1	0.266	0.409	0.223	23.6	0.0378	0.198
BR-17-20	263	264	1	0.507	0.325	0.218	33.4	0.0493	0.213
BR-17-20	264	265	1	0.438	0.0966	0.145	4.1	0.0032	0.061
BR-17-20	265	266	1	0.219	0.218	0.138	17.1	0.023	0.137
BR-17-20	266	267	1	0.0992	0.165	0.163	12.7	0.0095	0.03
BR-17-20	267	268	1	0.185	0.0899	0.201	15	0.013	0.091
BR-17-20	268	269	1	0.429	0.206	0.233	21.6	0.0287	0.198
BR-17-20	269	270	1	2.93	1.61	0.537	137	0.202	0.791
BR-17-20	270	271	1	0.967	0.414	0.32	47.2	0.0566	0.167
BR-17-20	271	272	1	0.0682	0.0391	0.156	6.1	0.0071	0.106
BR-17-20	272	273	1	0.462	0.246	0.161	27.7	0.021	0.122
BR-17-20	273	274.2	1.2	<0.5	0.201	0.284	7.1	0.006	0.122
BR-17-20	274.2	274.4	0.2	No sample					
BR-17-20	274.4	275	0.6	0.381	0.1405	0.081	5.9	0.0093	0.046
BR-17-20	275	276	1	0.144	0.05	0.041	1.1	0.0033	0.03
BR-17-20	276	277	1	0.234	0.078	0.057	6.6	0.0209	0.03
BR-17-20	277	278	1	0.241	0.0252	0.069	1.8	0.0051	0.03
BR-17-20	278	279	1	0.129	0.0637	0.086	1.2	0.0041	0.046
BR-17-20	279	280	1	0.0951	0.0139	0.05	0.8	<0.005	0.046
BR-17-20	280	281	1	0.0182	0.0105	0.039	<0.5	0.0017	0.046
BR-17-20	281	282	1	0.007	0.0114	0.06	<0.5	0.0013	0.198
BR-17-20	282	283	1	0.0066	0.0077	0.092	<0.5	0.002	0.061
BR-17-20	283	284	1	0.044	0.0295	0.104	2.1	0.0048	0.122
BR-17-20	284	285	1	0.31	0.252	0.086	21.5	0.0463	0.913
BR-17-20	285	286	1	0.424	0.174	0.064	14.8	0.0328	0.152
BR-17-20	286	287	1	0.0459	0.0091	0.075	3.2	0.0106	0.046
BR-17-20	287	288	1	0.0619	0.0395	0.047	2.3	0.0084	0.046
BR-17-20	288	289	1	0.064	0.0183	0.028	8.7	0.0364	0.106

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-17-20	289	290	1	0.264	0.141	0.044	1.4	0.0115	0.259
BR-17-20	290	291	1	0.256	0.137	0.067	2.3	0.0131	0.639
BR-17-20	291	292	1	3.03	1.3	0.088	17.2	0.306	1.673
BR-17-20	292	293	1	0.199	0.0562	0.075	1	0.0037	0.106
BR-17-20	293	293.5	0.5	0.157	0.0691	0.073	2.4	0.013	0.106
BR-17-20	293.5	294.4	0.9	0.112	0.0575	0.049	0.9	0.0035	0.046
BR-17-20	294.4	295.4	1	0.104	0.0368	0.052	0.5	0.0019	0.319
BR-17-20	295.4	296	0.6	0.0203	0.0077	0.055	<0.5	0.0016	0.046
BR-17-20	296	297	1	0.0467	0.0086	0.065	<0.5	0.0019	0.198
BR-17-20	297	298	1	0.246	0.0573	0.05	2.6	0.0343	1.415
BR-17-20	298	299	1	0.0581	0.0049	0.042	<0.5	0.0012	0.03
BR-17-20	299	300	1	0.591	0.307	0.078	17	0.103	0.502
BR-17-20	300	301	1	0.267	0.068	0.214	4.1	0.0101	0.35
BR-17-20	301	302	1	0.0201	0.0038	0.042	<0.5	0.0012	0.259
BR-17-20	302	303	1	0.0578	0.0036	0.043	<0.5	0.0013	0.046
BR-17-20	303	304	1	0.0327	0.0038	0.038	<0.5	0.004	0.076
BR-17-20	304	305	1	0.129	0.219	0.033	3.5	0.044	0.776
BR-17-20	305	306	1	0.0431	0.0033	0.026	<0.5	0.0008	0.426
BR-17-20	306	307	1	0.148	0.0587	0.04	0.6	0.0069	0.289
BR-17-20	307	308	1	0.0937	0.0183	0.04	<0.5	0.0017	0.167
BR-17-20	308	309	1	0.0359	0.0112	0.041	<0.5	0.0011	0.076
BR-17-20	309	310	1	0.0228	0.0038	0.019	<0.5	0.0008	0.122
BR-17-20	310	311	1	0.0355	0.0073	0.025	<0.5	0.0015	0.076
BR-17-20	311	312	1	0.132	0.0169	0.043	<0.5	0.0011	0.106
BR-17-20	312	313	1	0.113	0.0153	0.031	<0.5	0.0015	0.319
BR-17-20	313	314	1	0.22	0.0415	0.038	<0.5	0.0013	0.091
BR-17-20	314	314.7	0.7	0.0801	0.0146	0.039	<0.5	0.0009	0.091
BR-17-20	314.7	315.5	0.8	0.0291	0.005	0.018	<0.5	0.0006	0.046
BR-17-20	315.5	316	0.5	0.0263	0.0031	0.016	<0.5	0.0005	0.03
BR-17-20	316	317	1	0.0179	0.0071	0.025	<0.5	0.0006	0.03
BR-17-20	317	318	1	0.0186	0.0035	0.028	<0.5	0.0007	0.03
BR-17-20	318	319	1	0.0352	0.0051	0.022	<0.5	0.0007	0.03
BR-17-20	319	320	1	0.0622	0.0027	0.016	<0.5	0.0007	0.137
BR-17-20	320	321	1	0.074	0.144	0.024	1.3	0.001	0.106
BR-17-20	321	322	1	0.0415	0.0149	0.01	<0.5	0.0007	0.913
BR-17-20	322	323	1	0.0337	0.024	0.01	<0.5	0.0005	0.137
BR-17-20	323	324	1	0.0235	0.0019	0.011	<0.5	0.0005	0.091
BR-17-20	324	325	1	0.0139	0.0023	0.008	<0.5	0.0003	0.046
BR-17-20	325	326	1	0.0112	0.0047	0.014	<0.5	0.0005	0.046
BR-17-20	326	327	1	0.0061	0.002	0.009	<0.5	0.0004	0.061
BR-17-20	327	328	1	0.0295	0.0023	0.006	<0.5	0.0003	0.122
BR-17-20	328	329	1	0.0201	0.0017	0.012	<0.5	0.0006	0.061
BR-17-20	329	330	1	0.0269	0.0043	0.025	<0.5	0.0013	0.046
BR-17-20	330	331	1	0.0317	0.0018	0.014	<0.5	0.0004	0.046
BR-17-20	331	332	1	0.0213	0.0031	0.009	<0.5	0.0003	0.091
BR-17-20	332	333	1	0.024	0.0031	0.015	<0.5	0.0003	0.061
BR-17-20	333	334	1	0.0694	0.006	0.012	<0.5	0.0002	0.046
BR-17-20	334	335	1	0.0144	0.0019	0.007	<0.5	0.0002	0.091
BR-17-20	335	336	1	0.032	0.0168	0.023	<0.5	0.0009	0.167
BR-17-20	336	337	1	0.023	0.0092	0.02	<0.5	0.0006	0.122
BR-17-20	337	338	1	0.2	0.085	0.038	1.1	0.0134	1.552

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-17-20	338	339	1	0.244	0.0795	0.033	1.1	0.0172	0.274
BR-17-20	339	340	1	0.813	0.32	0.034	3.5	0.0535	0.502
BR-17-20	340	341	1	0.118	0.0133	0.021	<0.5	0.0024	0.061
BR-17-20	341	342	1	0.495	0.155	0.078	4.1	0.0187	1.187
BR-17-20	342	343	1	0.364	0.0429	0.033	0.8	0.0023	2.434
BR-17-20	343	344	1	0.0578	0.0095	0.019	<0.5	0.0009	0.487
BR-17-20	344	345	1	0.0552	0.0114	0.013	<0.5	0.0009	0.106
BR-17-20	345	346.2	1.2	0.0908	0.0255	0.033	0.9	0.003	0.365
BR-17-20	346.2	347.4	1.2	0.177	0.0524	0.029	1.5	0.0069	0.106
BR-17-20	347.4	348.5	1.1	0.0864	0.0168	0.019	0.8	0.0016	0.35
BR-17-20	348.5	349.5	1	0.0385	0.0081	0.017	0.6	0.0009	0.091
BR-17-20	349.5	350.5	1	0.0463	0.0047	0.015	0.8	0.0005	0.304
BR-17-20	350.5	351.5	1	0.0079	0.0046	0.016	0.8	0.0009	0.228
BR-17-20	351.5	352.5	1	0.0206	0.0082	0.02	2.2	0.0007	0.106
BR-17-20	352.5	353.5	1	0.0149	0.0081	0.017	1.8	0.001	0.046
BR-17-20	353.5	354.5	1	0.194	0.168	0.027	10.2	0.0011	0.046
BR-17-20	354.5	355.5	1	0.106	0.0639	0.025	11.5	0.0011	0.122
BR-17-20	355.5	356.5	1	0.0183	0.0133	0.023	4.1	0.0018	0.046
BR-17-20	356.5	357.5	1	0.0055	0.003	0.018	4	0.0005	0.03
BR-17-20	357.5	358.5	1	0.0923	0.0242	0.019	4.7	0.0007	0.03
BR-17-20	358.5	359.5	1	0.0309	0.0122	0.017	4.3	0.0005	0.03
BR-17-20	359.5	360.5	1	0.0431	0.0102	0.019	4.7	0.0006	0.046
BR-17-20	360.5	361.5	1	0.0157	0.0072	0.017	13	0.0011	0.243
BR-17-20	361.5	363	1.5	0.0617	0.0308	0.016	8.6	0.0015	0.228
BR-17-20	363	364	1	0.0433	0.0423	0.008	4.6	0.0004	0.821
BR-17-20	364	365	1	0.114	0.0591	0.007	9.4	0.0015	0.776
BR-17-20	365	366	1	0.0325	0.0148	<0.005	2.9	0.0003	0.289
BR-17-20	366	367	1	0.0172	0.0308	0.013	2.3	0.0004	0.076
BR-17-20	367	368	1	0.0379	0.0034	0.008	1.9	0.0002	0.198
BR-17-20	368	369	1	0.0613	0.0084	0.007	2.7	0.0004	0.517
BR-17-20	369	370	1	0.147	0.0272	0.005	3.6	0.0005	0.456
BR-17-20	370	371	1	0.107	0.0073	0.007	2.3	0.0004	0.152
BR-17-20	371	372	1	0.0884	0.0033	0.008	1.5	0.0002	0.35
BR-17-20	372	373	1	0.057	0.0124	0.009	1.6	0.0003	0.106
BR-17-20	373	374	1	0.0053	0.0041	0.007	2.7	0.0004	0.365
BR-17-20	374	375	1	0.0244	0.0091	0.005	1.4	0.0002	0.061
BR-17-20	375	376	1	0.0245	0.0044	<0.005	1.1	0.0003	0.061
BR-17-20	376	377	1	0.0108	0.002	0.006	1.1	0.0003	0.046
BR-17-20	377	378	1	0.0197	0.0047	<0.005	1	0.0003	0.091
BR-17-20	378	379	1	0.0392	0.0076	0.005	1.3	0.0004	0.228
BR-17-20	379	380	1	0.0191	0.0056	0.005	0.8	0.0004	0.076
BR-17-20	380	381	1	0.0762	0.031	0.005	1.4	0.0032	0.076
BR-17-20	381	382	1	0.0544	0.0113	0.006	0.6	0.0009	0.228
BR-17-20	382	383	1	0.187	0.0575	0.009	4.3	0.0065	0.213
BR-17-20	383	384	1	0.0415	0.0056	0.006	1.1	0.0005	0.046
BR-17-20	384	385	1	0.0188	0.0054	0.006	0.6	0.0002	0.137
BR-17-20	385	386	1	0.0471	0.0028	<0.005	<0.5	0.0002	0.441
BR-17-20	386	387	1	0.0123	0.0053	<0.005	0.5	0.0001	0.046
BR-17-20	387	388	1	0.0132	0.0095	0.006	0.7	0.0002	0.046
BR-17-20	388	389	1	0.034	0.0221	0.016	1.4	0.0005	0.076
BR-17-20	389	390	1	0.0136	0.0059	0.006	0.6	0.0003	0.061

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-17-20	390	391	1	0.0098	0.0013	0.005	<0.5	0.0002	0.03
BR-17-20	391	392	1	0.499	0.535	0.02	33.6	0.184	0.669
BR-17-20	392	393	1	0.0233	0.0077	0.015	1.3	0.0005	0.076
BR-17-20	393	394	1	0.191	0.0444	0.054	9.5	0.0017	0.365
BR-17-20	394	395	1	0.0847	0.1035	0.018	7.5	0.0006	1.232
BR-17-20	395	396	1	0.223	0.0603	0.026	25.1	0.0014	0.608
BR-17-20	396	397.3	1.3	0.232	0.0769	0.024	11	0.0008	2.145
BR-17-20	397.3	398	0.7	0.123	0.0628	0.023	5.6	0.0008	0.563
BR-17-20	398	400	2	0.0989	0.0387	0.017	9	0.0033	0.593
BR-17-20	400	402	2	0.0086	0.0022	0.013	<0.5	0.0004	0.046
BR-17-20	402	404	2	0.0063	0.0022	0.019	0.8	0.0004	0.061
BR-17-20	404	406	2	0.0065	0.0013	0.012	0.5	0.0006	0.046
BR-17-20	406	408	2	0.011	0.0021	0.006	0.5	0.0003	0.061
BR-17-20	408	410	2	0.0531	0.0078	0.01	0.8	0.0003	0.137
BR-17-20	410	412	2	0.0238	0.0075	0.006	0.8	0.0002	0.213
BR-17-20	412	414	2	0.0128	0.007	0.007	0.8	0.0004	0.198
BR-17-20	414	416	2	0.0149	<0.005	0.007	0.5	0.0002	0.076
BR-17-20	416	417	1	0.0162	0.0037	0.006	0.6	0.0003	0.213
BR-17-20	417	417.7	0.7	0.022	0.0067	0.009	1	0.0002	0.304
BR-17-20	417.7	418.5	0.8	0.013	0.0028	0.009	<0.5	0.0003	0.03
BR-17-20	418.5	420	1.5	0.008	0.0019	0.016	<0.5	0.0003	0.046
BR-17-20	420	421	1	0.0106	0.0017	0.011	<0.5	0.0002	0.046
BR-17-20	421	422	1	0.0072	0.0016	0.007	<0.5	0.0002	0.274
BR-17-20	422	423	1	0.0254	0.0021	0.011	<0.5	0.0002	0.411
BR-17-20	423	424	1	0.0191	0.0018	0.016	<0.5	0.0002	0.198
BR-17-20	424	425	1	0.0458	0.0141	0.015	3	0.002	4.838
BR-17-20	425	426	1	0.0224	0.0028	0.014	0.7	0.0004	0.487
BR-17-20	426	427	1	0.0315	0.0039	0.008	0.7	0.0002	0.213
BR-17-20	427	428	1	0.0531	0.0099	0.022	6.7	0.0007	0.319
BR-17-20	428	429	1	0.0443	0.0079	0.008	0.5	0.0003	0.061
BR-17-20	429	430	1	0.0111	0.0084	0.007	<0.5	0.0005	0.061
BR-17-20	430	431	1	0.017	0.0188	0.009	0.6	0.0003	0.198
BR-17-20	431	432	1	0.0456	0.0081	0.006	<0.5	0.0003	0.091
BR-17-20	432	433	1	0.0288	0.0059	0.007	<0.5	0.0002	0.046
BR-17-20	433	434	1	0.0705	0.0199	0.011	8.5	0.0019	0.106
BR-17-20	434	435	1	0.0316	0.0053	0.019	0.9	0.0004	0.365
BR-17-20	435	436	1	0.0277	0.0051	0.008	<0.5	0.0002	0.061
BR-17-20	436	437	1	0.006	0.0049	0.009	<0.5	0.0002	0.03
BR-17-20	437	438	1	0.105	0.135	0.032	6.3	0.0012	0.137
BR-17-20	438	439.4	1.4	0.0077	<0.005	0.011	<0.5	0.0003	0.046
BR-17-20	439.4	440	0.6	0.0123	0.0017	0.01	<0.5	0.0003	0.046
BR-17-20	440	441	1	0.016	0.009	0.016	2.9	0.0005	0.091
BR-17-20	441	442	1	0.292	0.121	0.064	35.2	0.0106	2.495
BR-17-20	442	443	1	0.0306	0.0198	0.025	5.6	0.0014	0.715
BR-17-20	443	444	1	0.0044	0.0035	0.017	1.4	0.0007	0.046
BR-17-20	444	445	1	0.0067	0.0023	0.018	0.5	0.0005	0.076
BR-17-20	445	446	1	0.014	0.0087	0.026	2.1	0.0005	0.274
BR-17-20	446	447.2	1.2	0.0596	0.0264	0.034	7.8	0.0017	0.411
BR-17-20	447.2	448	0.8	0.0349	0.0136	0.02	2.8	0.0007	0.076
BR-17-20	448	449	1	0.0322	0.0582	0.017	3.6	0.0008	0.106
BR-17-20	449	450	1	0.0592	0.0725	0.022	7.9	0.0029	2.023

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-17-20	450	451	1	0.0222	0.0112	0.016	1.4	0.0005	2.419
BR-17-20	451	452	1	0.0044	<0.005	0.028	0.7	0.0004	0.821
BR-17-20	452	453	1	0.0162	0.0103	0.015	1	0.0005	0.076
BR-17-20	453	454	1	0.0124	0.0074	0.012	0.5	0.0003	0.517
BR-17-20	454	455	1	0.109	0.0188	0.011	1.3	0.0004	0.243
BR-17-20	455	456	1	0.0326	0.011	0.012	0.5	0.0002	0.046
BR-17-20	456	457	1	0.0151	0.003	0.011	<0.5	0.0002	0.046
BR-17-20	457	458	1	0.0767	0.0132	0.02	1.6	0.0017	0.456
BR-17-20	458	459	1	0.0458	0.0066	0.017	1.8	0.0021	0.046
BR-17-20	459	460	1	0.0244	0.0045	0.013	<0.5	0.0005	0.061
BR-17-20	460	461	1	0.0182	0.0017	0.01	<0.5	0.0003	0.046
BR-17-20	461	462	1	0.0135	0.0059	0.009	1.2	0.0035	0.046
BR-17-20	462	463	1	0.0088	0.0023	0.008	<0.5	0.0006	0.03
BR-17-20	463	464	1	0.011	0.0205	0.009	8.3	0.0234	0.03
BR-17-20	464	465	1	0.0122	0.0023	0.006	<0.5	0.0013	0.046
BR-17-20	465	466	1	0.0144	0.0014	<0.005	<0.5	0.0016	0.046
BR-17-20	466	467	1	0.0111	0.0023	<0.005	<0.5	0.0004	0.046
BR-17-20	467	468	1	0.0099	0.0015	0.005	<0.5	0.0014	0.03
BR-17-20	468	469	1	0.0084	0.001	0.011	<0.5	0.0004	0.046
BR-17-20	469	470	1	0.0115	0.0011	0.018	<0.5	0.007	0.061
BR-17-20	470	471	1	0.0549	0.0014	0.007	<0.5	0.0012	0.259
BR-17-20	471	472	1	0.0141	0.0024	0.012	<0.5	0.0035	0.03
BR-17-20	472	473	1	0.0055	0.0031	0.006	<0.5	0.0023	0.061
BR-17-20	473	474	1	0.0163	0.0013	0.01	<0.5	0.0104	0.046
BR-17-20	474	475	1	0.0061	0.0013	0.027	<0.5	0.0013	0.061
BR-17-20	475	476	1	0.0046	0.0011	0.009	<0.5	0.0024	0.03
BR-17-20	476	477	1	0.0093	0.001	0.008	<0.5	0.0036	0.03
BR-17-20	477	478	1	0.0053	0.0007	0.009	<0.5	0.0013	0.03
BR-17-20	478	479	1	0.0122	0.0012	0.007	<0.5	0.0082	0.046
BR-17-20	479	480	1	0.0085	0.0099	0.007	<0.5	0.0085	0.152
BR-17-20	480	481.2	1.2	0.0281	0.007	0.008	<0.5	0.0018	1.065
BR-17-20	481.2	482.4	1.2	0.0076	0.0009	<0.005	<0.5	0.0004	0.046
BR-17-20	482.4	483.6	1.2	0.0077	0.0011	<0.005	<0.5	0.0018	0.046
BR-17-20	483.6	484.8	1.2	0.0075	0.0014	0.006	<0.5	0.0018	0.091
BR-17-20	484.8	486	1.2	0.0074	0.0016	0.006	<0.5	0.0006	0.046
BR-17-20	486	487.2	1.2	0.0086	0.0019	0.006	<0.5	0.0027	0.046
BR-17-20	487.2	488.4	1.2	0.0119	0.0035	0.011	1.7	0.0089	0.198
BR-17-20	488.4	489.6	1.2	0.0192	0.0074	0.008	1.1	0.0185	0.046
BR-17-20	489.6	490.8	1.2	0.0209	0.0022	0.008	<0.5	0.0015	0.046
BR-17-20	490.8	492	1.2	0.008	0.0011	<0.005	<0.5	0.0004	0.061
BR-17-20	492	493	1	0.0102	0.0038	0.007	<0.5	0.0021	0.076
BR-17-20	493	494	1	0.0155	0.0026	0.005	<0.5	0.0012	0.122
BR-17-20	494	495	1	0.008	0.0015	0.012	0.6	0.0055	0.106
BR-17-20	495	496	1	0.007	0.0009	0.006	<0.5	0.0007	0.046
BR-17-20	496	497	1	0.0072	0.0007	<0.005	<0.5	0.0003	0.046
BR-17-20	497	498	1	0.0061	0.0008	<0.005	<0.5	0.0002	0.046
BR-17-20	498	498.5	0.5	0.0121	0.0011	<0.005	<0.5	0.0003	0.061

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-18-20	0	135	No sample						
BR-18-20	135	137	2	0.01	0.001	<0.005	<0.5	0.0002	0.03

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-18-20	137	139	2	0.009	0.0012	<0.005	<0.5	0.0006	0.106
BR-18-20	139	141	2	0.0084	0.0013	<0.005	<0.5	0.0002	0.03
BR-18-20	141	143	2	0.0077	0.001	<0.005	<0.5	0.0002	0.046
BR-18-20	143	145	2	0.0087	0.001	<0.005	<0.5	0.0015	0.319
BR-18-20	145	147	2	0.0082	0.0013	<0.005	<0.5	0.0001	0.03
BR-18-20	147	149	2	0.0074	0.0009	<0.005	<0.5	0.0001	0.046
BR-18-20	149	151	2	0.0073	0.0006	<0.005	<0.5	0.0001	0.046
BR-18-20	151	153	2	0.0102	0.0011	<0.005	<0.5	0.0001	0.046
BR-18-20	153	155	2	0.0093	0.0007	0.005	<0.5	0.0003	0.046
BR-18-20	155	157	2	0.0128	0.0034	0.008	0.6	0.0014	0.076
BR-18-20	157	159	2	0.0075	0.001	<0.005	<0.5	0.0002	0.046
BR-18-20	159	161	2	0.0073	0.001	<0.005	<0.5	0.0001	0.046
BR-18-20	161	162	1	0.0067	0.0007	<0.005	<0.5	0.0001	0.061
BR-18-20	162	163	1	0.0068	0.0007	<0.005	<0.5	0.0002	0.152
BR-18-20	163	164	1	0.0066	0.0009	0.006	<0.5	0.0001	0.061
BR-18-20	164	165	1	0.0069	0.0007	<0.005	<0.5	0.0001	0.35
BR-18-20	165	166	1	0.0065	0.001	<0.005	<0.5	0.0001	0.061
BR-18-20	166	167	1	0.0067	0.0009	<0.005	<0.5	0.0001	0.061
BR-18-20	167	168	1	0.0063	0.0008	<0.005	<0.5	0.0001	0.091
BR-18-20	168	169	1	0.0062	0.0007	<0.005	<0.5	0.0001	0.076
BR-18-20	169	170.15	1.15	0.006	0.0009	<0.005	<0.5	0.0001	0.046
BR-18-20	170.15	171	0.85	0.0055	0.0009	<0.005	<0.5	0.0005	0.137
BR-18-20	171	172	1	0.006	0.001	<0.005	<0.5	0.0004	0.183
BR-18-20	172	173.1	1.1	0.0064	0.0011	<0.005	<0.5	0.0073	0.639
BR-18-20	173.1	173.9	0.8	0.0039	0.0048	0.202	1	0.0066	5.994
BR-18-20	173.9	174.7	0.8	0.0292	0.0113	0.134	2.1	0.0191	2.297
BR-18-20	174.7	175.5	0.8	1.495	1.025	0.483	86.9	0.874	26.926
BR-18-20	175.5	176.5	1	1.105	0.849	0.515	69.3	1.17	38.944
BR-18-20	176.5	177.5	1	0.341	0.189	0.58	28.5	0.886	41.834
BR-18-20	177.5	178.5	1	1.365	0.749	0.845	90.8	0.847	24.644
BR-18-20	178.5	179.5	1	0.689	1.02	0.328	98	1.39	44.116
BR-18-20	179.5	180.8	1.3	2.09	1.545	0.915	136	0.568	54.308
BR-18-20	180.8	181.3	0.5	1.005	2.19	1.45	155	0.943	85.189
BR-18-20	181.3	182	0.7	1.845	2.03	1.325	167	0.548	88.688
BR-18-20	182	182.5	0.5	2.07	2.35	1.14	393	0.576	85.189
BR-18-20	182.5	183	0.5	7.7	3.93	3.61	455	0.517	74.997
BR-18-20	183	183.7	0.7	3.6	1.71	1.495	312	0.311	44.42
BR-18-20	183.7	184.5	0.8	0.13	0.367	0.035	6.4	0.036	0.837
BR-18-20	184.5	185.5	1	0.107	0.0309	0.02	6	0.0038	0.669
BR-18-20	185.5	186.5	1	0.0978	0.166	0.005	5.2	0.0083	0.487
BR-18-20	186.5	187.5	1	0.0594	0.0256	<0.005	4.7	0.001	0.091
BR-18-20	187.5	188.5	1	0.0238	0.124	<0.005	5.8	0.0131	0.456
BR-18-20	188.5	189.5	1	0.0105	0.0771	<0.005	3.4	0.0087	1.521
BR-18-20	189.5	190.4	0.9	0.0237	0.0423	<0.005	4.5	0.0148	1.582
BR-18-20	190.4	192.4	2	0.0137	0.0937	0.016	2.4	0.0133	1.384
BR-18-20	192.4	194	1.6	0.228	0.226	0.014	4.7	0.0169	0.137
BR-18-20	194	196	2	0.15	0.241	0.012	1.7	0.0132	1.536
BR-18-20	196	197.4	1.4	0.0639	0.395	0.012	3	0.0115	3.544
BR-18-20	197.4	198.4	1	0.0057	0.0065	<0.005	<0.5	0.0023	0.061
BR-18-20	198.4	199.4	1	0.0036	0.0016	<0.005	<0.5	0.001	0.03
BR-18-20	199.4	200.4	1	0.0049	0.0021	<0.005	<0.5	0.0028	0.046

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-18-20	200.4	201	0.6	0.0066	0.0011	<0.005	0.9	0.0126	0.046
BR-18-20	201	201.3	0.3	No sample					
BR-18-20	201.3	202.3	1	0.0051	0.0028	<0.005	<0.5	0.0017	0.106
BR-18-20	202.3	202.8	0.5	No sample					
BR-18-20	202.8	204.8	2	0.0069	0.002	<0.005	<0.5	0.0011	0.015
BR-18-20	204.8	206.8	2	0.0066	0.002	<0.005	<0.5	0.0011	0.03
BR-18-20	206.8	208.8	2	0.0067	0.0103	<0.005	<0.5	0.0026	0.03
BR-18-20	208.8	210.8	2	0.0089	0.004	<0.005	<0.5	0.0022	0.061
BR-18-20	210.8	212.8	2	0.0112	0.0111	0.037	<0.5	0.0104	0.03
BR-18-20	212.8	214.8	2	0.015	0.137	0.048	1.3	0.0316	0.167
BR-18-20	214.8	216.8	2	0.0067	0.0034	<0.005	<0.5	0.0018	0.198
BR-18-20	216.8	218.8	2	0.0064	0.003	<0.005	<0.5	0.0015	0.03
BR-18-20	218.8	220.8	2	0.0102	0.0058	<0.005	<0.5	0.0042	0.03
BR-18-20	220.8	222.8	2	0.008	0.0152	0.007	<0.5	0.0034	1.445
BR-18-20	222.8	224.2	1.4	0.0088	0.0048	0.009	<0.5	0.0031	0.03
BR-18-20	224.2	225	0.8	0.07	0.0568	0.026	1.2	0.0153	0.015
BR-18-20	225	226	1	0.0558	0.105	0.032	1.6	0.0186	0.122
BR-18-20	226	227	1	0.134	0.108	0.012	5.6	0.0088	0.532
BR-18-20	227	228	1	0.0604	0.152	0.04	1.6	0.0252	3.544
BR-18-20	228	229	1	0.0781	0.13	0.037	1.2	0.0167	1.749
BR-18-20	229	231	2	0.197	0.426	0.253	2.4	0.0157	9.493
BR-18-20	231	233	2	0.675	1.015	0.261	10.3	0.0441	0.365
BR-18-20	233	235	2	0.54	0.249	0.07	113	0.05	0.426
BR-18-20	235	237	2	0.239	0.115	0.059	45.4	0.0097	0.183
BR-18-20	237	239	2	0.876	0.28	0.145	69.4	0.0376	0.837
BR-18-20	239	241	2	0.259	0.128	0.053	16	0.0172	0.183
BR-18-20	241	243	2	0.328	0.176	0.044	38.1	0.0334	0.867
BR-18-20	243	245	2	0.0697	0.187	0.079	48.8	0.0304	0.487
BR-18-20	245	247	2	0.267	0.346	0.132	86	0.0303	1.749
BR-18-20	247	249	2	0.155	0.364	0.106	162	0.0408	1.278
BR-18-20	249	251	2	0.212	0.194	0.057	81.3	0.0202	0.426
BR-18-20	251	253	2	0.327	0.112	0.039	51.4	0.0086	0.821
BR-18-20	253	255	2	0.335	0.0954	0.042	47.5	0.0108	0.426
BR-18-20	255	257	2	0.325	0.0831	0.019	39.4	0.011	0.821
BR-18-20	257	259	2	0.113	0.0544	0.013	25	0.022	0.106
BR-18-20	259	261	2	0.2	0.132	0.052	38.4	0.0327	0.243
BR-18-20	261	263	2	0.123	0.0807	0.083	16.9	0.0162	0.304
BR-18-20	263	265	2	0.237	0.0733	0.056	96.6	0.0296	0.396
BR-18-20	265	267	2	0.451	0.113	0.024	116	0.0433	0.228
BR-18-20	267	269	2	0.156	0.0504	0.024	28.2	0.0097	0.167
BR-18-20	269	271	2	0.0898	0.0391	0.013	4.8	0.0046	0.38
BR-18-20	271	272.5	1.5	0.0655	0.0184	<0.005	2.9	0.0015	0.426
BR-18-20	272.5	273.1	0.6	0.0568	0.0203	<0.005	4.1	0.0027	0.213
BR-18-20	273.1	275	1.9	0.0182	0.0048	0.005	2.6	0.0016	0.213
BR-18-20	275	277	2	0.0625	0.0164	<0.005	3.3	0.0018	0.365
BR-18-20	277	279	2	0.0837	0.021	<0.005	6	0.0028	0.183
BR-18-20	279	281	2	0.0317	0.0076	<0.005	4.4	0.0019	0.137
BR-18-20	281	283	2	0.0257	0.0061	<0.005	2.8	0.0013	0.137
BR-18-20	283	285	2	0.0394	0.0063	<0.005	5.2	0.0015	0.335
BR-18-20	285	287	2	0.0244	0.0069	<0.005	4.5	0.0016	0.183
BR-18-20	287	289	2	0.0339	0.0047	<0.005	3.4	0.0017	0.152

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-18-20	289	291	2	0.0171	0.0041	<0.005	3.8	0.0012	0.517
BR-18-20	291	293	2	0.0143	0.0036	<0.005	4	0.0013	0.137
BR-18-20	293	294.5	1.5	0.023	0.0103	<0.005	2.7	0.0023	0.411
BR-18-20	294.5	296.5	2	0.0335	0.0216	<0.005	2.5	<0.005	0.198
BR-18-20	296.5	297.1	0.6	0.0345	0.016	<0.005	1	0.003	0.046
BR-18-20	297.1	299	1.9	0.0397	0.012	<0.005	<0.5	0.0027	0.122
BR-18-20	299	301	2	0.0152	0.005	<0.005	1.9	0.0022	0.198
BR-18-20	301	303	2	0.0491	0.021	<0.005	4.7	0.0026	0.396
BR-18-20	303	305	2	0.0224	0.0115	0.006	11.6	0.003	0.319
BR-18-20	305	307	2	0.0145	0.0143	<0.005	12.2	0.0021	0.35
BR-18-20	307	309	2	0.0279	0.0146	<0.005	7.8	0.0019	0.35
BR-18-20	309	311	2	0.0116	0.007	<0.005	9.9	0.0022	0.243
BR-18-20	311	313	2	0.042	0.0122	<0.005	6.5	0.0014	0.335
BR-18-20	313	315	2	0.0584	0.0284	<0.005	24	0.0051	1.019
BR-18-20	315	317	2	0.016	0.0061	<0.005	11.9	0.0031	0.487
BR-18-20	317	319	2	0.0133	0.007	0.005	6.8	0.0018	0.502
BR-18-20	319	321	2	0.0334	0.0129	<0.005	4.5	0.003	0.487
BR-18-20	321	323	2	0.0151	0.0039	<0.005	1.4	0.0016	0.198
BR-18-20	323	325	2	0.0324	0.0073	<0.005	2.4	0.0021	0.487
BR-18-20	325	327	2	0.0155	0.0047	<0.005	1.8	0.0018	0.304
BR-18-20	327	329	2	0.0204	0.0085	<0.005	2.4	0.0029	0.365
BR-18-20	329	331	2	0.0271	0.0078	<0.005	1.9	<0.005	0.335
BR-18-20	331	333	2	0.0338	0.0077	<0.005	2.4	0.0018	0.472
BR-18-20	333	335	2	0.0337	0.0117	<0.005	2	0.0015	0.441
BR-18-20	335	337	2	0.0239	0.0725	0.005	4.9	0.003	0.989
BR-18-20	337	338	1	0.0243	0.0607	0.009	14.6	0.0069	0.958
BR-18-20	338	339	1	0.161	0.0736	0.011	13.1	0.0023	1.491
BR-18-20	339	340	1	0.291	0.142	0.057	39.8	0.0059	4.168
BR-18-20	340	341	1	0.257	0.107	0.025	18.8	0.0028	1.582
BR-18-20	341	342.4	1.4	0.176	0.109	0.008	36.4	0.0067	0.776
BR-18-20	342.4	344	1.6	0.0467	0.01	0.005	7.9	0.0029	0.274
BR-18-20	344	346	2	0.0094	0.0029	<0.005	1.5	0.0024	0.183
BR-18-20	346	348	2	0.0121	0.0007	<0.005	<0.5	0.0003	0.076
BR-18-20	348	350	2	0.0108	0.0016	<0.005	<0.5	0.0038	0.091
BR-18-20	350	352	2	0.0083	0.0012	<0.005	<0.5	0.0018	0.228
BR-18-20	352	354	2	0.0081	0.0014	<0.005	<0.5	0.0036	0.076
BR-18-20	354	356	2	0.0071	0.0008	<0.005	<0.5	0.001	0.076
BR-18-20	356	357	1	0.0069	0.001	<0.005	<0.5	0.0028	0.091
BR-18-20	357	358.8	1.8	0.0074	0.0008	<0.005	<0.5	0.0005	0.137
BR-18-20	358.8	360	1.2	0.0071	0.0008	<0.005	<0.5	0.0013	0.076
BR-18-20	360	361	1	0.0077	0.0008	0.007	<0.5	0.0035	0.046
BR-18-20	361	362.2	1.2	0.0073	0.0009	<0.005	<0.5	0.0018	0.091
BR-18-20	362.2	364	1.8	0.0073	0.0009	<0.005	<0.5	0.001	0.076
BR-18-20	364	366	2	0.0062	0.0008	<0.005	<0.5	0.0024	0.061
BR-18-20	366	368	2	0.0057	0.0006	<0.005	<0.5	0.001	0.076
BR-18-20	368	370	2	0.0054	0.0006	<0.005	<0.5	0.0016	0.061
BR-18-20	370	372	2	0.0068	0.0005	<0.005	<0.5	0.0065	0.106
BR-18-20	372	374	2	0.0071	0.0005	<0.005	<0.5	0.0022	0.122
BR-18-20	374	376	2	0.0052	0.0006	<0.005	<0.5	0.0012	0.106
BR-18-20	376	378	2	0.0058	0.0007	0.007	<0.5	0.0005	0.091
BR-18-20	378	380	2	0.0058	0.0008	0.006	<0.5	0.0011	0.091

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-18-20	380	380.9	0.9	0.0046	0.0005	0.007	<0.5	0.0031	0.03
BR-18-20	380.9	382.4	1.5	0.0065	0.0008	0.008	<0.5	0.0013	0.076
BR-18-20	382.4	384	1.6	0.0048	0.0004	0.009	<0.5	0.0018	0.183
BR-18-20	384	386	2	0.005	0.0003	<0.005	<0.5	0.0006	0.076
BR-18-20	386	388	2	0.0072	0.0011	0.009	<0.5	0.0034	0.061
BR-18-20	388	390	2	0.006	0.0012	0.014	<0.5	0.0006	0.046
BR-18-20	390	392	2	0.0055	0.0009	0.009	<0.5	0.0019	0.046
BR-18-20	392	394	2	0.0046	0.0006	0.02	<0.5	0.0023	0.046
BR-18-20	394	396	2	0.0064	0.0006	0.022	<0.5	0.0016	0.046
BR-18-20	396	398	2	0.0067	0.0007	0.009	<0.5	0.0011	0.046
BR-18-20	398	400	2	0.0056	0.0006	0.015	<0.5	0.0005	0.046
BR-18-20	400	402	2	0.0057	0.0003	0.009	<0.5	0.0012	0.03
BR-18-20	402	404	2	0.0062	0.0003	0.008	<0.5	0.0006	0.046
BR-18-20	404	406	2	0.0061	0.0005	0.008	<0.5	0.0006	0.091
BR-18-20	406	408	2	0.0081	0.0005	0.009	<0.5	0.002	0.03
BR-18-20	408	410	2	0.0072	0.0006	0.006	<0.5	0.0021	0.091
BR-18-20	410	412	2	0.0079	0.0006	0.005	<0.5	0.002	0.076
BR-18-20	412	414	2	0.007	0.001	0.005	<0.5	0.0021	0.046
BR-18-20	414	416	2	0.011	0.0017	0.043	<0.5	0.0041	0.152
BR-18-20	416	418	2	0.0084	0.0017	0.018	<0.5	0.0026	0.319
BR-18-20	418	420	2	0.0102	0.0021	0.009	<0.5	0.0019	0.137
BR-18-20	420	422	2	0.0168	0.0019	0.015	<0.5	0.0011	0.046
BR-18-20	422	432	10	No sample					
BR-18-20	432	434	2	0.0091	0.0009	0.008	<0.5	0.001	0.03
BR-18-20	434	435	1	0.0268	0.0012	0.005	<0.5	0.0006	0.122
BR-18-20	435	436.3	1.3	0.0307	0.0017	0.007	<0.5	0.0008	0.578
BR-18-20	436.3	437	0.7	0.0085	0.0076	0.046	<0.5	0.002	0.106
BR-18-20	437	438.3	1.3	0.0141	0.0033	0.022	<0.5	0.0006	0.091
BR-18-20	438.3	440	1.7	0.0113	0.0028	0.011	<0.5	0.0012	0.046
BR-18-20	440	442	2	0.0161	0.0018	0.005	<0.5	0.0009	0.228
BR-18-20	442	444	2	0.0119	0.0017	0.011	<0.5	0.0013	0.091
BR-18-20	444	446	2	0.0104	0.0018	0.005	<0.5	0.0011	0.091
BR-18-20	446	448	2	0.0121	0.0045	<0.005	<0.5	0.0014	0.076
BR-18-20	448	450	2	0.0121	0.0106	0.022	0.5	0.0017	0.106
BR-18-20	450	451	1	0.0171	0.0042	0.014	<0.5	0.0008	0.502
BR-18-20	451	452.6	1.6	0.215	0.0088	0.017	0.8	0.0066	0.167
BR-18-20	452.6	454	1.4	0.0165	0.0078	0.01	0.5	0.0203	0.441
BR-18-20	454	456	2	0.0089	0.0027	0.009	<0.5	0.004	0.122
BR-18-20	456	457	1	0.0088	0.0008	<0.005	<0.5	0.0002	0.122
BR-18-20	457	458.4	1.4	0.0101	0.0008	<0.005	<0.5	0.0078	0.198
BR-18-20	458.4	460	1.6	0.0086	0.0009	0.008	<0.5	0.0002	0.076
BR-18-20	460	461	1	0.0094	0.0006	0.007	<0.5	0.0001	0.152
BR-18-20	461	462.3	1.3	0.0094	0.0011	<0.005	<0.5	0.0001	0.122
BR-18-20	462.3	464	1.7	0.0108	0.0012	<0.005	<0.5	0.0012	0.152
BR-18-20	464	466	2	0.0083	0.0036	0.009	<0.5	0.002	0.091
BR-18-20	466	468	2	0.0088	0.0027	<0.005	<0.5	0.0018	0.076
BR-18-20	468	469	1	0.0182	0.0045	0.042	0.5	0.0021	0.152
BR-18-20	469	470.2	1.2	0.0317	0.0033	0.019	<0.5	0.0015	0.213
BR-18-20	470.2	471.4	1.2	No sample					
BR-18-20	471.4	472.5	1.1	0.0085	0.0005	<0.005	<0.5	0.0002	0.046
BR-18-20	472.5	474.5	2	0.0111	0.0008	<0.005	<0.5	0.0002	0.091

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-18-20	474.5	476.5	2	0.0101	0.001	<0.005	<0.5	0.0003	0.106
BR-18-20	476.5	478.5	2	0.009	0.0011	<0.005	<0.5	0.0018	0.183
BR-18-20	478.5	480.5	2	0.0107	0.0015	0.007	<0.5	0.0008	0.152
BR-18-20	480.5	482.5	2	0.0101	0.0021	0.009	<0.5	0.0015	0.411
BR-18-20	482.5	484.5	2	0.0296	0.0163	0.01	1.2	0.0044	0.122
BR-18-20	484.5	485.1	0.6	0.013	0.0029	<0.005	<0.5	0.0037	0.046
BR-18-20	485.1	486.5	1.4	0.0108	0.0037	<0.005	<0.5	0.0032	0.061
BR-18-20	486.5	488.5	2	0.0135	0.001	<0.005	<0.5	0.0013	0.046
BR-18-20	488.5	490.5	2	0.0121	0.0057	0.005	<0.5	0.0227	0.213
BR-18-20	490.5	492.5	2	0.0103	0.0053	0.005	<0.5	0.0011	0.122
BR-18-20	492.5	494.5	2	0.0112	0.0059	<0.005	<0.5	0.0046	0.091
BR-18-20	494.5	496.5	2	0.0103	0.0008	<0.005	<0.5	0.0012	0.061
BR-18-20	496.5	498.5	2	0.0124	0.0005	<0.005	<0.5	0.0007	0.076
BR-18-20	498.5	500	1.5	0.0136	0.0049	0.006	<0.5	0.0081	0.061
BR-18-20	500	501	1	0.0138	0.0019	<0.005	<0.5	0.0114	0.106
BR-18-20	501	502.1	1.1	0.0093	0.0035	<0.005	1	0.163	0.061
BR-18-20	502.1	504	1.9	0.0106	0.0013	<0.005	<0.5	0.066	0.076
BR-18-20	504	506	2	0.0116	0.0009	<0.005	<0.5	0.0119	0.152
BR-18-20	506	508	2	0.0124	0.0012	0.007	<0.5	0.0005	0.076
BR-18-20	508	510	2	0.0214	0.0144	0.005	<0.5	0.028	0.152
BR-18-20	510	512	2	0.0205	0.0154	0.007	0.7	0.0093	0.426
BR-18-20	512	513.4	1.4	0.0114	0.0028	0.01	<0.5	0.0112	0.106
BR-18-20	513.4	514.1	0.7	0.0119	0.0008	0.013	<0.5	0.0004	0.228
BR-18-20	514.1	515.7	1.6	0.0133	0.0013	0.006	<0.5	0.0014	0.122
BR-18-20	515.7	517	1.3	0.0093	0.0009	<0.005	<0.5	0.0002	0.061
BR-18-20	517	519	2	0.0091	0.0005	0.007	<0.5	0.0003	0.076
BR-18-20	519	521	2	0.0081	0.0007	0.006	<0.5	0.0001	0.076
BR-18-20	521	522.6	1.6	0.0081	0.0005	<0.005	<0.5	0.0001	0.152
BR-18-20	522.6	524	1.4	0.0049	0.0012	0.006	<0.5	0.0004	0.137
BR-18-20	524	526	2	0.0122	0.0011	0.019	<0.5	0.002	0.106
BR-18-20	526	528	2	0.0132	0.0034	<0.005	<0.5	0.0018	0.061
BR-18-20	528	530	2	0.0136	0.0057	0.033	<0.5	0.0372	0.076
BR-18-20	530	532	2	0.0133	0.0028	0.009	<0.5	0.0021	0.167
BR-18-20	532	534	2	0.0112	0.0015	0.006	<0.5	0.0013	0.076
BR-18-20	534	536	2	0.0107	0.0012	<0.005	<0.5	0.0014	0.046
BR-18-20	536	537.7	1.7	0.0131	0.0022	0.007	<0.5	0.0023	0.274
BR-18-20	537.7	539	1.3	0.0079	0.0241	0.012	0.8	0.005	0.106
BR-18-20	539	541	2	0.0049	0.0026	0.011	<0.5	0.0004	0.061
BR-18-20	541	543	2	0.0079	0.0007	<0.005	<0.5	0.0002	0.061
BR-18-20	543	545	2	0.0099	0.0009	<0.005	<0.5	0.0002	0.061
BR-18-20	545	547	2	0.0051	0.0006	<0.005	<0.5	0.0001	0.046
BR-18-20	547	549	2	0.0059	0.0007	<0.005	<0.5	0.0001	0.046
BR-18-20	549	551	2	0.004	0.0007	0.007	<0.5	0.0005	0.046
BR-18-20	551	553	2	0.0049	0.0018	<0.005	<0.5	0.0002	0.152
BR-18-20	553	555	2	0.0055	0.0008	<0.005	<0.5	0.0016	0.061
BR-18-20	555	557	2	0.005	0.001	<0.005	<0.5	0.0122	0.046
BR-18-20	557	558	1	0.0067	0.0018	<0.005	<0.5	0.0001	0.091
BR-18-20	558	560	2	0.0081	0.001	0.006	<0.5	0.0001	0.046
BR-18-20	560	562	2	0.0056	0.0026	0.014	<0.5	0.0019	0.076
BR-18-20	562	564	2	0.0843	0.0281	0.144	1	0.0142	0.259
BR-18-20	564	566	2	0.0035	0.0012	0.019	<0.5	0.0004	0.076

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-18-20	566	568	2	0.0045	0.0014	0.007	<0.5	0.0012	0.122
BR-18-20	568	570	2	0.004	0.0011	0.005	<0.5	0.0003	0.091
BR-18-20	570	572	2	0.004	0.0007	<0.005	<0.5	0.0001	0.061
BR-18-20	572	574	2	0.0062	0.0106	<0.005	1.6	0.0202	0.137
BR-18-20	574	576	2	0.0026	0.0031	0.017	0.6	0.0044	0.304
BR-18-20	576	578	2	0.0029	0.006	0.008	0.7	0.0091	0.122
BR-18-20	578	580	2	0.0114	0.0206	0.005	1.5	0.054	0.563
BR-18-20	580	582	2	0.0036	0.0023	0.006	<0.5	0.0009	0.137
BR-18-20	582	584	2	0.0059	0.0013	0.005	<0.5	0.0002	0.091
BR-18-20	584	586	2	0.005	0.001	<0.005	<0.5	0.0001	0.061
BR-18-20	586	587	1	0.0039	0.0009	0.007	<0.5	0.0001	0.076
BR-18-20	587	588.3	1.3	0.0036	0.0016	0.022	<0.5	0.0002	0.076
BR-18-20	588.3	590	1.7	0.0058	0.0023	<0.005	<0.5	0.0001	0.167
BR-18-20	590	592	2	0.0057	0.0008	0.011	<0.5	0.0001	0.228
BR-18-20	592	594	2	0.0062	0.0008	0.008	<0.5	0.0001	0.076
BR-18-20	594	596	2	0.0047	0.0008	0.005	<0.5	0.0001	0.076
BR-18-20	596	598	2	0.0034	0.0007	<0.005	<0.5	0.0001	0.091
BR-18-20	598	600	2	0.0056	0.0022	0.006	<0.5	0.0001	0.228
BR-18-20	600	602	2	0.0093	0.0016	0.026	<0.5	0.0001	0.228
BR-18-20	602	604	2	0.0055	0.0009	<0.005	<0.5	<0.0001	0.106
BR-18-20	604	606	2	0.0063	0.0028	<0.005	<0.5	0.0001	0.076
BR-18-20	606	607	1	0.0073	0.0019	0.014	<0.5	0.0001	0.122

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-20-20	225	227	2	0.0094	0.0049	0.054	2.9	0.0033	0.122
BR-20-20	227	228.2	1.2	0.0346	0.0852	0.024	7.1	0.0201	1.871
BR-20-20	228.2	229	0.8	1.56	1.58	0.537	112	0.291	53.091
BR-20-20	229	230	1	0.116	1.01	0.6	75.9	0.157	54.004
BR-20-20	230	231	1	0.739	1.55	0.618	85.2	0.424	38.335
BR-20-20	231	232	1	1.305	0.851	0.5	141	0.612	11.577
BR-20-20	232	233.2	1.2	1.105	0.423	0.4	46	0.0431	4.853
BR-20-20	233.2	234	0.8	1.505	2.64	0.666	164	0.796	31.185
BR-20-20	234	235	1	3.35	2.74	0.858	229	0.993	28.295
BR-20-20	235	235.5	0.5	2.64	2.33	0.719	226	0.931	30.197
BR-20-20	235.5	237	1.5	1.4	0.929	0.327	50.2	0.185	8.291
BR-20-20	237	238	1	3.14	2.07	0.502	40.7	0.562	1.323
BR-20-20	238	239	1	0.259	0.181	0.109	7.6	0.0662	2.647
BR-20-20	239	240	1	0.488	0.366	0.15	8.1	0.0676	0.761
BR-20-20	240	241	1	0.395	0.303	0.111	7.9	0.154	0.046
BR-20-20	241	241.5	0.5	0.207	0.0326	0.076	2	0.0117	1.552
BR-20-20	241.5	243	1.5	0.0125	0.0073	0.007	<0.5	0.004	0.882
BR-20-20	243	245	2	0.0109	0.0051	0.009	<0.5	0.0034	0.213
BR-20-20	245	247	2	0.0114	0.0127	0.007	<0.5	0.0037	0.122
BR-20-20	247	248.7	1.7	0.0097	0.0089	0.011	<0.5	0.0033	0.061
BR-20-20	248.7	250.2	1.5	0.0159	0.0015	<0.005	<0.5	0.0028	0.03
BR-20-20	250.2	252.2	2	0.0245	0.0018	<0.005	<0.5	0.0086	0.015

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-22-20	0	184	No sample						
BR-22-20	184	186	2	0.0409	0.0069	0.039	0.9	0.03	0.426

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-22-20	186	188	2	0.0227	0.0035	0.018	<0.5	0.0011	0.517
BR-22-20	188	190	2	0.41	0.1795	0.109	4.8	0.001	3.21
BR-22-20	190	192	2	0.031	0.002	0.016	<0.5	0.0012	0.152
BR-22-20	192	194	2	0.0232	0.0008	0.011	<0.5	0.001	0.03
BR-22-20	194	196	2	0.0103	0.0016	0.01	<0.5	0.0006	0.046
BR-22-20	196	198	2	0.0179	0.0008	0.017	<0.5	0.0006	0.008
BR-22-20	198	200	2	0.004	0.0053	0.02	<0.5	0.0009	0.046
BR-22-20	200	202	2	0.0092	0.0017	0.018	<0.5	0.0007	0.015
BR-22-20	202	204	2	0.0097	0.0032	0.038	<0.5	0.0015	0.015
BR-22-20	204	206	2	0.0102	0.0045	0.101	<0.5	<0.005	0.015
BR-22-20	206	208	2	0.0197	0.0031	0.09	<0.5	0.0013	0.03
BR-22-20	208	210	2	0.0085	0.0058	0.12	<0.5	0.0022	0.183
BR-22-20	210	212	2	0.0072	0.0211	0.176	0.7	0.0091	0.624
BR-22-20	212	214	2	0.0139	0.0082	0.113	0.6	0.0019	0.106
BR-22-20	214	216	2	0.143	0.246	0.329	2.1	0.0418	1.263
BR-22-20	216	218	2	0.0387	0.0358	0.4	2.1	0.133	0.046
BR-22-20	218	219.7	1.7	0.177	0.0265	0.256	1.5	0.0204	0.106
BR-22-20	219.7	220.7	1	0.169	0.291	0.905	8.6	0.472	0.046
BR-22-20	220.7	221.7	1	0.0183	0.009	0.178	1.3	0.0041	0.015
BR-22-20	221.7	222.7	1	0.0176	0.0111	0.143	0.8	0.0037	0.03
BR-22-20	222.7	223.7	1	0.0787	0.307	0.575	5.1	0.16	0.228
BR-22-20	223.7	224.7	1	0.104	0.1335	0.481	3.8	0.0502	1.187
BR-22-20	224.7	225.7	1	0.236	0.1465	0.921	7.8	0.117	1.719
BR-22-20	225.7	226.3	0.6	0.221	0.182	1.185	7.9	0.0752	0.7
BR-22-20	226.3	227	0.7	0.135	0.975	1.865	11.4	0.326	4.549
BR-22-20	227	228	1	0.211	0.0523	0.482	6.2	0.0829	6.648
BR-22-20	228	229	1	0.39	0.1055	0.652	16	0.281	4.853
BR-22-20	229	230	1	0.0372	0.0082	0.153	0.7	0.0108	0.122
BR-22-20	230	231	1	0.0518	0.0081	0.152	1	0.0092	0.624
BR-22-20	231	232	1	0.663	0.073	1.05	11.8	0.144	9.432
BR-22-20	232	233	1	0.209	0.0739	0.553	9	0.0355	3.453
BR-22-20	233	234	1	0.246	0.119	0.489	16.4	0.015	2.16
BR-22-20	234	235	1	0.0222	0.0223	0.502	5.1	0.0093	0.837
BR-22-20	235	236	1	0.0232	0.0127	0.555	2	0.0081	0.806
BR-22-20	236	237	1	0.0256	0.026	0.152	1.4	0.0051	0.061
BR-22-20	237	237.7	0.7	0.0294	0.051	0.383	3.7	0.0507	0.35
BR-22-20	237.7	238.2	0.5	0.281	0.169	1.83	33.3	2.19	1.78
BR-22-20	238.2	239.2	1	0.0196	0.0689	0.173	1.8	0.0493	0.685
BR-22-20	239.2	240.4	1.2	0.0983	0.131	0.927	7.6	0.122	2.464
BR-22-20	240.4	241.2	0.8	0.087	0.079	2.3	23.7	0.418	2.038
BR-22-20	241.2	242.1	0.9	0.0946	0.0209	0.414	3.8	0.175	5.218
BR-22-20	242.1	243.2	1.1	0.0034	0.0159	0.318	1.4	0.0057	1.917
BR-22-20	243.2	244.1	0.9	0.151	0.037	1.075	13.2	1.265	0.259
BR-22-20	244.1	245	0.9	0.141	0.0044	0.13	<0.5	0.0379	0.913
BR-22-20	245	246	1	0.231	0.0067	0.166	0.9	0.0107	2.951
BR-22-20	246	247	1	0.0472	0.0074	0.132	0.5	0.0038	0.898
BR-22-20	247	248	1	0.0043	0.0043	0.044	<0.5	0.0012	0.015
BR-22-20	248	249	1	0.0043	0.0087	0.203	0.6	0.0042	0.243
BR-22-20	249	250	1	0.0353	0.0115	0.189	<0.5	0.0101	0.137
BR-22-20	250	251	1	0.111	0.0125	0.237	1	0.0071	0.35
BR-22-20	251	252	1	0.0209	0.0055	0.107	<0.5	0.0014	0.167

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-22-20	252	253	1	0.193	0.009	0.334	2	0.0116	4.944
BR-22-20	253	254	1	0.13	0.0073	0.337	1.1	0.0042	10.497
BR-22-20	254	255.2	1.2	0.12	0.0125	0.488	1.6	0.0153	5.431
BR-22-20	255.2	256	0.8	0.213	0.0086	0.178	<0.5	0.0031	0.091
BR-22-20	256	257	1	0.21	0.0156	0.345	<0.5	0.0044	0.396
BR-22-20	257	258	1	0.216	0.0056	0.138	<0.5	0.0029	0.243
BR-22-20	258	259	1	0.651	0.0522	0.279	2.5	0.0286	0.061
BR-22-20	259	260	1	0.928	0.439	2.42	17.9	0.1115	0.958
BR-22-20	260	261	1	1.675	0.405	1.45	39.3	0.352	0.213
BR-22-20	261	262	1	0.606	0.201	0.395	11	0.047	1.141
BR-22-20	262	263	1	0.213	0.0807	0.32	3.6	0.0269	0.106
BR-22-20	263	264	1	0.34	0.132	0.751	5.1	0.0511	0.806
BR-22-20	264	265	1	0.0803	0.0116	0.537	2.6	0.249	0.578
BR-22-20	265	266	1	0.0218	0.0104	0.344	0.9	0.0047	0.259
BR-22-20	266	267	1	0.0746	0.0409	0.365	2.9	0.0275	0.7
BR-22-20	267	268	1	0.0517	0.0042	0.174	<0.5	0.0024	0.061
BR-22-20	268	269	1	0.022	0.0064	0.144	<0.5	0.0022	0.259
BR-22-20	269	270	1	0.109	0.0062	0.235	1.8	0.0034	0.274
BR-22-20	270	271	1	0.038	0.0045	0.153	1	0.0021	0.122
BR-22-20	271	272	1	0.137	0.0528	0.776	9.9	0.183	0.259
BR-22-20	272	273	1	0.0876	0.0763	0.626	5.9	0.073	0.106
BR-22-20	273	274	1	0.0695	0.0559	0.877	6.1	0.0096	0.152
BR-22-20	274	275	1	0.435	0.0184	0.619	4.3	0.0089	0.608
BR-22-20	275	276	1	0.596	0.0352	1.075	8.6	0.0222	0.289
BR-22-20	276	277	1	0.0539	0.0059	0.173	0.8	0.0044	0.243
BR-22-20	277	278	1	0.0724	0.0117	0.201	1.5	0.0086	0.319
BR-22-20	278	278.3	0.3	0.0113	0.0126	0.45	3.1	0.0074	0.958
BR-22-20	278.3	280	1.7	0.0168	0.0077	0.132	4.2	0.0026	0.152
BR-22-20	280	282	2	0.0135	0.0089	0.065	1.8	0.0024	0.122
BR-22-20	282	284	2	0.394	0.102	0.06	5.2	0.024	0.335
BR-22-20	284	286	2	0.237	0.0667	0.084	3.3	0.0073	1.232
BR-22-20	286	288	2	0.138	0.0371	0.04	2.1	0.0053	0.624
BR-22-20	288	290	2	0.0785	0.0155	0.032	0.7	0.0014	0.106
BR-22-20	290	292	2	0.208	0.0161	0.027	1.2	0.0047	0.715
BR-22-20	292	294	2	0.184	0.007	0.025	0.6	0.001	0.578
BR-22-20	294	295.6	1.6	0.0341	0.0031	0.023	0.5	0.0011	0.076
BR-22-20	295.6	297	1.4	0.0473	0.0115	0.022	<0.5	0.0022	0.076
BR-22-20	297	299	2	0.0093	0.005	0.03	0.5	0.0011	0.046
BR-22-20	299	301	2	0.0848	0.0092	0.025	<0.5	0.0008	0.046
BR-22-20	301	303	2	0.0683	0.0834	0.015	1	0.0006	0.076
BR-22-20	303	305	2	0.0654	0.0041	0.029	0.9	0.0009	0.091
BR-22-20	305	307	2	0.253	0.0385	0.033	6.9	0.0036	0.472
BR-22-20	307	309	2	1.57	0.392	0.041	30.7	0.0208	3.195
BR-22-20	309	311	2	0.996	0.238	0.036	24.5	0.0087	4.123
BR-22-20	311	312.7	1.7	0.592	0.0896	0.041	16.5	0.0097	2.495

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-23-20	0	320	No sample						
BR-23-20	320	322	2	0.0139	0.0024	0.01	<0.5	0.0038	0.243
BR-23-20	322	324	2	0.012	0.0029	0.005	<0.5	0.0007	0.548

Hole ID	From	To	Interval	Zn %	Pb %	Au g/t	Ag g/t	Cu %	$BaSO_4$
BR-23-20	324	325.7	1.7	0.0182	0.578	0.381	6.9	0.0109	51.418
BR-23-20	325.7	326.4	0.7	0.0233	0.586	0.363	11.1	0.0109	90.057
BR-23-20	326.4	327	0.6	0.11	0.0411	0.353	3.1	0.0035	80.474
BR-23-20	327	328	1	0.0063	0.401	0.348	5.6	0.0052	80.93
BR-23-20	328	329	1	0.0209	0.844	2.5	123	0.0942	75.149
BR-23-20	329	330	1	4.33	12.9	1.105	963	0.973	68.152
BR-23-20	330	331	1	0.622	8.26	2.04	741	0.872	80.017
BR-23-20	331	332	1	3.49	5.12	2.48	829	1.045	76.823
BR-23-20	332	333	1	10.9	7.05	1.09	325	0.641	66.782
BR-23-20	333	334	1	10.2	4.08	1.075	211	0.389	59.328
BR-23-20	334	335	1	8.15	3.65	0.891	268	0.314	58.568
BR-23-20	335	336	1	5.26	2.17	0.95	242	0.443	49.897
BR-23-20	336	337	1	2.2	1.15	1.09	196	0.319	42.747
BR-23-20	337	338	1	1.86	2.97	0.899	200	0.498	38.335
BR-23-20	338	338.6	0.6	1.88	1.55	1.035	274	0.409	11.257
BR-23-20	338.6	339.1	0.5	0.586	0.603	0.591	40.9	0.423	11.181
BR-23-20	339.1	340	0.9	0.365	0.107	0.516	26.9	1.06	47.158
BR-23-20	340	340.7	0.7	0.0495	0.11	0.15	4.4	0.111	2.693
BR-23-20	340.7	341.3	0.6	0.031	0.019	0.096	10.9	0.14	11.729
BR-23-20	341.3	342.6	1.3	0.992	0.804	0.421	49.7	0.273	7.028
BR-23-20	342.6	344	1.4	0.0234	0.0288	0.054	1	0.0033	3.879
BR-23-20	344	346	2	0.0216	0.006	0.008	<0.5	0.0081	0.289
BR-23-20	346	368	22	No sample					

APPENDIX 1: RUPICE MRE JORC TABLES

Section 1 Sampling Techniques and Data
(Criteria in this section apply to all succeeding sections.)

<table>
<tr><th>Criteria</th><th>JORC Code Explanation</th><th>Commentary</th></tr>
<tr><td rowspan="3">Sampling techniques</td><td>Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</td><td>PQ3 and HQ3 diamond core was cut in half to provide a sample for assay typically weighing around 4-6kg. Samples were submitted to the ALS facility in Bor, Serbia for industry standard analytical analysis.</td></tr>
<tr><td>Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</td><td>The half core and weight of the sample is sufficiently representative.

No calibration of any equipment was required as all samples were sent for assay by a commercial laboratory.</td></tr>
<tr><td>Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.</td><td>PQ3 and HQ3 diamond core was used to obtain nominally 1m samples from which 4-6kg of material was pulverised to produce sample for fire assay, ICP-MS and X-ray Fluorescence (XRF).</td></tr>
<tr><td>Drilling techniques</td><td>Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</td><td><table>
<tr><th>Drill Hole</th><th>Non Core (m)</th><th>PQ3 Diamond Core (m)</th><th>HQ3 Diamond Core (m)</th></tr>
<tr><td>BR-10-20</td><td></td><td>0 - 101.6</td><td>101.6 - 373.6</td></tr>
<tr><td>BR-11-20</td><td></td><td>0 - 20</td><td>20 - 184</td></tr>
<tr><td>BR-12-20</td><td></td><td>0 - 25.8</td><td>258 - 130.1</td></tr>
<tr><td>BR-13-20</td><td></td><td>0 - 22.6</td><td>22.6 - 155.2</td></tr>
<tr><td>BR-17-20</td><td></td><td>0 - 94.3</td><td>94.3 - 498.5</td></tr>
<tr><td>BR-18-20</td><td></td><td>0 - 93</td><td>93 - 607</td></tr>
<tr><td>BR-20-20</td><td></td><td>0 - 113.2</td><td>113.2 - 252.2</td></tr>
<tr><td>BR-22-20</td><td>0 - 135</td><td></td><td>135 - 312.7</td></tr>
<tr><td>BR-23-20</td><td></td><td>0 - 115.5</td><td>115.5 - 368</td></tr>
</table></td></tr>
<tr><td rowspan="3">Drill sample recovery</td><td>Method of recording and assessing core and chip sample recoveries and results assessed.</td><td rowspan="3">All core was logged for geology and RQD with recovery in the mineralised and sampled zone greater than 90%. The PQ3 and HQ3 diameter and sampling of half core ensured the representative nature of the samples.

There is no observed relationship between sample recovery and grade, and with little to no loss of material there is considered to be little to no sample bias.</td></tr>
<tr><td>Measures taken to maximise sample recovery and ensure representative nature of the samples.</td></tr>
<tr><td>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</td></tr>
<tr><td rowspan="3">Logging</td><td>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</td><td>Diamond drill core samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. Not all drill holes penetrated the massive sulphide mineralisation, but all were used to guide the geological interpretations supporting the Mineral Resource estimates.</td></tr>
<tr><td>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</td><td>All core is photographed, and logging is qualitative.</td></tr>
<tr><td>The total length and percentage of the relevant intersections logged.</td><td>All core is logged.</td></tr>
<tr><td rowspan="3">Sub-sampling techniques and sample preparation</td><td>If core, whether cut or sawn and whether quarter, half or all core taken.</td><td>The diamond core was cut in half using a diamond saw. Nominally 1 in 30 samples was cut in quarters, and both halves analysed (for purposes of field duplicates).</td></tr>
<tr><td>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</td><td>Not applicable, as all samples are core.</td></tr>
<tr><td>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</td><td>Collection of around 4-6kg of half core material with subsequent pulverisation of the total charge provided an appropriate and representative</td></tr>
</table>

Section 1 Sampling Techniques and Data
(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code Explanation	Commentary
		sample for analysis. Sample preparation was undertaken at the ALS laboratory in Bor, to industry best practice.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	Whole rock blanks and certified standards (~1 in 15) were introduced to the sample run to ensure laboratory QAQC. Additionally, industry best practice was adopted by ALS for laboratory sub-sampling and the avoidance of any cross contamination.
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.	The half core sampling is considered a reasonable representation of the in-situ material. Nominally 1 in 30 samples were cut in quarters, and both halves analyses (for purposes of field duplicates).
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Sample size of around 4-6kg is considered to be appropriate to reasonably represent the material being tested.
Quality of assay data and laboratory tests	*The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*	Analyses were undertaken at the accredited laboratory of ALS in Bor, Serbia which has full industry certification. Multi elements were assayed by an ICP-AES technique following a four-acid digest. Gold was determined using a fire assay on a nominal 50g charge. Barite was determined from a lithium borate fusion followed by dissolution and ICP-AES analysis. Total sulphur was determined by Leco. All techniques were appropriate for the elements being determined. Samples are considered a partial digestion when using an aqua regia digest.
	For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	There was no reliance on determination of analysis by geophysical tools.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	Certified Reference Material ("CRM") appropriate for the elements being analysed were added at a rate better than 1 in 15. All results reported by ALS on the CRMs were better than 2 standard deviations (2SD), it is considered that acceptable levels of accuracy have been achieved. Additional lab checks were sent to SGS in Bor. To date,154 samples were submitted for check assaying from within the mineralised drill intercepts. The check assays correlated within tolerance to the original ALS assays.
Verification of sampling and assaying	*The verification of significant intersections by either independent or alternative company personnel.*	There has been no independent logging of mineralised intervals, however, it has been logged by several company personnel and verified by senior staff.
	The use of twinned holes.	None of the reported holes are twin holes.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Data is stored on the Virtual Cloud and at various locations including Vares, Bosnia & Herzegovina and Cheltenham, UK. And is managed by gDat data solutions in an acQuire database, which is regularly backed-up.
	Discuss any adjustment to assay data.	No adjustments were necessary.
Location of data points	*Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.*	Sampling sites were surveyed using Total Station to better than 0.05m accuracy in the local BiH coordinate system.
	Specification of the grid system used.	The grid system used MGI 1901 / Balkans Zone 6.
	Quality and adequacy of topographic control.	The topographic surface of the immediate area was generated from a LiDAR survey to an accuracy of approximately 0.05m. It is considered sufficiently accurate for the Company's current activities.
Data spacing and distribution	*Data spacing for reporting of Exploration Results.*	Results from two drill holes are being reported. All samples were collected at 2m intervals down hole.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	Drill hole spacing is deemed sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource classifications applied.
	Whether sample compositing has been applied.	Sample composite was not employed.

Section 1 Sampling Techniques and Data
(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code Explanation	Commentary
Orientation of data in relation to geological structure	*Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.*	Reported holes were drilled at an average declination and azimuth as stated in Table 2 of the accompanying report. The drill holes are considered to be reasonably orthogonal to the interpreted dip of the mineralisation, or close to it.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	It is not considered that the drilling orientation has introduced a sampling bias, as the drilling is considered to be orthogonal to the strata bound mineralisation, or close to it.
Sample security	*The measures taken to ensure sample security.*	Chain of Custody of digital data is managed by the Company. Physical material was stored on site and, when necessary, delivered to the assay laboratory. Thereafter laboratory samples were controlled by the nominated laboratory. All sample collection was controlled by digital sample control file(s) and hard-copy ticket books.
Audits or reviews	*The results of any audits or reviews of sampling techniques and data.*	A Site and Laboratory (ALS and SGS, Bor) visit was made by Dr Belinda van Lente, an employee of CSA Global in January 2018. There were no material issues found for the 2017 drill campaign.

Section 2: Reporting of Exploration Results
(Criteria listed in the preceding section also apply to this section)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	*Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.*	The Rupice deposit is located within the Company's 100% owned Concession, No. 04-18-21389-1/13, located 13km west of Vares in Bosnia. There are no known material issues with any third party other than normal royalties due to the State.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	The Concession is in good standing with the governing authority and there is no known impediment to the Concession remaining in force until 2038 (25 years), subject to meeting all necessary reporting requirements.
Exploration done by other parties	*Acknowledgment and appraisal of exploration by other parties.*	Modern exploration commenced with the work of Energoinvest in the late 1960s. During 1968-1969 underground development of 455m of drives and cross cuts were made, and 11 surface trenches dug for a total length of 93.5mm. Between 1980 and 1989, 49 holes were drilled for an advance of 5,690.8m. Sample material from all of these programs was routinely analysed for lead, zinc, and barite, and on occasion silver and gold. The deposit was the subject of a number of reserve estimates in the 1980s. This work is documented in many reports which are certified by those geoscientists and Institutes that undertook the work. The work is considered to be of a standard equal to that prevalent within today's exploration industry.
Geology	*Deposit type, geological setting and style of mineralisation.*	The host rocks at Rupice comprises Middle Triassic limestone, dolostone, calcareous and dolomitic marl, and a range of mostly fine-grained siliciclastic rocks including cherty mudstone, mudstone, siltstone and fine-grained sandstone. The main mineralised horizon is a brecciated dolomitic unit that dips at around 50º to the northeast and has been preferentially mineralised with base, precious and transitional metals. The Triassic sequence and has been intensely deformed both by early stage ductile shearing and late stage brittle faulting. The Rupice polymetallic mineralisation consists of sphalerite, galena, barite and chalcopyrite with gold, silver, tetrahedrite, boulangerite and bournonite, with pyrite. The majority of the high-grade mineralisation is hosted within the brecciated dolomitic unit, which is offset and cut by northwest striking, westerly dipping syn-post mineral faulting. This faulting displaces the mineralised body up to 20 metres in places. Thickening of the central portion of the orebody occurs where these faults flexure and deform. Mineralised widths up to 65 metres true thickness are seen in the central portion of the orebody. To date, the massive sulphide mineralisation at Rupice has a defined strike length of 650 metres, with an average true-width thickness of around 20 metres. However, mineralisation at Rupice still remains open towards the north and down-dip to the south.

Section 2: Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section)

Criteria	JORC Code explanation	Commentary
Drill hole information	*A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* o *easting and northing of the drill hole collar* o *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* o *dip and azimuth of the hole* o *downhole length and interception depth* o *hole length.* *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	167 diamond drill holes (38,134.65m) were used for the Mineral Resource estimate. This includes 46 historical holes (5,071.8m) not drilled by Adriatic Metals. All these holes were used to support the Mineral Resource estimate. The Mineral Resource estimate conveys the tenor of grade from the drill holes.
Data aggregation methods	*In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.*	No data aggregation methods were applied.
	Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low-grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	Not applicable as no data aggregation methods were applied.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	Equivalent explanations are described in the body of the text.
Relationship between mineralisation widths and intercept lengths	*These relationships are particularly important in the reporting of Exploration Results.*	Exploration results are not being reported.
	If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	The majority of the high-grade mineralisation is hosted within the brecciated dolomitic unit, which is offset and cut by northwest striking, westerly dipping syn-post mineral faulting. This faulting displaces the mineralised body up to 20 metres in places. Thickening of the central portion of the orebody occurs where these faults flexure and deform. Mineralised widths up to 65 metres true thickness are seen in the central portion of the orebody. To date, the massive sulphide mineralisation at Rupice has a defined strike length of 650 metres, with an average true-width thickness of around 20 metres. However, mineralisation at Rupice still remains open towards the north and down-dip to the south. Recent drilling by Eastern Mining was mostly inclined at between 70° and 80° to the southwest, perpendicular to the deposit strike, and intersected the mineralisation reasonably orthogonally.
	If it is not known and only the downhole lengths are reported, there should be a clear statement to this effect (e.g. 'downhole length, true width not known').	True width intercepts in drill holes being reported are as follows – BR-10-20 – 1.7m BR-11-20 – 4.8m BR-12-20 – 2.9m BR-13-20 – 10.0m BR-17-20 – 1.4m BR-18-20 – 7.0m BR-20-20 – 9.8m BR-22-20 – 4.0m BR-23-20 – 7.0m

Section 2: Reporting of Exploration Results
(Criteria listed in the preceding section also apply to this section)

Criteria	JORC Code explanation	Commentary
Diagrams	*Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	Relevant maps and diagrams are included in the body of the report.
Balanced reporting	*Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high-grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	Not applicable. All mineralised incepts are being reported.
Other substantive exploration data	*Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	No substantive exploration data not already mentioned in the report has been used in the preparation of the Mineral Resource estimate.
Further work	*The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).*	Further drilling is being undertaken for geotechnical and hydrological purposes, and extension exploration drilling.
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Diagrams have been included in the body of this report.

Section 3: Estimation and Reporting of Mineral Resources
(Criteria listed in section 1, and where relevant in section 2, also apply to this section)

Criteria	JORC Code explanation	Commentary
Database integrity	*Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.*	Data used in the Mineral Resource Estimate was provided as a validated Micromine database, which in turn was sourced from a validated database prepared by Adriatic Metals. The validation routines were employed to confirm validity of data. Key files (collar, survey, geology, assay) were validated to ensure that they were populated with the correct original data. All drill holes were logged to electronic logbooks. All drill hole collar, downhole survey and geological data are stored on the Virtual Cloud and at various locations including Vares, Bosnia & Herzegovina and Cheltenham, UK. And is managed by gDat data solutions in an acQuire database. The database is updated as new data become available.

	Data validation procedures used.	The resultant database was validated for potential errors in Micromine software using specially designed processes.
		The following error checks were carried out during final database creation:
		• Missing collar coordinates.
		• Missing values in fields FROM and TO.
		• Cases when FROM values equal or exceed TO ones (FROM≥TO).
		• Data availability. The data availability was checked for each drill hole in the tables:
		  – Collar coordinates
		  – Sampling data
		  – Downhole survey data
		  – Lithological characteristics.
		• Duplicate drill hole numbers in the table of the drill hole collar coordinates.
		• Duplicate sampling intervals.
		• Duplicate downhole measurement data.

Section 3: Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section)

Criteria	JORC Code explanation	Commentary
		• Duplicate intervals of the lithological column. • Sample "overlapping" (when the sample TO value exceeds FROM value of the next sample). • Negative-grade samples. Drill hole data was verified against source documentation. The surveyed drill holes were then also verified visually for consistency. **The Competent Person is satisfied that database integrity is appropriate to support Mineral Resource estimation.**
Site visits	*Comment on any site visits undertaken by the Competent Person and the outcome of those visits.*	Phillip Fox is based on-site in Vares and was responsible for planning and implementation of the recent drilling programs, overseeing the preparation of the samples and their dispatch to the various laboratories. Mr. Fox assumes responsibility for the data components, QA/QC and geological interpretation. Dmitry Pertel assumes responsibility for the grade interpolation and reporting of the Mineral Resource estimate and has previously completed a site visit.
	If no site visits have been undertaken, indicate why this is the case.	A site visit has been undertaken.
Geological interpretation	*Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.*	Sufficient drilling has been conducted to reasonably interpret the geology and the polymetallic mineralisation. The mineralisation is traceable between numerous drill holes and drill sections. Interpretation of the deposit was based on the current understanding of the deposit geology. Each cross section generally spaced 20-30 m apart was displayed in Micromine software together with drill hole traces colour-coded according to grade values. The interpretation honoured modelled fault planes and interpretation of main geological structures. The mineralised structure of the deposit was interpreted and modelled using core logging data. The low-grade halo domain was interpreted to capture all mineralized samples, and based on the current understanding of the geological model. The fault zones were interpreted and modelled using geological logging. Cut-off grades for high grade domains were 10% for Zn, 3% for Pb, 25% for $BaSO_4$, 1% for Cu, 2.5g/t for Au, and 110g/t for Ag. All cut-offs selected for interpretation were based on results of classical statistical analysis. The interpretation was independently reviewed by a consultant geologist.
	Nature of the data used and of any assumptions made.	Geological logging in conjunction with assays has been used to interpret the mineralisation. The majority of holes were sampled at 2m intervals, with some more detailed sampling conducted.
	The effect, if any, of alternative interpretations on Mineral Resource estimation.	Alternative interpretations are likely to materially impact on the Mineral Resource estimate on a local, but not global basis. No alternative interpretations were adopted at this stage of the project.
	The use of geology in guiding and controlling Mineral Resource estimation.	Geological logging in conjunction with assays and results of the statistical analysis has been used to interpret the mineralisation. Available historical maps and sections have been used to guide interpretation. All internal waste was included into the interpreted mineralised bodies.
	The factors affecting continuity both of grade and geology.	Continuity is affected by the nature of the host rocks, interpreted faults and limits of the drill holes. **The Competent Person is satisfied that the geological interpretation is appropriate to support Mineral Resource estimation.**
Dimensions	*The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	The strike length is about 650m and width up to 250m. The combined thickness of the mineralised zones varies from several metres to 65m. Depth below surface is from 0 to 380 m, which is the lower limit of current drilling. **The Competent Person is satisfied that the dimensions interpreted are appropriate to support Mineral Resource estimation.**
Estimation and modelling techniques	*The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.*	The Mineral Resource estimate was based on surface diamond drill core using ordinary kriging (OK) to form 5x5x5m blocks. The block model was constrained by wireframes modelled based on geology using sectional interpretation. Additional wireframing for each element for the high-grade domains within these geological wireframes (except for As, Sb and Hg) was completed. Weakly mineralised halos and fault zones used geological logging and multi-element assay data. The applied cut-off grades for high grade domains were:

Section 3: Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section)

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td></td><td></td><td>
<table>
<tr><th>Element</th><th>HG Cut-offs</th></tr>
<tr><td>S, %</td><td>10</td></tr>
<tr><td>Zn, %</td><td>10</td></tr>
<tr><td>Pb, %</td><td>3</td></tr>
<tr><td>Au, g/t</td><td>2.5</td></tr>
<tr><td>Ag, g/t</td><td>110</td></tr>
<tr><td>Cu, %</td><td>1</td></tr>
<tr><td>BaSO4, %</td><td>25</td></tr>
</table>
Micromine software was used to generate the wireframes and for block modelling
Hard boundaries were used between mineralised lenses at each domain. The drill hole data were composited to a target length of 2m based on the length analysis of raw intercepts.
Geostatistical analysis was completed for all elements, and averaged long ranges were employed to justify the search ellipse – 102m along strike, 61m down dip and 31m across dip.
Interpolation parameters were:
Search pass 1: 2.5m by 2.5m by 2.5m. Minimum samples number - 1, minimum holes – 1, maximum samples number - 16.
Search pass 1: 1/3 of the variogram log ranges. Minimum samples number - 3, minimum holes – 2, maximum samples number - 16.
Search pass 2: 2/3 of the variogram log ranges. Minimum samples number - 3, minimum holes – 2, maximum samples number - 16.
Search pass 3: Full semi-variogram ranges. Minimum samples - 3, maximum samples – 16, minimum holes 2.
All subsequent search passes: incremented by full semi-variogram ranges in each direction. Minimum samples – 1, maximum samples – 16, minimum holes - 1.
Block discretisation 2*2*2.
The optimal parent cell size was selected in the course of block modelling based of 20x20m exploration drilling.
Classical statistical analysis was used to identify grade domains for barite, gold and silver.
The Competent Person is satisfied that estimation and modelling techniques are appropriate to support Mineral Resource estimation.
</td></tr>
<tr><td></td><td>The availability of check estimates, previous estimates and/or mine production records and whether the MRE takes appropriate account of such data.</td><td>Previous JORC-compliant Mineral Resources were estimated by CSA Global in July 2019. The current estimate is about 32% higher in tonnage and about 22% lower grades due to the modelling methodology and domaining applied.
Mine production results were not available.</td></tr>
<tr><td></td><td>The assumptions made regarding recovery of by-products.</td><td>The Rupice deposit is a silver-gold-zinc-lead-barite deposit. Previous mining and beneficiation over a four-year period have shown that a conventional sulphide flotation method is a suitable recovery method. Metallurgical test work is ongoing to optimise the process flowsheet.</td></tr>
<tr><td></td><td>Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).</td><td>As, Sb and Hg have been estimated in the model using their own semi-variogram models and OK interpolation method.</td></tr>
<tr><td></td><td>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</td><td>The average exploration drilling spacing was 20x20m. The selected parent cell size was 5x5m (quarter the exploration density). The search was based on the results of geostatistical analysis with average for all elements long ranges of 102x61x31m.</td></tr>
<tr><td></td><td>Any assumptions behind modelling of selective mining units.</td><td>No assumptions were made for selective mining unit, apart from the assumption that the deposit is likely to be mined by underground method and that 5x5m parent cell approximately reflects SMU for underground mining.</td></tr>
<tr><td></td><td>Any assumptions about correlation between variables.</td><td>Correlation between some variables was very strong (for example, between silver and lead), but no assumptions were made for the modelling purposes.
Correlation between bulk density and main elements ($BaSO_4$, Pb, Zn and Cu) was used to calculate bulk density for all model domains except for the combined high-grade domain.</td></tr>
<tr><td></td><td>Description of how the geological interpretation was used to control the resource estimates.</td><td>Geological interpretation of the mineralised zone, weakly mineralised halo and fault zones was based on the geological logging. When grades within modelled wireframes for the mineralized zone had mixed populations, high-grade domain was modelled using cut-offs justified by statistical analysis.</td></tr>
</table>

Section 3: Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section)

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td></td><td></td><td>High grade domains for each element were modelled individually, except for As, Sb and Hg, which did not demonstrate mixed grade populations within the modelled mineralized zone.</td></tr>
<tr><td></td><td>Discussion of basis for using or not using grade cutting or capping.</td><td>Classical statistical analysis was carried out for each element and each domain. It was found that histograms and probability plots did not demonstrate any apparent mixed populations within the limits of corresponding modelled domains. Top-cuts were identified and applied as shown in the table below:
<table>
<tr><th>Element</th><th>Halo</th><th>Faults</th><th>Low Grade</th><th>High Grade</th></tr>
<tr><td>S, %</td><td>20</td><td>-</td><td>-</td><td>-</td></tr>
<tr><td>Zn, %</td><td>5.0</td><td>-</td><td>-</td><td>-</td></tr>
<tr><td>Pb, %</td><td>-</td><td>-</td><td>-</td><td>-</td></tr>
<tr><td>Au, g/t</td><td>-</td><td>-</td><td>-</td><td>-</td></tr>
<tr><td>Ag, g/t</td><td>400</td><td>60</td><td>850</td><td>-</td></tr>
<tr><td>Cu, %</td><td>1.92</td><td>0.49</td><td>-</td><td>-</td></tr>
<tr><td>BaSO4, %</td><td>-</td><td>43</td><td>-</td><td>-</td></tr>
<tr><td>Sb, %</td><td>1.1</td><td>-</td><td colspan="2">-</td></tr>
<tr><td>As, %</td><td>0.42</td><td>0.39</td><td colspan="2">1.66</td></tr>
<tr><td>Hg, ppm</td><td>320</td><td>150</td><td colspan="2">2,000</td></tr>
</table></td></tr>
<tr><td></td><td>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</td><td>Grade estimation was validated using visual inspection of interpolated block grades versus underlying data, and swath plots.
Swath plots demonstrated reasonable correlation of modelled grades with the sample composites.
The Competent Person is satisfied that estimation and modelling techniques are appropriate to support Mineral Resource estimation.</td></tr>
<tr><td>Moisture</td><td>Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.</td><td>The tonnages were estimated on an in-situ dry bulk density basis which includes natural moisture. Moisture content was not estimated.</td></tr>
<tr><td>Cut-off parameters</td><td>The basis of the adopted cut-off grade(s) or quality parameters applied.</td><td>The reporting cut-off grade of 50g/t silver equivalent was supported by estimation of marginal cut-off for underground mining using input economic parameters and criteria.
The Competent Person is satisfied that cut-off parameters were appropriately considered, to support Mineral Resource estimation.</td></tr>
<tr><td>Mining factors or assumptions</td><td>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</td><td>A scoping and on-going preliminary economic assessment studies were performed to ensure that there are reasonable prospects for the eventual economic extraction of the mineralisation, which demonstrated that the deposit is likely to be developed by underground mining method(s). Input parameters were provided by the Company as being typical for the commodity, mining method and costs for a Balkan silver-lead-zinc mining operation.</td></tr>
<tr><td>Metallurgical factors or assumptions</td><td>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</td><td>A number of flotation tests have recently been carried out on both Rupice and Veovača (nearby deposit) bulk samples. Preliminary results indicate there is potential to produce Zn, Pb/Cu and barite concentrates via flotation processes, with good recoveries of all constituents reported in this Mineral Resource estimate.
The test work also indicates that a barite product that meets market specification requirements of purity, specific gravity, and fineness of particle size can be achieved, which meets the requirements of Clause 49 of the JORC Code.
This test work remains ongoing.
The Competent Person is satisfied that metallurgical factors and assumptions were appropriately considered, to support Mineral Resource estimation.</td></tr>
<tr><td>Environmental factors or assumptions</td><td>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential</td><td>No detailed assumptions regarding possible environmental impacts to the site area were considered. The general locality has a number of active mining operations and no environmental impediments are anticipated.</td></tr>
</table>

Section 3: Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section)

Criteria	JORC Code explanation	Commentary
	environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfield project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.	
Bulk density	*Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.*	Bulk densities were determined on drill core every 2m in ore and every 5m in waste. At total of 5,864 determinations were used to calculate regression formulas using barite, lead zinc and copper grades vs bulk density or to interpolate bulk density values into the combined high-grade domain.
	The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.	Bulk density determinations adopted the weight in air / weight in water method using a suspended or hanging scale. First the core billet was accurately weighed dry ("in air"), the core billet was removed, and the wire cage fully submerged in water and its tare set to "zero" mass. The billet of core was then fully submerged and weighed ("weight in water"). The bulk density is calculated by the formula BD = Md / Md – Mw, where Md = weight in air and Mw = weight in water.
	Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.	No assumptions were made for Bulk Density. **The Competent Person is satisfied that density was appropriately considered, to support Mineral Resource estimation.**
Classification	*The basis for the classification of the Mineral Resources into varying confidence categories.*	Resource classification was based on confidence in the QA/QC data analysis, geological interpretation, drill spacing, geostatistical measures, a visual evaluation of cross sections and drill density, and manual interpretation of resource categories. The interpreted boundaries between categories were wireframed and used to code the block models. Generally, the Indicated category was assigned to the areas with reasonable continuity of mineralised lodes based on 20x20m and 40x40m exploration drilling. All other blocks were classified as Inferred. No blocks were classified as Measured
	Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).	The classification has taken into account all available geological and sampling information as well as the structural information, and the classification level is considered appropriate for the current stage of this project.
	Whether the result appropriately reflects the Competent Person's view of the deposit.	The Mineral Resource estimate appropriately reflects the view of the Competent Person. **The Competent Person is satisfied that classification of this Mineral Resource estimate appropriately reflects the data and interpreted geological controls on mineralisation.**
Audits or reviews	*The results of any audits or reviews of MREs.*	The current model has not been audited by an independent third party but has been subject to CSA Global's internal peer review processes.
Discussion of relative accuracy/ confidence	*Where appropriate a statement of the relative accuracy and confidence level in the MRE using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.*	Industry standard modelling techniques were used, including but not limited to: • Classical statistical analysis, cut-offs selection. • Interpretation and wireframing. • Top-cutting and interval compositing. • Geostatistical analysis. • Block modelling and grade interpolation techniques. • Model classification, validation and reporting. The relative accuracy of the estimate is reflected in the classification of the deposit. The relative accuracy of the Mineral Resource estimate is reflected in the reporting of the Mineral Resource to an Indicated and Inferred classification as per the guidelines of the 2012 JORC Code.
	The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.	The statement refers to global estimation of tonnes and grade and is suitable for use in a subsequent PFS and further exploration at the deposit.

Section 3: Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section)

Criteria	JORC Code explanation	Commentary
	These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.	No production data is available. The Competent Person is satisfied that classification of this Mineral Resource estimate appropriately reflects the data and interpreted geological controls on mineralisation.